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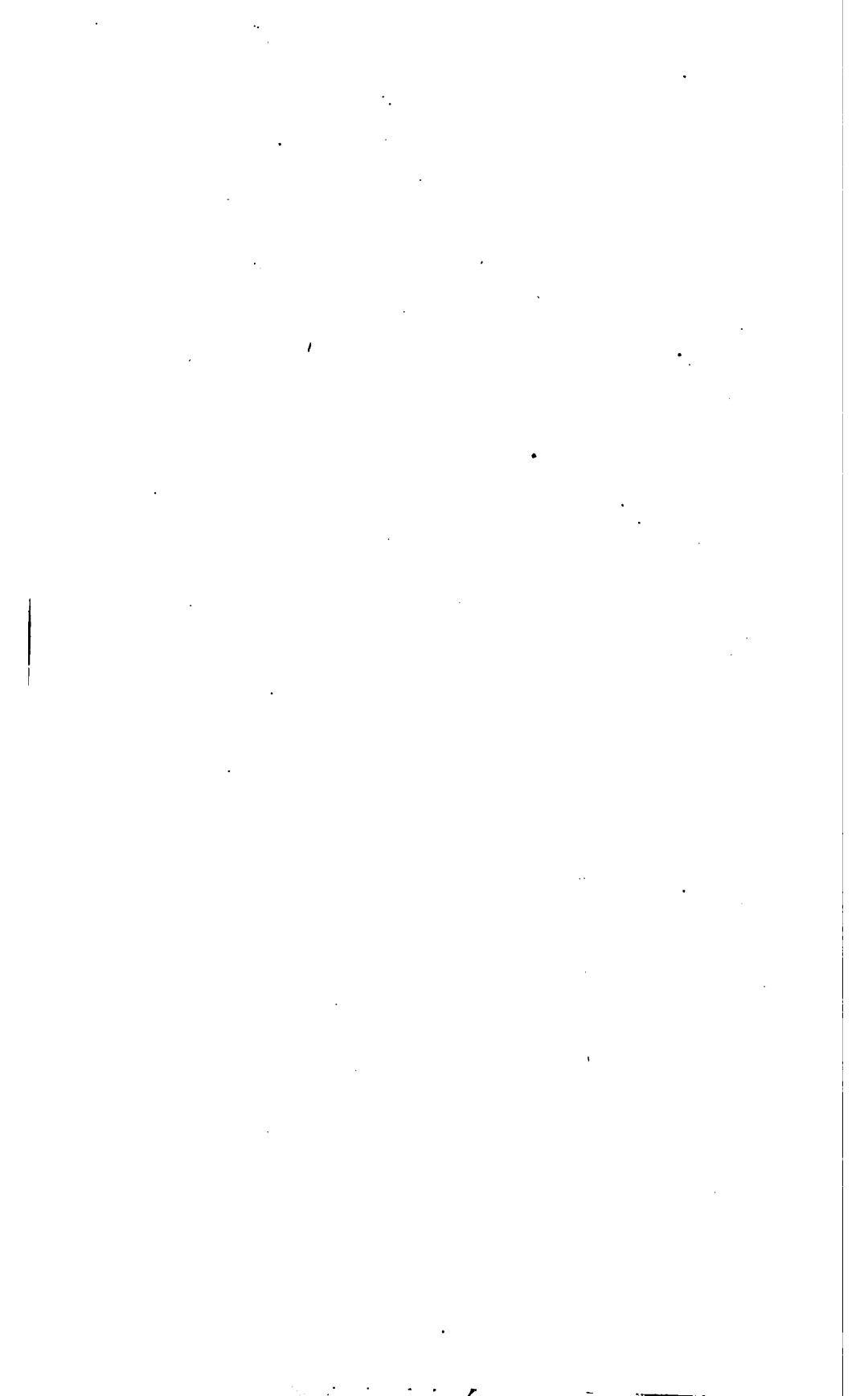


FROM THE

UNITED STATES GOVERNMENT







War 759.17

**TRAINING MANUAL**  
**IN**  
**TOPOGRAPHY, MAP READING**  
**AND RECONNAISSANCE**

Prepared by  
**MAJOR GEORGE R. SPALDING**  
CORPS OF ENGINEERS

Under the direction of the Chief of Engineers, U. S. Army



WASHINGTON  
GOVERNMENT PRINTING OFFICE  
1917



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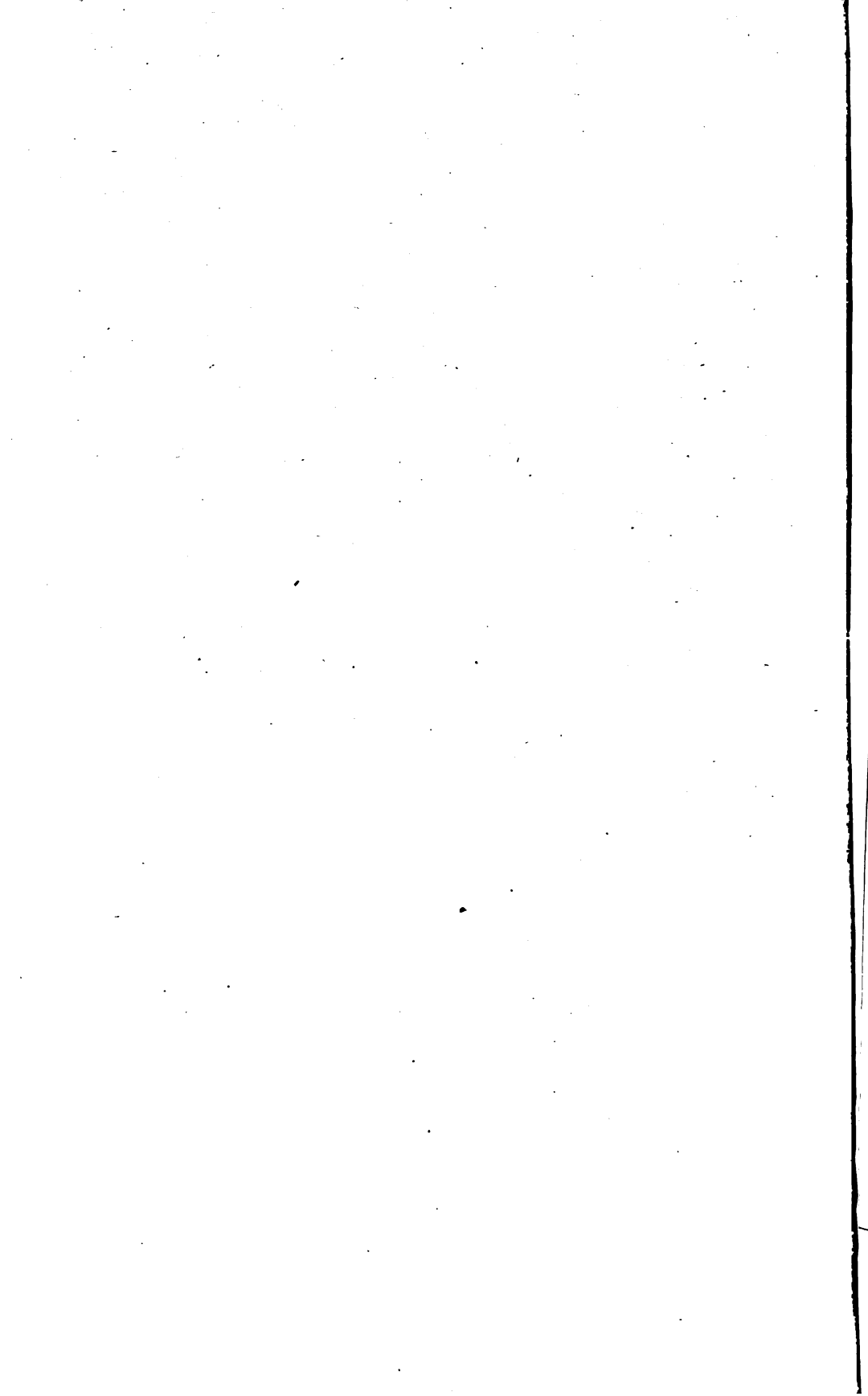
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# TRAINING MANUAL IN TOPOGRAPHY, MAP READING, AND RECONNAISSANCE.

## LESSON I.

### TOPOGRAPHY.

1. So important is the influence of "*the lay of the land*" upon *military operations* that every officer must thoroughly acquaint himself at the earliest practicable moment with the topography of the area within which his responsibilities lie.

2. A mere knowledge of the main roads, of the direction and distances to near-by towns is by no means sufficient. He must know where the plains are, where the hills rise, how the streams run. *He must have a mental picture, a bird's-eye view, impressed on his brain of the main physical and military features of his territory.*

### EROSION.

3. The faculty for grasping the topography of an area as a whole is rarely a natural one. "*To the beginner*" in the study of topography "*every hill is an isolated feature—the elevations and depressions of ground present to him nothing but irregularity and confusion.*"

4. As a matter of fact, there is a considerable degree of regularity and system in our present-day ground forms. Whatever may have been the irregularity and confusion of the original surface of the earth, practically all of the *ground forms which we know to-day are the result of erosion.*

5. It has been estimated that the average elevation of the land surface has been reduced 7,000 feet by erosion. Winds and waves, glaciers, chemical action, frost, and plant growth have all had their part in the breaking up and wearing down of the original rocks, but by far the larger portion of the *ground forms which exist to-day have been carved out of the older formations by the action of running water.*

### MASTER LINES OF TOPOGRAPHY.

6. Not all the water in heavy rains can seep into the soil; much of it runs off. At one point a little stream begins; as it flows downward another joins it; soon several unite into a fair-sized creek, which rushes along carrying its burden of soil into the main valley, whence the river may carry it on toward the sea. This simple process continued for ages has sufficed to *carve out our deepest valleys.* It is continuing to deepen them year by year, and more and more to wear down the ridges between the valleys.

7. If our remaining ground forms are the result of such a process, it is manifest that the *drainage lines* of an area, together with the *ridge lines*, form a system of *master lines* which, once traced out and studied, will give a grasp of the main features of the topography that can be had in no other way.

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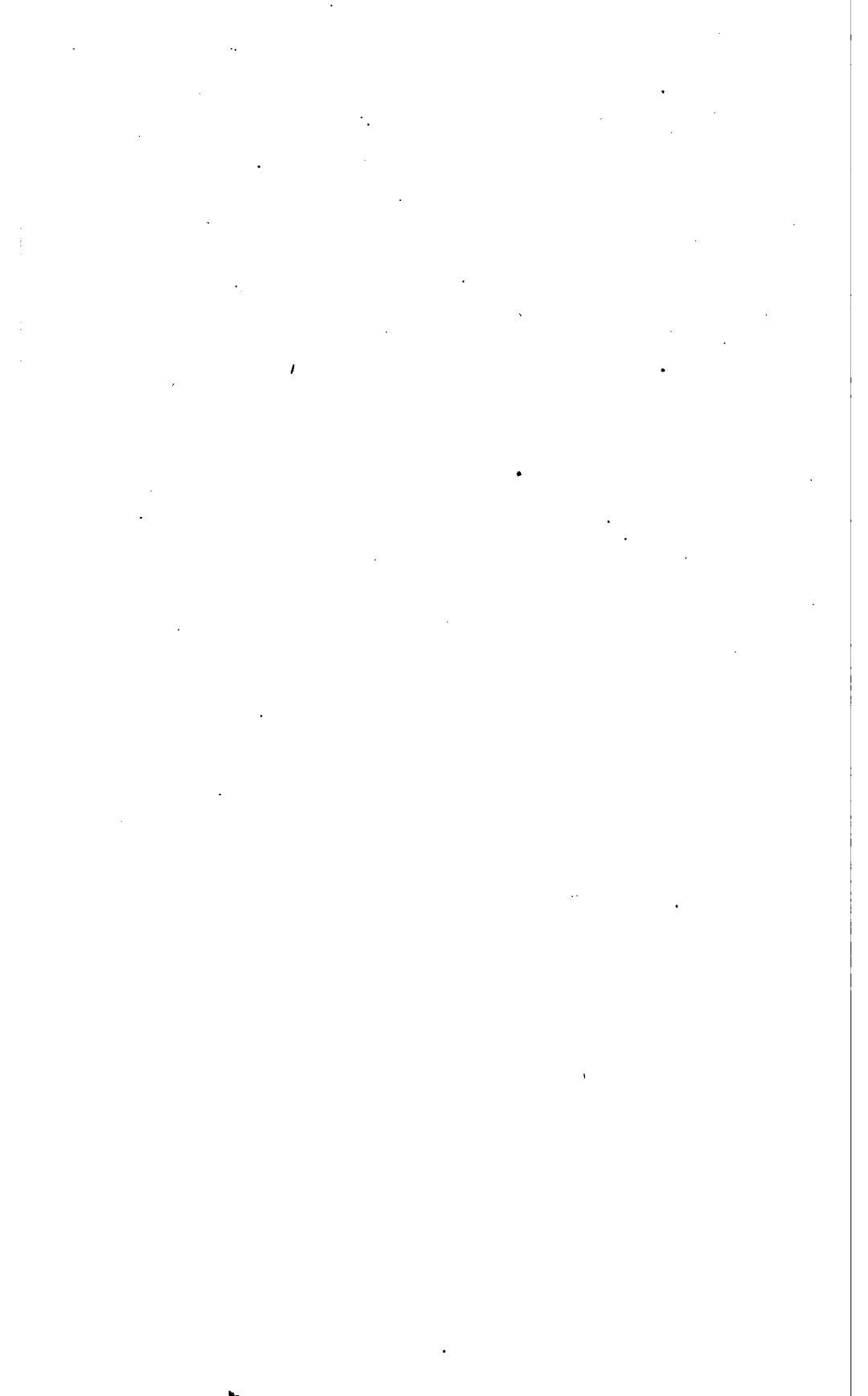


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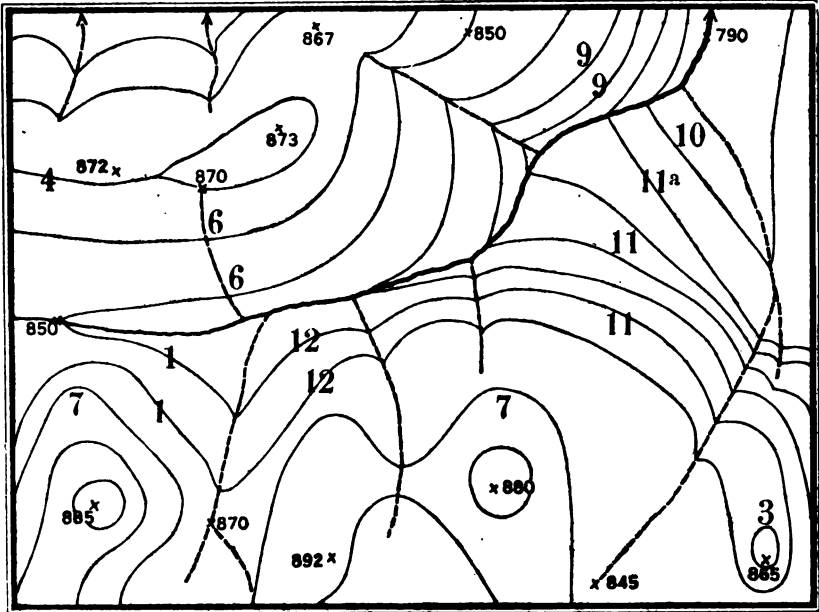


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## PRACTICE WORK.

21. Figures VI, VII and VIII are sketches giving the drainage net and critical points of three areas in the vicinity of Fort Leavenworth, Kans. The instructor will require each member of the class to trace these skeletons one at a time and to draw in the contours following the systematic method heretofore described.

There can be no better training for one who is studying topography, sketching, or map reading. Not until one can complete a skeleton such as these, with great readiness, is he able to take up the reading of or sketching of topography. It is not considered desirable for anyone to take up the study of Lesson III until he has mastered



**MISTAKES IN DRAWING CONTOURS**  
**FIGURE V**

"logical contouring." It may be necessary, therefore, to devote an additional lesson period to practice in drawing contours.

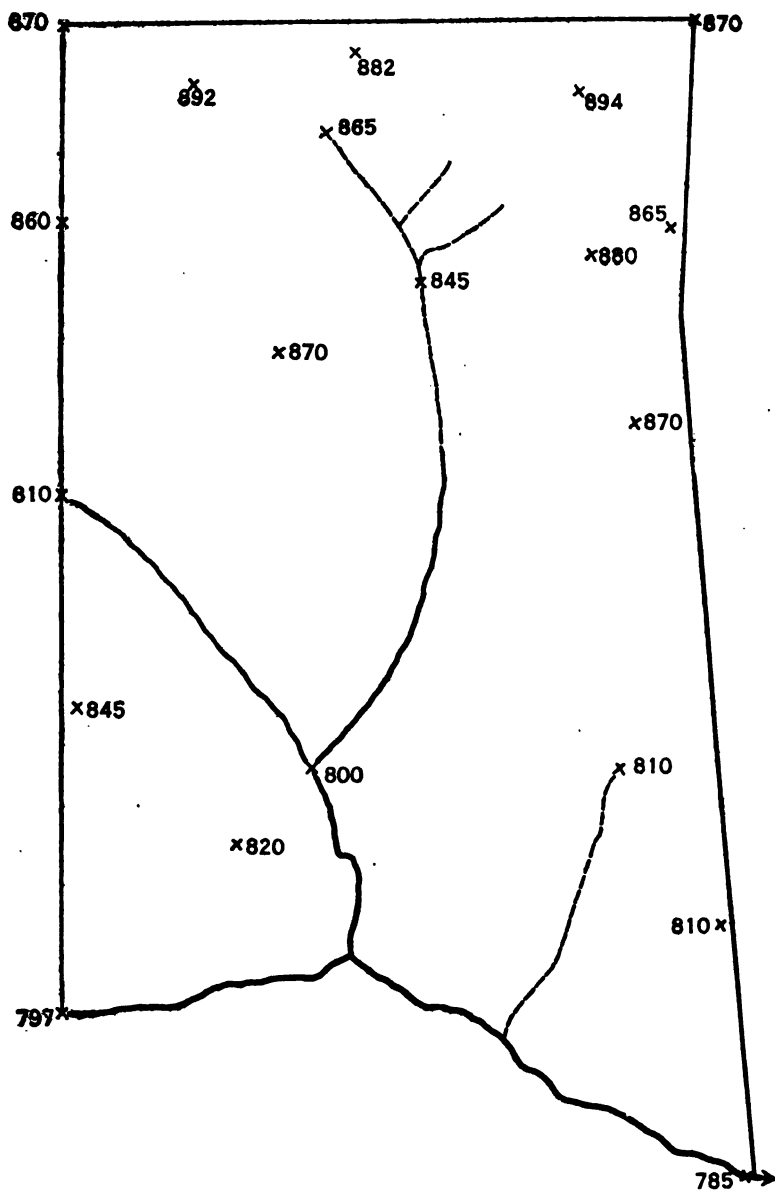
## LESSON III.

## SKETCHING.

22. The instruments issued by the Engineer Department for sketching are based on the plane-table method. They are simple. Skill in their use can not, of course, be acquired without practice, but one can *begin* to use them with very little preliminary instruction.

It is the beginner's lack of a general plan of operations, his lack of appreciation of the essentials, his waste of effort and patience on the nonessentials, that make sketching the *bête noire* of a soldier's training, rather than the admitted inaccuracy of hand instruments and his lack of skill in their use.





**DRAW 10-FT. CONTOURS ON THE ABOVE SKETCH**

**LOWEST CONTOUR 790**

**FIGURE VI**

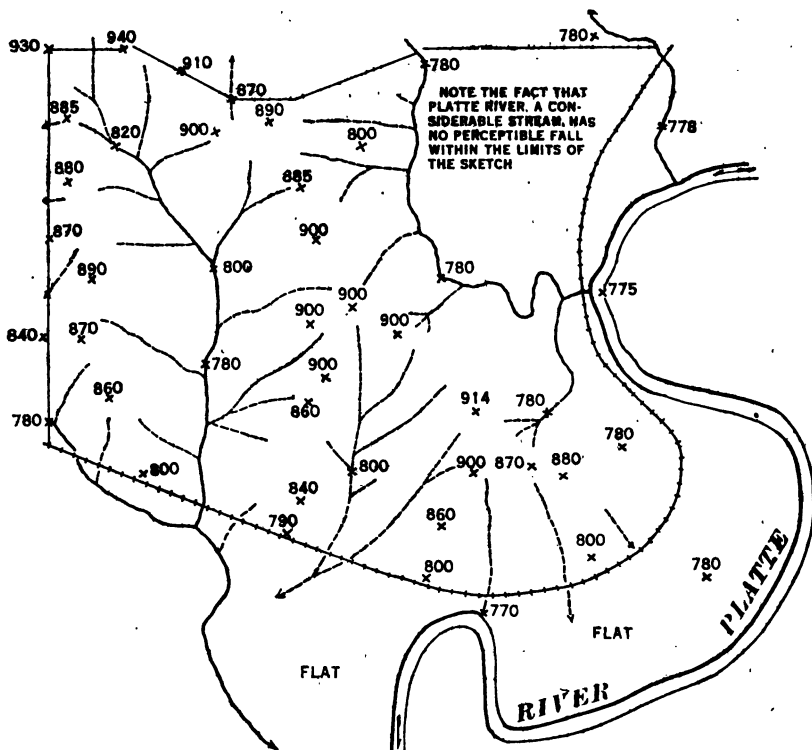


following method is for the beginner. It may be modified as he becomes more expert.

24. First, traverse around the area, returning to the point of beginning. In traversing, locate—

(a) Every drainage line crossed or which runs along generally parallel to the line of the traverse and note the direction in which the stream flows (or the dry creek drains). This is absolutely necessary.

(b) Every house or other easily identified feature near the road, which will enable the sketcher later to identify himself on the sketch.



DRAW 20-FT. CONTOURS ON THE ABOVE SKETCH

LOWEST CONTOUR 780

FIGURE VIII

(c) The high points between drainage lines, i. e., the point on the ridge line where the traverse crosses the ridge line and a point or so on each side of the traverse on the ridge to locate the ridge line as well as may be possible.

(d) Determine the elevations of all of these points. Do not draw any contours yet. Even the experienced sketcher should be slow to put in contours until he has reconnoitered enough of the area to pin down the drainage system. He must wait until he has seen enough of

*the country to know how the big features lie. The little ones will take care of themselves later as the work progresses.*

25. **Second, adjust the traverse.** When in the circuit traverse the sketcher has reached a point from which the point of beginning can be seen, it will be found that when the instrument is oriented the ray to the point of beginning on the ground will not pass directly through the point of beginning as plotted on the paper. This is to be expected. If the error in direction is not out more than a degree, let it go at that for the time being and pace the distance to the point of beginning. Lay this distance off on the ray as actually drawn.

*There will be an error of closure.* If there has been no opportunity to check *orientation* or *distance* in the circuit, it will be good work if the closing error is not greater than 5 per cent of the entire length of the traverse. Providing the error in direction can not be accounted for by *local attraction at any point*, nor the error in distance by *incorrect plotting of any course*, *distribute the error* by moving points of traverse.

26. It will not be necessary to go into refinements in this adjustment. *Move the last point up to the point of beginning; the next to last point but one in the same direction but a lesser distance, etc. Be sure in doing this that no two courses have a plotted angle between them which differs noticeably from the actual angle on the ground; otherwise your sketch will mislead some one.* The sketch must have no *misleading errors*. It will have errors, but they must not be those which will mislead.

27. **Third, traverse through the area.** The sketcher has *now been around the area*. He has located all the *water that flows into the area and all that flows out*. He has *tied down his drainage system pretty well*. He will have noted the relative size of the streams or drainage lines and their elevations and this will give him a good idea as to which ones are the *main drainage lines of the areas*. He must now find out *how these drainage lines connect up inside his area*. In open country he may be able to locate the stream junctions in the interior by intersections from the traverse. Ordinarily, however, these stream junctions are hidden by tree growth or folds of the ground. It never does in sketching (at least for a beginner and seldom for an experienced man) to *guess how the drainage runs through the area*. *There is no royal road to stream junctions.*

If the sketch is to be a truthful report of a topographic reconnaissance, the sketcher must make the reconnaissance. Let him *traverse into the interior and find out what is there*.

*Here is where the bad misleading mistakes of the sketch made by an untrained man are apt to be made.* Contrary to all advice he has probably attempted to contour as he went along. He has drawn in a number of ground forms as they appeared to him as he went along on his circuit traverse. These forms are usually exaggerated in size. *Every hill looks big when one is on top of it*. His forms therefore project into his area much farther than they should. When he gets inside, he must either rub them all out or change his drainage lines, which he finds by reconnaissance to be *thus and so to so and thus* to correspond to his badly built ground. The result is worse than useless; it will deceive the user of the sketch.

28. The manner in which the *drainage connects up inside the area can only be found by going into the area and contouring must wait on*

this information. In entering the area follow a road or trail (the location of such features are needed anyway) and the sketcher traverses as he goes. *One traverse* across the area may not be enough; usually will not be enough, though if the line followed is well considered, short offset traverses from the cross traverse will serve to locate the *main drainage lines* of a small area (less than a square mile).

In these *cross traverses* it is sometimes best to follow the *main valley* and sometimes best to follow the *ridges*. The knowledge of the area as gained by the circuit traverse will help determine which is the easiest route to traverse to *get the stream junctions and ridge line points needed*. But any line at all will do if one is careful to run as accurate a traverse as he can and *remembers what he is looking for*. He must never run a haphazard traverse and be satisfied with the information found along it.

He must get off the line by offsets if necessary to get vital information such as stream junctions and stream heads or spur directions.

The beginner should never leave his instrument on the line of traverse and wander off to see what he can see. If he does he will plot it wrong when he gets back. *He must pick up the instrument and take it with him, traversing as he goes*. He may find a gold mine in the way of an outlook which will open up the entire countryside to his view and enable him to *check back* and insure his *orientation and distance*.

29. **Fourth, adjust.** Now the student has been around his area and has been *inside* and searched out and located his *stream junctions and ridge lines*. He has a skeleton much like the ones he has contoured by interpolation. But unless he has been adjusting his elevations all the time he will have some very peculiar level data. He will find that a stream which is 200 feet high on entering his area and 150 feet high as it leaves, has a most unaccountable elevation of 148 feet in the interior of his area. He will also have found on his first circuit that the elevations did not close and he will have adjusted this by dropping back. In other words, as he arrives on his circuit at the point where he began, he will find that he is 20 feet above the proper elevation. This is not bad if his circuit has been long. It is to be expected with a clinometer. Of course, he accepts the elevation of the point of beginning as correct; changes the last station by 15 feet, the next to the last but one by 10 feet, the next to the last but two by 5 feet, and leaves the rest as they are, or he may carry the distribution of the error down a little finer by taking in more stations and making the change more gradually, but any reasonable adjustment is all right, providing, of course, he maintains *elevations within sight of each other relatively correct*.

*He must not in his adjustment make a stream deep where it is shallow or vice versa nor must he change a hollow to a rise*. Similarly he must adjust his cross lines. When he crosses a stream line, two points of which he has already located in his circuit traverse, he must know that he should get an elevation of his crossing point corresponding to the relative distances to the two points already determined (unless there is in between some feature such as a waterfall or rapids or a dam. These things will discover themselves if the sketcher is on the lookout for them).



30. The reconnaissance sketcher has few, if any, points located for him with precision. He must, therefore, use all of his knowledge of ground, of water flow, of railroad grades, etc., to keep his work logical and consistent. He must know that large rivers do not fall more than a few inches to the mile (unless full of rapids); that within the area likely to be covered by a reconnaissance the fall of a large river will be so little as to be not readily ascertainable with reconnaissance instruments. He must know that any water-carrying drainage line (that is one carrying water the year around) is apt to have a lesser fall than a dry gully in the same vicinity and his acquaintance with the region being sketched will (if he observes) give him some idea as to the approximate fall per mile. He must know that as a reasonably true proposition tributaries have a greater fall than main water lines. His work must be continually required to answer such tests. If it does not he must be ready to give the reason.

#### CONTOURING THE SKELETON.

31. It is assumed that the student has now a logically correct skeleton of the drainage system and ridge lines. He must, of course, be sure that he has in all the roads and trails of military importance. He must not show these connecting up and running through unless he knows they connect up or run through and where they connect up and run. He must always remember that he is making a reconnaissance and reporting the result of his reconnaissance, not filling up inches on his sheet with conjectures. He must leave a blank if he *does not know*. The student should now take this skeleton and contour it without going back over the country. (I hear the objection, "I thought you should not draw what you do not see or can not remember. I thought one should never sketch in contours except in the face of facts.") Well enough, for the man who can do this, but the reconnaissance sketcher must learn. He can not follow the methods of the experts at once. By requiring him to contour his sketch, the data of which is incomplete, as of course it will be with the beginner, he will find out what essential data he has left out. He will find that he forgot to get the elevation of a hill, or the direction line of a ridge or a stream junction; he will have forgotten whether a certain stream had banks 10 feet high or 50 feet high; he will find that he left out the direction of the flow of a certain stream, and for the life of him will not be able to remember which way it did flow. All of this will teach him to put down his data in sufficient fullness so that he will be able to contour correctly from the data on his sheet, at least as correctly as the time spent on his reconnaissance will justify.

32. After the beginner has done a number of area sketches in this way he will have arrived at the time when he can sketch in form lines as he goes along (lightly, because they will be later rubbed out) and later can, after he has covered enough of the area to find the trend of the big features, complete his work as he goes along. But all of this presupposes that he has become so expert in his traversing that he will need to do little adjusting and that his eye for ground has developed to the point where he can see the forms and knows how to represent them on paper. Even then he will be tripped up occasionally and be obliged to rub out much work if he begins to contour

too early. One can contour as he goes along if he is working with accurate instruments and is sure that no adjustment will be needed later, but when working with reconnaissance instruments he is very apt to get into trouble.

#### LESSON IV.

33. In Lesson III there was described as fully as possible the procedure to be followed by a beginner in executing an area sketch. This procedure was given before the instruments and the technique of their use were described for two reasons:

First. It was felt that many of the officers and men under instruction will have had previous experience in the use of sketching instruments and that, therefore, they should proceed in the third lesson period as outlined.

Second. As the main purpose of this manual is not to teach the use of any particular set of instruments, but rather to teach the principles of topography, it was believed that the dry detail about instruments, scales, etc., might well wait until the class had absorbed a proper idea of what a contoured sketch is and what the procedure in learning to make one should be.

#### FIELD SKETCHING INSTRUMENTS AND THEIR USE.

34. The Engineer Department has designed a standard field sketching outfit, based solely upon the *plane table method* of sketching. The entire outfit packs conveniently into a carrying case. The supplies which are expendable consist of pencils, erasers, sketching paper, and celluloid. The celluloid is for use in the rain. The permanent equipment consists of a small plane table with folding wooden tripod, a service clinometer, a pace tally, an alidade, pencil pocket, which pins onto the service coat, and a holder for carrying timing pad in mounted work.

#### THE ALIDADE.

35. The alidade supplied is used for three purposes: (1) To determine differences in elevation from the scales of slopes provided; (2) for use as a sighting vane; (3) for use as a measuring scale, there being provided in addition to the scale of inches, blank spaces for pasting on individual scales of double paces, etc.

#### SCALE OF STRIDES.

36. Before proceeding to sketch it is of course essential for each sketcher to secure or construct a working scale. If the work is to be done dismounted the scale should be in strides (double paces). To prepare a scale of your strides for a sketch which is to be made 6 inches equal 1 mile, proceed as follows:

Measure off a rating course of 1 mile,  $\frac{1}{2}$  mile, or  $\frac{1}{4}$  mile. The longer the course the better. It should be over average ground (up and down hill) similar to that which is to be sketched and should be carefully measured. Walk this course both ways several times, counting strides with the pace tally. Take the average for this distance and from it find the number of strides to 1 mile. Say the

number of strides for 1 mile is 1,048. The scale of the sketch is to be 6 inches equals 1 mile, therefore 6 inches on the map will represent 1,048 of your strides. If you divide 6 by 1,048 you will have the scale length for one stride. It is too small a division to be useful, so multiply by 100 and find length for 100 strides is 0.57 inch. Pages 69 and 70 show working scales for the ordinary range of topographic sketches.

With a scale of equal parts (one reading inches and tenths will do) lay off as many divisions as you may desire in your scale. Each of the divisions will represent 100 of your strides. Divide the left division into 10 equal parts with your eye. Each of these will then be 10 of your strides. No smaller distance can be well measured off on your sketch.

#### SLOPE SCALES.

37. The alidade, as has been mentioned, in addition to the blank spaces for the individual stride scales, is provided with slope scales. (These are sometimes called *map distance* scales, which is confusing.) These scales are used in sketching, in connection with the clinometer, to find the differences in elevation between two points, the vertical angle from one to the other having been read by the clinometer.

The slope scales give results which are sufficiently accurate for sketching purposes. They are not reliable for angles greater than  $15^\circ$ .

Each interval on the slope scale represents the distance on the sketch (scale 6 inches to the mile) corresponding to a rise of 10 feet for the slope given. Working on a 6-inch scale, therefore, the method of determining the difference in elevation between two points is as follows: From the point of known elevation, read the slope to the point the elevation of which is to be determined. Say, it is  $3^\circ$ . Pace to the second point to find the distance and plot the distance. Look on your alidade for the slope scale of  $3^\circ$ . (The figure representing the slope is engraved at the midpoint of the interval for that slope.) Apply the slope interval for  $3^\circ$  to the plotted distance and find out how many times this interval is contained in the plotted distance. Multiply this number and fraction (there will usually be a fraction, which must, of course, be estimated) by 10 feet and the result is the difference in elevation. Similarly, for other clinometer readings, take the slope interval corresponding to the clinometer reading and find out how many times it is contained in the plotted distance, and then multiply by 10 feet.

38. This same slope scale may be used for any scale, providing that instead of multiplying the number of intervals and fractions thereof by 10, we multiply by the rise for that scale. The rise for any given scale is found by dividing 60 by the number of inches which represents the mile. For instance, the rise for a 3 inch to the mile scale is  $60/3$ , or 20 feet; for 4 inches to the mile scale it is  $60/4$ , or 15 feet; for  $\frac{1}{2}$  inch to the mile scale,  $60/\frac{1}{2}$ , or 120 feet. The method is the same, the slope scale is the same, no matter what the scale. The only thing that changes is the rise per interval, and this rise per interval is found as indicated above.

39. It will occur to the instructor or to some of the sketchers that to hunt around the alidade for the slope scale corresponding to a particular clinometer reading is rather a nuisance, and so it is.

This difficulty may be obviated by constructing "a scale of differences" and pasting it on the blank space of the alidade not used for the stride scale. It is constructed, marked, and used as follows:

On a suitable piece of paper lay off a line; on this line lay off several intervals equal to the 1-degree slope scale interval. These are about 0.65 inch each. Mark the division points, 10, 20, 30, 40, etc. Divide each interval into 10 parts (the 10-degree slope interval will do this about correctly), cut and paste on alidade. If working on a scale of 6 inches to the mile, this difference scale is used as follows: Read the vertical angle with the clinometer. Pace the distance. Plot the distance. Say the clinometer read  $1^\circ$  exactly; apply the "scale of differences" to the plotted distance between the points and read off directly the difference in elevation. If the clinometer read  $2\frac{1}{2}^\circ$ , apply the scale as before, but multiply the difference in elevation as secured directly (which is that for a  $1^\circ$  angle) by  $2\frac{1}{2}$  to secure the difference in elevation for a  $2\frac{1}{2}^\circ$  vertical angle. This same "scale of differences" may be used for any other scale in sketching by simply multiplying the result as above secured by the proper scale factor. The proper scale factor is found by dividing six by the number of inches to the mile in the scale being used. For a 3-inch scale, multiply by  $\frac{6}{3}$ , or 2; if working on a 2-inch scale, multiply by  $\frac{6}{2}$ , or 3. Such a scheme saves time and worry and is comparable in convenience to using a percentage clinometer and a per cent scale.

It will be seen that the method simply makes universal use of the 1-degree interval, instead of a different interval for each vertical angle. This is not too inaccurate for sketching use.

Of course, if using another scale than 6 inches to the mile for any considerable amount of work, the "scale of differences" can be remarked to correspond. That is, change the readings on scale by multiplying by 2 for a 3-inch scale, by 3 for a 2-inch scale, etc.

#### SERVICE CLINOMETER.

40. To use the clinometer, the observer sights the object through the peephole and, at the same time, sees the scale of degrees inside the rim. The red figures are minus (depression angles), the black ones plus (elevation angles) readings. The pendulum is allowed to swing freely by sliding back the bar and pressing the stop. The reading, is taken when the desired point is sighted and the pendulum has come to a rest. The pendulum should not be stopped to take the reading as this may displace the scale. It is best to rest the instrument or the hands holding it against a tree, fence, post, or other object while taking a reading. Theoretically the reading should be made to a point about the same height above the ground as the observer's eye. Actually this is very difficult to do and it is best to always read to the ground line and then, after ascertaining the difference in elevation, make allowance for the height of the eye above the ground. The clinometer should be tested occasionally as follows: Hold the instrument, stop uppermost, against a post or tree (point marked by a piece of paper pinned to it) and read to another point marked on another tree, 50 or 60 feet distant, and note the reading. Reverse this operation and read from the second mark back to the first one and note reading. For example, the first

reading is minus  $2^{\circ}$ , the reading back is plus  $1^{\circ}$ . Add the two readings and divide by 2 and you have the correct reading ( $1\frac{1}{2}^{\circ}$ ) of the slope between the two points. The clinometer then reads  $\frac{1}{2}^{\circ}$  too much on minus and  $\frac{1}{2}^{\circ}$  too little on plus readings. Reading must be corrected accordingly.

41. The sketching board is a simple board with a magnetic needle set in a trough in one edge. The needle is 3 inches long and quite sensitive. No plumb bob is provided, but a hole is accurately bored so that a plumb bob can be improvised and use made of the slope scale on the board in case the clinometer is lost. The plate on the back of the board is let in flush, so that the board can be turned freely on the tripod for orientation, and then firmly clamped by a slight turn of the tripod screw. As the tripod is not used in mounted work holes have been bored at the corners of the board for the insertion of a carrying cord if desired.

#### TO ORIENT THE BOARD BY COMPASS.

42. Set up the tripod with board loosely screwed onto it and level the board by eye by moving the tripod legs. Free the needle by turning the cam and then turn the board slowly around until the needle swings from side to side in the trough. Let the needle settle, turning the board as necessary so that the needle when settled lies directly along the north and south line (the median line of the trough). Without changing the position of the board reach under and tighten up the screw of the tripod. Care must always be taken not to turn the tripod screw too tight, as the threads are likely to be started by rough treatment. The board is now oriented. Draw a line parallel to the needle on the paper and mark the north end with a half arrow. Above this write M. M. or N. (magnetic meridian or north).

#### TO ORIENT THE BOARD BY BACK SIGHT.

43. Having plotted (located and drawn in) a station and arrived at a point farther on to which you have sighted and drawn a line, set up the tripod and board, measure off the number of strides taken between the two points on your line and stick a pin in the point found. This is your present position. Place your ruler against the pin and along the line between the two points and turn the board until the station you have just come from is sighted. Tighten up the tripod screw without moving the board and you are oriented. Verify this by reading the needle.

#### TO LOCATE A POINT BY TRAVERSING.

44. By this is meant measuring the distance between two points, by counting strides, or time or travel required to pass from one to the other. The term traverse is applied to the route followed by the sketcher in making the sketch. Being at point A (whose position is plotted on your sketch), with board oriented, stick a pin in point A on the sketch. Lay alidade alongside the pin and pivot it around until point B (the point to which you are to traverse) is sighted. Verify the position of the needle and then draw a ray toward B. Move to B, counting strides with pace tally, and upon arrival set up

the tripod, orienting roughly by a back sight on A. (Do not waste any time on this.) Lay a ruler along the ray, zero of scale of strides at A, and lay off on the ray the number of strides that your tally register shows was taken between the two points. The point marked is B.

#### TO LOCATE A POINT BY INTERSECTION.

45. Assume that from point A, with your board oriented, you took a careful sight and drew a ray toward a church a few hundred yards off to the side. After arriving at B and plotting its position, you carefully orient the board. Pivot the ruler around the pin in B until the church is sighted, then, verifying the position of the needle, draw a ray toward the church. The intersection of this ray and of the one you took from A is the sketch position of the church.

#### TO LOCATE BY RESECTION.

46. This is determining the sketcher's position (the reverse of intersection) by orienting the board and drawing rays toward himself from two or more points whose positions are already determined and plotted. Having previously plotted the position of points A and B, the sketcher comes into his area later, at some point from which those two points can be seen. His present position is not yet determined. To determine it, set up the board and carefully orient by compass, then stick pins in the sketch positions of A and B. Pivot the alidade on the sketch position of A, sight A, and draw a ray. Do the same with B. The intersection of the two lines is your position.

#### TO RESECT FROM THREE KNOWN POINTS.

47. In the previous paragraph a method of resection from two known points was given. For this a needle orientation is necessary. At times local attraction may deflect the needle and the three-point resection may be useful. The simplest method is by use of a transparent or translucent paper (celluloid will do splendidly). The process is as follows: Pin the paper on the board by thumb tacks. Stick a pin in it anywhere at a convenient point to represent your station (pay no attention to what may be on your sketch). Pivoting on the pin, draw, with great care, rays to each of three points which are in view and which also appear on your sketch. Lift the paper off the board. You have on it three rays, which make with each other the proper angles, considered from your position. All you need now to do is to put the tracing paper over your sketch, and by looking through to your sketch shift the paper until each ray passes through the sketch representative of the object to which this ray was drawn. As soon as each of the rays passes through its proper point (which will take a deal of fussing around the first time) you have it. Prick the point of intersection through to your sketch and the pinhole will give you your plotted position. This has been all done without orienting the board. If we wish to work from this station, the next step is to orient. This is done by back sighting to one of the three objects. Remember, this is but a cut-and-try method. It may take considerable time. It may help much at times.

## LESSON V.

48. The class by this time has progressed to the point where a great majority know what to look for in making an area sketch and know how to use all of their sketching instruments. It is now believed essential, at the risk of some repetition, for the instructor to give a special talk on the technique of the *sketcher's traverse*, the *detail* which should be shown on the sketch, and a few hints which may make for *clearness*.

## TECHNIQUE OF A SKETCHER'S TRAVERSE.

49. Set up the board at the point of beginning, station 1. Free the needle. Swing the board until the needle comes to a rest along the median line of the declinator trough. The board is now oriented. Clamp the board by tightening the screw holding the board to the tripod. The billiard-cloth covering of the tripod head will hold the board in position. Do not use an excess of force in clamping. Plot a point (use a pin to pivot on) on the paper to represent the point of beginning. Place the alidade on the board. Pivot it on the pin representing station 1. Sight along the line to be traversed to station 2. It is advisable where possible to sight on some well-defined object, as a tree, fence, corner, etc. This is necessary when the course from 1 to 2 is short. If the course is a long one, and follows a well-marked road or trail, a sight along the mid line or edge of the road will serve. Draw the ray. Pencil should have a chisel point and should be held vertically so that the pencil line will follow edge of alidade as closely as may be. *Always see that needle is along mid line of declinator trough when ray is drawn. Put in local data around station 1. Not necessary to draw rays to all points to be plotted. This fills up the sketch with lines. Point the alidade at object, and having ascertained the distance to it by pacing or by estimating plot the object in its proper place at once. Do not plot any points ahead of station 1 along the line of traverse. Draw rays to well-defined, easily identified distant objects, noting on the ray the object to which drawn.*

A ray to these same objects from another point on the traverse will serve to locate the objects, and once located they will serve as excellent checks upon orientation or may serve to locate the instrument by resection when for some reason or other the location is otherwise unknown. The tendency with the beginner is to draw rays to everything in sight. This is to be discouraged, as he loses much time in getting the rays—usually gets them confused so that all are useless—and seldom is he able to identify more than a very few of the objects so sighted. Read the clinometer, reading from station 1 to the objects sighted, noting the slope on the ray. Read the clinometer to station 2 last of all. Most texts tell you to sight at a point at station 2, which is the same distance above the ground as is your eye in taking the sight. It is much better to pick out a definite point to sight on. In other words, sight at the top of the chimney of a distant house, the lower window sill of a nearby house, the base of a tree, or, failing anything else, the ground line. Now, the slope you have read is the slope from your eye to the point sighted. You know the elevation of your eye. After getting the

difference in elevation between eye and object sighted this difference is added to or subtracted from the elevation of your eye and the result is the elevation of the object sighted. From this the elevation to the ground level at station 2 is found.

50. Set your pace tally to zero, pick up your equipment, and start off in the direction of station 2, walking with your customary step. Do not try to make your steps uniform. Walk naturally. Your scale should have been made to read double strides while you were walking naturally over country similar to that which you are to sketch. Press the pace tally every time your right foot strikes the ground, pace tally in your left hand. Whenever you reach an object which should appear on your sketch, as a house, bridge, stream line, ridge line, etc., do not take the time to set up and orient unless necessary. This will only be necessary when you wish to get a direction with care, as in the case of the direction of an important stream or ridge line. If the object is a house close to the roadside, it should be plotted in at once without set-up or orientation.

51. Arrived at station 2, set up. Scale off number of strides shown by your pace tally between stations 1 and 2 on ray already drawn. Mark station 2 by small circle with dot in center; elevation as soon as found beside the circle. To find elevation of 2. Sight back to 1 with clinometer. If reading is not the same as it was from 1 to 2, take the mean (providing of course line of sight is from ground to ground, or allowance has been made for elevation of eye in each case). Now hunt for the proper slope scale for the slope read. Apply the interval to the plotted distance from 1 to 2, to find the number of intervals and fractions thereof contained in the distance. Multiply this number by the rise per interval, 10 feet for 6-inch scale, 20 feet for 3-inch scale, etc. As soon as station 2 is plotted and its elevation found, orient board by compass and check by back sight. Then proceed as before. (The elevations of all points on the traverse between 1 and 2 should of course be noted as well as the elevation of the side shots taken. These are found in the same way as that of station 2.)

In plotting distances avoid as much as possible scaling off long lines by short plotted distances. In other words, keep track of the number of strides from the beginning point of a long tangent or slightly curving road and locate all stations on the tangent by scaling from the first point. This means that the pace tally is only set back to zero at a marked change of direction. Watch your pace tally to see that it does not fail to register.

#### DETAIL AND CLEARNESS.

52. The principal aim of the course so far has been to instruct the student officer in ground forms and the method of representing them on a map by contours. Every effort has been made to impress upon him and the instructor alike the necessity for viewing an *area of ground as a unit*; the necessity for *searching out the system of the topography* before minor matters are taken up.

In the sketching which has been done by the class, therefore, every effort has been made to *compel* each individual to *get around and through his area* so that he might pin down the *drainage system* if nothing else. Upon this rather inadequate framework he has been



compelled to draw in contours at very small vertical intervals. In putting in the troublesome contour lines he has very likely rubbed out roads, houses, most of his fences, and all of his trees. The resulting sketch is apt to be characterized more by its intense *blackness* than by its clearness and military value.

A military sketch must show the *essential military* features of the area and as many of the less important military and other features as the scale of the sketch and the skill of the sketcher make possible. Just what amount of detail should be shown on a sketch in any particular case is a matter of judgment. As one's skill in sketching and training in military tactics proceeds, his ability to determine these questions for himself will grow.

53. A sketch to be of value must be clear. The essential features must be brought out with bold strokes. Do not fill up the sketch with rude conventional signs for trees, grass, and corn. Do not fill it up with a mass of crowded contour lines. While the normal system requires 10-foot contours for a 6-inch scale, and 20-foot contours for a 3-inch scale, this system is not to be followed slavishly. If the country is so steep that 10-foot or 20-foot contours will crowd each other, use a larger interval.

Break contours at the railroads and *roads*, so that these important lines of communication will stand out. Break them at cliffs and write the words "cliff 60 feet high." Break them at streams and write "stream 50 feet wide, banks 40 feet high, unfordable except as indicated." Omit no important *landmarks*.

54. The user of the sketch must be able to locate himself on the sketch and for that reason landmarks must appear upon the sketch at frequent intervals (if they exist in fact). A tumbled-down shack in a sparsely-settled region, a group of cottonwood trees in a treeless waste, a waterhole in a semiarid country, a group of large buildings of a public or semipublic institution in the vicinity of a town will serve to help the user locate himself. A stone bridge may name a battlefield.

55. The conventional signs as adopted for use by all United States Government departments, as well as the special sketching signs given in the Field Service Regulations, follow paragraph 155. They must be learned.

56. At least three lesson periods must now be spent in sketching.

## LESSON VIII.

### MAP READING IN THE FIELD.

57. Map reading is essentially the reverse of map making. One who has been practiced in sketching by the plane-table method should have no difficulty in reading and using a large scale sketch of a small area. The essential features stand out almost at a glance. But a map of a large area of ground can not be read at a glance. It must be measured and studied in much the same way as the ground itself would have to be measured and studied before we become familiar with the country represented.

**Scale.**—As in making a sketch we need a "*working scale*," so in studying a map we need a "*reading scale*." It is not sufficient in *reading* a map for military purposes to glance at the scale given on

the map and then to glance at two points and guess at the distance between them. The *units* of distance most used in our service are the *yard* and the *mile*. It will be useful, therefore, to prepare our *reading scale* in yards or miles. Pages 67 and 68 give scales for the usual range of topographic maps.

58. **Examples.**—To prepare a *reading scale* of yards for a map on a scale of 1:80,000. Here 1 yard on the ground is represented by

$\frac{1}{80,000}$  of a yard on the map. 1,000 yards on the ground by  $\frac{1,000}{80,000} = \frac{1}{80}$  of a yard or  $36/80 = 0.45$  of an inch. Lay off a line 4.5 inches long and divide it into 10 parts and you have your scale. If a smaller unit than 1,000 yards is desired, divide the left unit into 10 equal parts.

59. To prepare a reading scale of miles for a map on a scale of 1:100,000. Here 1 mile on the ground is represented by  $\frac{1}{100,000}$  of a mile on the map. One mile is 5,280 feet, or 63,360 inches. Therefore the map representation of 1 mile on the ground is  $\frac{63,360}{100,000}$  or 0.634 of an inch. Lay off a line 6.34 inches long. It will represent 10 miles. Divide it into 10 equal parts and each part will represent 1 mile.

#### ORIENTATION AND DIRECTION.

60. To one who does not know his own position on the map or who does not hold it properly oriented when in use, a map is a hindrance rather than a help. One who is responsible for guiding troops by a map must keep his position on it by constant reference to the map. Too frequently in maneuvers, and even in actual war, is the map hidden away in a dispatch case. Then, after the column has already gone astray, frantic efforts are made by all concerned to recall the various textbook methods for orienting a map and for locating one's position upon the map.

#### PRACTICE WORK IN ORIENTATION.

61. It is useless to describe methods in a training manual unless the class is actually practiced in them. An indoor reading of the method of making a sketch or of orienting a map will do a beginner little good.

The following methods of orientation and resection should be tried out in the field by the class under the eye of the instructor:

*First method.*—Take a map of the training camp with the magnetic meridian marked upon it. Set up a sketching board on its tripod. Put the map on the board. Shift it until the magnetic meridian on the map becomes parallel to the meridian line of the needle trough. Pin the map down with thumb tacks. Orient the sketching board and resect from two points in view as described in paragraph 46.

*Second method.*—Using a compass, but not the sketching board. Lay the map on the ground. Lay the sight line of the compass along the magnetic meridian of the map. Rotate map and compass together until needle points north. If sight line of compass has

been kept along magnetic meridian of map, the map is oriented. Your location may be found by resecting as described in paragraph 46.

*Third method.*—No compass or no magnetic meridian. True meridian given; position unknown. Point the hour hand of your watch (held face upward) at the sun, if in the Northern Hemisphere. The line drawn from pivot to the point midway between the outer end of the hour hand and XII on the dial will point toward the south. Shift your map to correspond. This will give a very rough orientation. You may now be able to identify two or three distant points on the ground and their representations on the map. If you can do so, resect by the method explained in paragraph 46 or paragraph 47. Your resection will not be accurate, but it will serve to aid you in locating yourself.

62. While the last method is a good instruction method, there is no excuse in campaign for an officer not to have the magnetic meridian on his map. If the magnetic meridian is not shown on the map, ascertain the magnetic declination and draw the meridian on. The magnetic declination, it must be remembered, is the angle which the magnetic needle makes with the true north at the point. If the declination is east, it means that the north end of the needle settles to the east of true north. If west, the north end of the needle settles west. If the *magnetic declination* can not be readily ascertained, you can determine it approximately in the following manner:

#### DETERMINATION OF MAGNETIC DECLINATION.

63. In the explanation of this method, the term *magnetic azimuth* as here used is the horizontal angle from the north point of the *needle* measured *clockwise around the circle* to the *object sighted*. To read azimuths correctly, a box or pocket compass should be graduated *counter-clockwise*. If yours is not so graduated, better add a rough graduation in the counter-clockwise direction.

Observe the magnetic azimuth of the sun, a planet, or a bright star at *rising* and *setting* on the same day or at *setting* on one day and *rising* the next. Add these two azimuths together. Take the difference between this sum and  $360^\circ$ . One-half of this difference is the declination of your compass—*east*, if the *sum of the azimuths* is *less than*  $360^\circ$ ; *west*, if it is *greater*. In using this *method* the observations are best taken when the object is *just above the true horizon*, or at a *gradient of zero*. This can usually be done if a high point is chosen for observation. *If this can not be done*, be careful to take both observations with the object *at the same gradient* (as determined with clinometer). *This is most important with the sun*. Under the least favorable conditions an inequality of  $1^\circ$  in the gradients at the time of observation on the sun may introduce an error of  $\frac{1}{2}^\circ$  in the result.

In using a star, choose one which rises nearly east from the point of observation. If this be done the inequality of a degree in the gradients will be immaterial. Both observations need not be made at the same point, but should not be more than 10 miles apart in east and west or north and south directions. (See also par. 68.)

## LESSON IX.

## DAY GUIDING BY MAP AND COMPASS.

64. The following condensed quotation from a recent supplement to the British Manual of Map Reading and Sketching is taken from the International Military Digest, March, 1916:

After mastering the *conventional signs*, map reading is only a matter of observation and *common sense*, a fact which leads people to underestimate its difficulty and the need for *continual practice*.

When finding the way by road, it is important to consider the *time factor* in attempting to identify points of the road in advance, and *not place sole reliance* upon *cross-roads*, or *side roads*, etc., which may have changed since the map was published. The speed of march may be obtained from a speedometer or by a rough approximation of the marching rate of the column. \* \* \*

Orienting the map by pointing at the sun [a common textbook method and at times a valuable one] may lead to an error in the direction of as much as 7° or 8°. Therefore, some *permanent point*, as a *church steeple* or a *straight piece of road*, should be sighted on.

When a *point of the country* has been identified on the map, time often will be saved by using it as a *reference point* in referring to others. Such points may be noted as *so many degrees* from it, or in line with it, or just to the right or left. A protractor will assist in laying off angles and measuring bearings on the map.

On a small-scale map many details are not shown, but much may be inferred from what is shown.

In *night movements practice* is *essential*, and although it is not difficult to march by compass bearing, much assistance can be obtained by the ability to recognize a *few stars in different parts of the heavens*.

65. After the remarks given above have been discussed, the instructor should practice the members of the class in following a course along roads and across country from the map. In order that this practice may not be done in a perfunctory manner, it is desirable to require the student officers to traverse a course outlined by the instructor, and note on the map all features which may be altered. If the map is so nearly correct that this method is impracticable, flags bearing special numbers may be erected along the course and the student officers required to locate the flags on their sheets. It will be particularly good practice if a group of flags representing a trench are so located that they can be found only by following a compass bearing across country for a distance of several miles.

Such practice will convince all of the great difficulties in guiding by compass alone. A judicious use of the map and of prominent physical features will simplify the matter in open country.

Before starting, the course should be carefully protracted onto the map and note taken of the *prominent physical features through which* or *near which* the line passes. Before starting, identify one of these points on the ground and march on it. If you must descend into a valley to lose sight of the feature, take some point in the valley which is in line to march on. Thus, continue from feature to feature. In close country this is not so simple. Here it may be necessary for you to actually plot on your map, or an enlargement of it, your course as you go. Make your courses as long as possible.

## LESSON X.

## NIGHT GUIDING BY MAP, STAR, AND COMPASS.

## 66. The following is taken from the Artillery Journal:

As an aeronaut in Ladysmith, I had plenty of opportunities of foreseeing the great power aeronautics would have in warfare in the future, and that most of the effective fighting would be done at night.

At that time the regulations described night operations as extremely hazardous, and warned the commander who undertook such operations that he did so at his own peril and was responsible for the results. Various expedients were suggested to enable the troops to keep their directions, such as that the route should be previously reconnoitered and marked by tins, pieces of paper, and other devices; but how the reconnoitering party was ever to carry out this operation nobody has yet been able to understand. We found the *colonials* never required this artificial help, and could move about on a *starlit night* as easily as in *daylight* and as fast as the nature of the ground permitted, \* \* \* and ascertained from various *colonials*, Basutos, Indians, and Arabs that they could instinctively read the heavens as a *compass*, this knowledge having been transmitted from father to son for generations. \* \* \*

Although the system was only perfected in June, 1915, *soldiers* of all ranks have begun to realize the simplicity and wonderful utility of being able to read the *universal compass*, the *heavens*, and we begin to hear how useful this knowledge has been found for guiding supporting troops up to the first-line trenches, etc.

The heavens can not go wrong, and on a starlit night you can rely absolutely upon them to take you to your destination, *once you grasp* the rudiments of the system; you only *require* to know three or four first magnitude stars, for their exact position is given for every hour of the night in *Marching and Flying without a Compass* (Tilney, Lieutenant colonel, F. R. C. S.)

## TO FIND THE STARS.

67. *The Dipper and Cassiopeia*.—The star plans given here, and parts of the descriptions, are taken from *The Star Pocket Book* by Capt. Weatherhead, British Royal Navy.

*Ursa Major* (called the Big Dipper), shown in the upper portion of Figure IX, is the most important of the constellations. It is at once the easiest to distinguish, the easiest to find the North Star by, and the best *starting point* from which to learn the other stars. The "Pointers"  $\alpha$  and  $\beta$  point to *Polaris* (the North Star) at all times as the Dipper circles the Pole. On the opposite side of *Polaris* and at about the same distance from it is the constellation of *Cassiopeia*. Its form is that of the letter W.

The great importance which attaches to *Polaris* (the North Star) is that it is never more than  $2^\circ$  away from the point where the axis of the earth if extended would pierce the heavens. It therefore appears to the eye to be always in the same place, and it is, except for a maximum variation of about  $2^\circ$ .

68. As the *latitude* of any place is equal to the *altitude* of the Pole, when the Dipper and *Cassiopeia* are on either side of the North Star (east and west), the elevation of the North Star will give a reasonably correct figure for the latitude of the place of observation. When the Dipper and *Cassiopeia* are above or below the North Star, a compass reading to the North Star will give the *declination* of your *compass* to within the *least reading* of your *compass*.

69. *Arcturus, Spica, Denebola*.—The lower half of Figure IX shows the *Big Dipper* again. By continuing the sweep of the *Dipper handle*, you will find the bright star *Arcturus* about  $30^\circ$  from the end of the handle. Continue on with the curve and you will find *Spica* about  $30^\circ$  farther on.

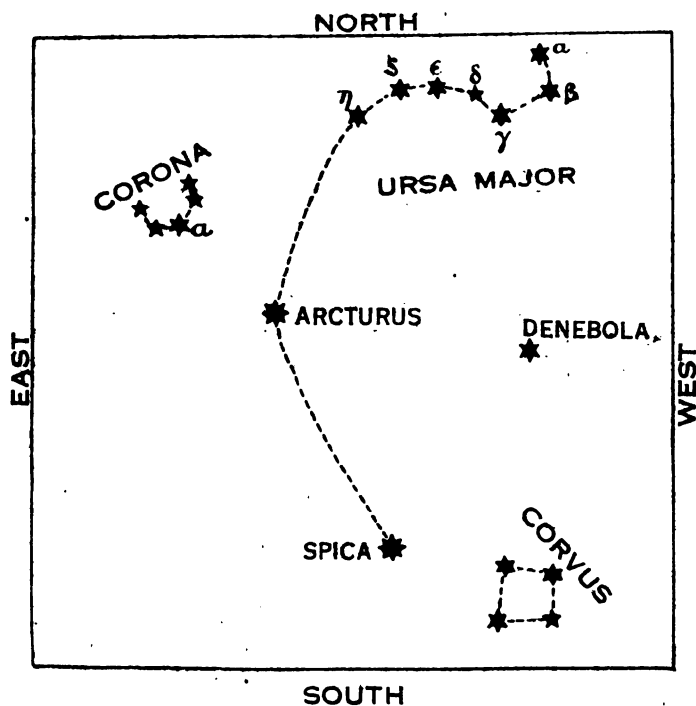
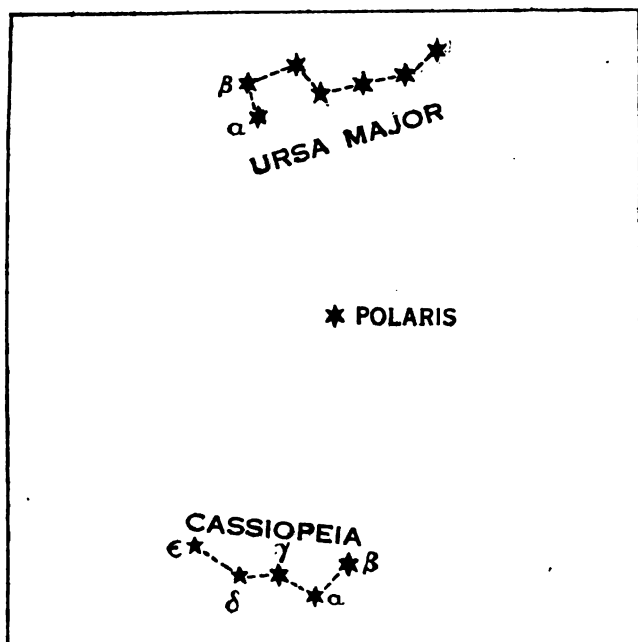


FIGURE IX

Arcturus has a good marker near it in the semicircle of stars called the *Northern Crown*, and *Spica* has the kite-shaped quadrilateral *Corvus*.

*Denebola* forms with *Arcturus* and *Spica* an equilateral triangle.

70. As an additional aid in finding these first three important single stars, it is pointed out that if a *star* is to be found at a *certain place* in the heavens at a *certain hour* on a *certain night*, it will be found in that *same place* the *next night about four minutes earlier* and on the next *four minutes earlier still*, or at the end of a month in that same place about *two hours* earlier, and so on for each successive month. Now, the "Pointers" ( $\alpha$  and  $\beta$  of the Big Dipper) are to be found high on the meridian at midnight on March 7 any year. At this time *Denebola* will also be near the meridian (a little to the east) and in the south. Follow the sweep of the Dipper handle and high up in the heavens almost to our east will be Arcturus, with *Spica* still on the sweep of the handle in the southeast, completing the equilateral triangle.

71. Hold the chart directly above your head, north to north, west to west, etc., and you should have no trouble in finding these stars. Remember the stars are to be found in this portion of the heavens and as stated at 10 o'clock on April 7, at 8 o'clock on May 7, etc. After May 7, therefore, we may expect to find them getting lower and lower in the western heavens as the summer advances until September, when the Dipper is to be found low down under the Pole; *Denebola* and *Spica* will have set before night comes on.

72. In looking for the stars during the *summer months*, therefore, face the west and hold the chart in front of you, north to the north and east side up. See table in paragraph 77 for the date on which *Arcturus*, *Spica*, and *Denebola* transit at *midnight*.

73. *Vega*, *Altair*, and *Deneb*.—The upper half of Figure X shows the Dipper once more and the important stars *Vega*, *Altair*, and  $\alpha$  Cygnus (also called *Deneb*).

*Vega* is to be found on the meridian at midnight July 1, *Altair* July 19, and *Deneb* August 2. They all, therefore, transit within about two hours of each other. There should be no difficulty in finding the T of Cygnus and from it *Altair*, and then *Vega*, which is on a line with *Altair* and its two accompanying stars.

In the early summer months, in the hours before midnight, we will find these stars in the eastern heavens. In the fall we will look for them in the west.

74. *Perseus*, *Andromeda*, the *Great Square*, and *Pleiades*.—In line with the "Pointers" on the other side of the North Star, and beyond Cassiopeia about as far as it is beyond the North Star, we find  $\alpha$  and  $\beta$  of Pegasus. These five stars are all on a line (great circle), and all cross the meridian together, but, of course, when the *Big Dipper* is high in the heavens, *Pegasus* being on the other side of the Pole is out of sight in ordinary latitudes. When Pegasus is high in the heavens, the Dipper is below the North Star. It is to be expected, then, that  $\alpha$  and  $\beta$  Pegasi will be on the meridian at midnight on September 7, just *six months* after the "Pointers" made their *upper transit at midnight* and on the *same night* as they make their *lower transit at midnight*.

The stars on these charts, therefore, are to be looked for in the early hours of the summer evening in the east; high in the heavens in the early fall; and in the west along Christmas time.

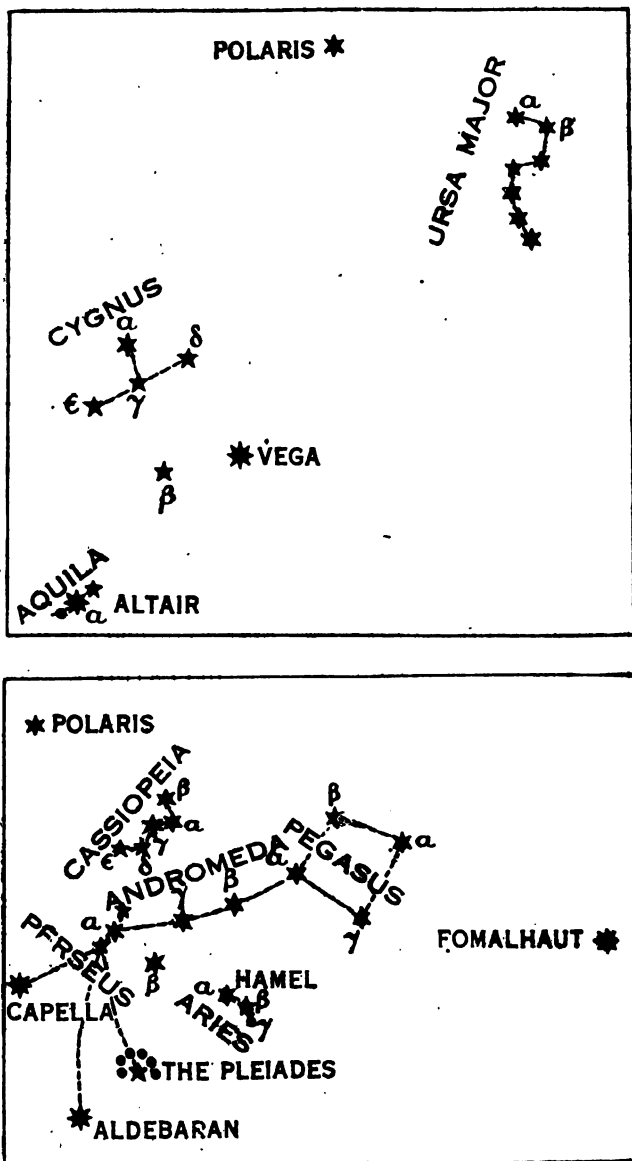


FIGURE X

75.  $\alpha$  and  $\beta$  Pegasi point directly at Fomalhaut, which, therefore, also crosses the meridian at midnight on September 7. These three stars form as perfect a set of pointers to the Pole as do the "Pointers



of the Dipper and may be of great use, therefore, when the pointers, low in the heavens, are obscured by clouds.

76. *Capella, Aldebaran, Castor, and Pollux* (Fig. XI).—Aldebaran is to be found on the meridian at midnight of November 29, Capella on December 9, Castor on January 13 and Pollux on January 16. In the fall months and early winter we will find them in the east in the hours before midnight and in the west in the later winter months. A

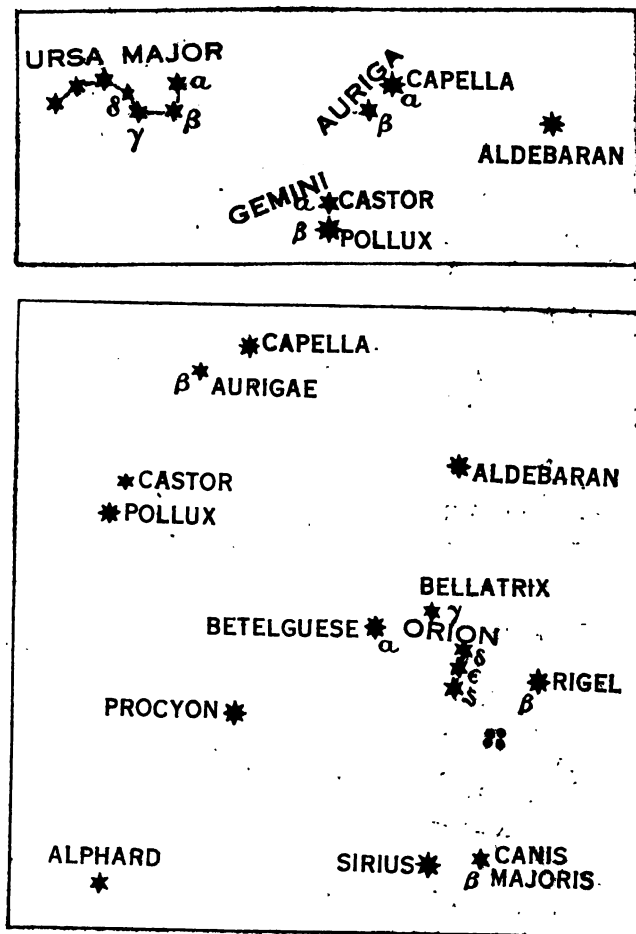


FIGURE XI

line drawn from the pole star perpendicular to the line from the "Pointers" passes through Capella. This line also passes directly through *Rigel*, a bright star in the constellation of Orion. These two stars, therefore, cross the meridian together and form another excellent set of north pointers.

The group of stars in the constellation of Orion are particularly brilliant, perhaps the most conspicuous of all star groups in the

winter heavens. Rigel, the stars in the belt of Orion, Bellatrix, and Betelgeuse are very near the celestial equator. Betelgeuse and  $\alpha$  Aurigae transit together as do Rigel and Capella. We therefore have in the winter this double line running from the vicinity of Orion to the North Star.

*Sirius*, the brightest star in the heavens, is practically in line with the belt of Orion and also in line and about equidistant from the belt is Aldebaran.

77. *Date of midnight transit and declination of stars* shown in Figures IX-XI.

| Date.           | Declina-<br>tion. | Star.     | Date.            | Declina-<br>tion. | Star.       |
|-----------------|-------------------|-----------|------------------|-------------------|-------------|
| January 1.....  | 16.5° S..         | Sirius.   | July 19.....     | 8.5° N..          | Altair.     |
| January 13..... | .....             | Castor.   | August 2.....    | 45.0° N..         | Deneb.      |
| January 15..... | 5.5° N..          | Procyon.  | September 5..... | 30.0° S..         | Fomalhaut.  |
| January 16..... | 28.0° N..         | Pollux.   | October 22.....  | 23.0° N..         | Hamel.      |
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78. The time of transit for any other night may be found approximately from the rule that the star transits four minutes earlier each successive night, about two hours each successive month, or 24 hours earlier (same date) at the end of the year.

79. The declination of a star is its angle, measured in the meridian from the equator. The latitude of a place on the earth is its angle measured in the meridian from the equator. Both are noted as north if north of equator, or south if south of equator. If the declination of a star is greater than the latitude of a place, it will pass the meridian to the north of the place. If less, it will pass the meridian to the south. Of course, if the declination is south and the latitude north, the star will always be to the south, and similarly, if the north declination of star is small and the latitude of the place high.

It is evident from the foregoing that by use of the additional sets of north-pointing stars, and with a little practice in studying the times of the year and hours of the nights when certain stars are to be found in the meridian to the north or south of us, we should seldom have any difficulty in knowing approximately at least our points of the compass.

If headquarters have, as we understand they have in France, tables from which the true azimuth of a star can be predicted for any hour of the day, and if orders based on these tables are to be issued, we must know the prominent stars. To learn them requires observation and practice, nothing else.

## LESSON XI.

### USE OF MAPS IN POSITION WARFARE.

80. The following condensed quotation from an article in the *British Journal Royal Artillery* is taken from the *International Military Digest*:

Now that large-scale maps, such as 1:20,000 or 1:10,000, are used extensively by batteries in the field, map reading has become an important part of an officer's

compelled to draw in contours at very small vertical intervals. In putting in the troublesome contour lines he has very likely rubbed out roads, houses, most of his fences, and all of his trees. The resulting sketch is apt to be characterized more by its intense *blackness* than by its clearness and military value.

A military sketch must show the *essential military* features of the area and as many of the less important military and other features as the scale of the sketch and the skill of the sketcher make possible. Just what amount of detail should be shown on a sketch in any particular case is a matter of judgment. As one's skill in sketching and training in military tactics proceeds, his ability to determine these questions for himself will grow.

53. A sketch to be of value must be clear. The essential features must be brought out with bold strokes. Do not fill up the sketch with rude conventional signs for trees, grass, and corn. Do not fill it up with a mass of crowded contour lines. While the normal system requires 10-foot contours for a 6-inch scale, and 20-foot contours for a 3-inch scale, this system is not to be followed slavishly. If the country is so steep that 10-foot or 20-foot contours will crowd each other, use a larger interval.

Break contours at the railroads and *roads*, so that these important lines of communication will stand out. Break them at cliffs and write the words "cliff 60 feet high." Break them at streams and write "stream 50 feet wide, banks 40 feet high, unfordable except as indicated." Omit no important *landmarks*.

54. The user of the sketch must be able to locate himself on the sketch and for that reason landmarks must appear upon the sketch at frequent intervals (if they exist in fact). A tumbled-down shack in a sparsely-settled region, a group of cottonwood trees in a treeless waste, a waterhole in a semiarid country, a group of large buildings of a public or semipublic institution in the vicinity of a town will serve to help the user locate himself. A stone bridge may name a battlefield.

55. The conventional signs as adopted for use by all United States Government departments, as well as the special sketching signs given in the Field Service Regulations, follow paragraph 155. They must be learned.

56. At least three lesson periods must now be spent in sketching.

## LESSON VIII.

### MAP READING IN THE FIELD.

57. Map reading is essentially the reverse of map making. One who has been practiced in sketching by the plane-table method should have no difficulty in reading and using a large scale sketch of a small area. The essential features stand out almost at a glance. But a map of a large area of ground can not be read at a glance. It must be measured and studied in much the same way as the ground itself would have to be measured and studied before we become familiar with the country represented.

Scale.—As in making a sketch we need a "*working scale*," so in studying a map we need a "*reading scale*." It is not sufficient in *reading* a map for military purposes to glance at the scale given on

the map and then to glance at two points and guess at the distance between them. The *units* of distance most used in our service are the *yard* and the *mile*. It will be useful, therefore, to prepare our *reading scale* in yards or miles. Pages 67 and 68 give scales for the usual range of topographic maps.

58. **Examples.**—To prepare a *reading scale* of *yards* for a map on a scale of 1:80,000. Here 1 yard on the ground is represented by  $\frac{1}{80,000}$  of a yard on the map. 1,000 yards on the ground by  $\frac{1,000}{80,000} = \frac{1}{80}$  of a yard or  $\frac{36}{80} = 0.45$  of an inch. Lay off a line 4.5 inches long and divide it into 10 parts and you have your scale. If a smaller unit than 1,000 yards is desired, divide the left unit into 10 equal parts.

59. To prepare a reading scale of miles for a map on a scale of 1:100,000. Here 1 mile on the ground is represented by  $\frac{1}{100,000}$  of a mile on the map. One mile is 5,280 feet, or 63,360 inches. Therefore the map representation of 1 mile on the ground is  $\frac{63,360}{100,000}$  or 0.634 of an inch. Lay off a line 6.34 inches long. It will represent 10 miles. Divide it into 10 equal parts and each part will represent 1 mile.

#### ORIENTATION AND DIRECTION.

60. To one who does not know his own position on the map or who does not hold it properly oriented when in use, a map is a hindrance rather than a help. One who is responsible for guiding troops by a map must keep his position on it by constant reference to the map. Too frequently in maneuvers, and even in actual war, is the map hidden away in a dispatch case. Then, after the column has already gone astray, frantic efforts are made by all concerned to recall the various textbook methods for orienting a map and for locating one's position upon the map.

#### PRACTICE WORK IN ORIENTATION.

61. It is useless to describe methods in a training manual unless the class is actually practiced in them. An indoor reading of the method of making a sketch or of orienting a map will do a beginner little good.

The following methods of orientation and resection should be tried out in the field by the class under the eye of the instructor:

*First method.*—Take a map of the training camp with the magnetic meridian marked upon it. Set up a sketching board on its tripod. Put the map on the board. Shift it until the magnetic meridian on the map becomes parallel to the meridian line of the needle trough. Pin the map down with thumb tacks. Orient the sketching board and resect from two points in view as described in paragraph 46.

*Second method.*—Using a compass, but not the sketching board. Lay the map on the ground. Lay the sight line of the compass along the magnetic meridian of the map. Rotate map and compass together until needle points north. If sight line of compass has

been kept along magnetic meridian of map, the map is oriented. Your location may be found by resecting as described in paragraph 46.

*Third method.*—No compass or no magnetic meridian. True meridian given; position unknown. Point the hour hand of your watch (held face upward) at the sun, if in the Northern Hemisphere. The line drawn from pivot to the point midway between the outer end of the hour hand and XII on the dial will point toward the south. Shift your map to correspond. This will give a very rough orientation. You may now be able to identify two or three distant points on the ground and their representations on the map. If you can do so, resect by the method explained in paragraph 46 or paragraph 47. Your resection will not be accurate, but it will serve to aid you in locating yourself.

62. While the last method is a good instruction method, there is no excuse in campaign for an officer not to have the magnetic meridian on his map. If the magnetic meridian is not shown on the map, ascertain the magnetic declination and draw the meridian on. The magnetic declination, it must be remembered, is the angle which the magnetic needle makes with the true north at the point. If the declination is east, it means that the north end of the needle settles to the east of true north. If west, the north end of the needle settles west. If the *magnetic declination* can not be readily ascertained, you can determine it approximately in the following manner:

#### DETERMINATION OF MAGNETIC DECLINATION.

63. In the explanation of this method, the term *magnetic azimuth* as here used is the horizontal angle from the north point of the *needle* measured *clockwise around the circle* to the *object sighted*. To read azimuths correctly, a box or pocket compass should be graduated *counter-clockwise*. If yours is not so graduated, better add a rough graduation in the counter-clockwise direction.

Observe the magnetic azimuth of the sun, a planet, or a bright star at *rising* and *setting* on the same day or at *setting* on one day and *rising* the next. Add these two azimuths together. Take the difference between this sum and  $360^\circ$ . One-half of this difference is the declination of your compass—*east*, if the *sum* of the *azimuths* is *less* than  $360^\circ$ ; *west*, if it is *greater*. In using this *method* the observations are best taken when the object is *just above the true horizon*, or at a *gradient of zero*. This can usually be done if a high point is chosen for observation. *If this can not be done*, be careful to take both observations with the object *at the same gradient* (as determined with clinometer). *This is most important with the sun*. Under the least favorable conditions an inequality of  $1^\circ$  in the gradients at the time of observation on the sun may introduce an error of  $\frac{1}{2}^\circ$  in the result.

In using a star, choose one which rises nearly east from the point of observation. If this be done the inequality of a degree in the gradients will be immaterial. Both observations need not be made at the same point, but should not be more than 10 miles apart in east and west or north and south directions. (See also par. 68.)

## LESSON IX.

## DAY GUIDING BY MAP AND COMPASS.

64. The following condensed quotation from a recent supplement to the British Manual of Map Reading and Sketching is taken from the International Military Digest, March, 1916:

After mastering the *conventional signs*, map reading is only a matter of observation and *common sense*, a fact which leads people to underestimate its difficulty and the need for *continual practice*.

When finding the way by road, it is important to consider the *time factor* in attempting to identify points of the road in advance, and *not place sole reliance* upon *cross-roads*, or *side roads*, etc., which may have changed since the map was published. The speed of march may be obtained from a speedometer or by a rough approximation of the marching rate of the column. \* \* \*

Orienting the map by pointing at the sun [a common textbook method and at times a valuable one] may lead to an error in the direction of as much as  $7^{\circ}$  or  $8^{\circ}$ . Therefore, some *permanent point*, as a *church steeple* or a *straight piece of road*, should be sighted on.

When a *point of the country* has been identified on the map, time often will be saved by using it as a *reference point* in referring to others. Such points may be noted as so many *degrees* from it, or in line with it, or just to the right or left. A protractor will assist in laying off angles and measuring bearings on the map.

On a small-scale map many details are not shown, but much may be inferred from what is shown.

In *night movements practice* is *essential*, and although it is not difficult to march by compass bearing, much assistance can be obtained by the ability to recognize a *few stars in different parts of the heavens*.

65. After the remarks given above have been discussed, the instructor should practice the members of the class in following a course along roads and across country from the map. In order that this practice may not be done in a perfunctory manner, it is desirable to require the student officers to traverse a course outlined by the instructor, and note on the map all features which may be altered. If the map is so nearly correct that this method is impracticable, flags bearing special numbers may be erected along the course and the student officers required to locate the flags on their sheets. It will be particularly good practice if a group of flags representing a trench are so located that they can be found only by following a compass bearing across country for a distance of several miles.

Such practice will convince all of the great difficulties in guiding by compass alone. A judicious use of the map and of prominent physical features will simplify the matter in open country.

Before starting, the course should be carefully protracted onto the map and note taken of the *prominent physical features through which or near which* the line passes. Before starting, identify one of these points on the ground and march on it. If you must descend into a valley to lose sight of the feature, take some point in the valley which is in line to march on. Thus, continue from feature to feature. In close country this is not so simple. Here it may be necessary for you to actually plot on your map, or an enlargement of it, your course as you go. Make your courses as long as possible.

## LESSON X.

## NIGHT GUIDING BY MAP, STAR, AND COMPASS.

## 66. The following is taken from the Artillery Journal:

As an aeronaut in Ladysmith, I had plenty of opportunities of foreseeing the great power aeronautics would have in warfare in the future, and that most of the effective fighting would be done at night.

At that time the regulations described night operations as extremely hazardous, and warned the commander who undertook such operations that he did so at his own peril and was responsible for the results. Various expedients were suggested to enable the troops to keep their directions, such as that the route should be previously reconnoitered and marked by tins, pieces of paper, and other devices; but how the reconnoitering party was ever to carry out this operation nobody has yet been able to understand. We found the *colonials* never required this artificial help, and could move about on a *starlit night* as easily as in *daylight* and as fast as the nature of the ground permitted, \* \* \* and ascertained from various *colonials*, *Basutos*, *Indians*, and *Arabs* that they could instinctively *read the heavens* as a *compass*, this knowledge having been transmitted from father to son for generations. \* \* \*

Although the system was only perfected in June, 1915, *soldiers* of all ranks have begun to realize the simplicity and wonderful utility of being able to read the *universal compass*, the *heavens*, and we begin to hear how useful this knowledge has been found for guiding supporting troops up to the first-line trenches, etc.

The heavens can not go wrong, and on a *starlit night* you can rely absolutely upon them to take you to your destination, *once you grasp* the rudiments of the system; you only *require* to know three or four first magnitude stars, for their exact position is given for every hour of the night in *Marching and Flying without a Compass* (Tilney, lieutenant colonel, F. R. C. S.)

## TO FIND THE STARS.

67. *The Dipper and Cassiopeia*.—The star plans given here, and parts of the descriptions, are taken from *The Star Pocket Book* by Capt. Weatherhead, British Royal Navy.

*Ursa Major* (called the Big Dipper), shown in the upper portion of Figure IX, is the most important of the constellations. It is at once the easiest to distinguish, the easiest to find the North Star by, and the best *starting point* from which to learn the other stars. The "Pointers"  $\alpha$  and  $\beta$  point to *Polaris* (the North Star) at all times as the Dipper circles the Pole. On the opposite side of *Polaris* and at about the same distance from it is the constellation of *Cassiopeia*. Its form is that of the letter W.

The great importance which attaches to *Polaris* (the North Star) is that it is never more than  $2^\circ$  away from the point where the axis of the earth if extended would pierce the heavens. It therefore appears to the eye to be always in the same place, and it is, except for a maximum variation of about  $2^\circ$ .

68. As the *latitude* of any place is equal to the *altitude* of the Pole, when the Dipper and *Cassiopeia* are on either side of the North Star (east and west), the elevation of the North Star will give a reasonably correct figure for the latitude of the place of observation. When the Dipper and *Cassiopeia* are above or below the North Star, a compass reading to the North Star will give the *declination* of your compass to within the least reading of your compass.

69. *Arcturus, Spica, Denebola*.—The lower half of Figure IX shows *Big Dipper* again. By continuing the sweep of the *Dipper handle*, you will find the bright star *Arcturus* about  $30^\circ$  from the end of the handle. Continue on with the curve and you will find *Spica* about farther on.

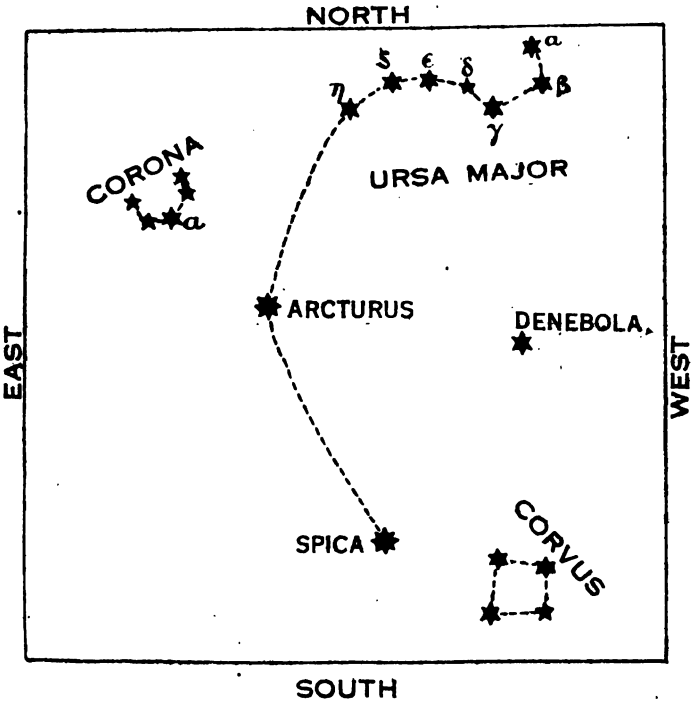
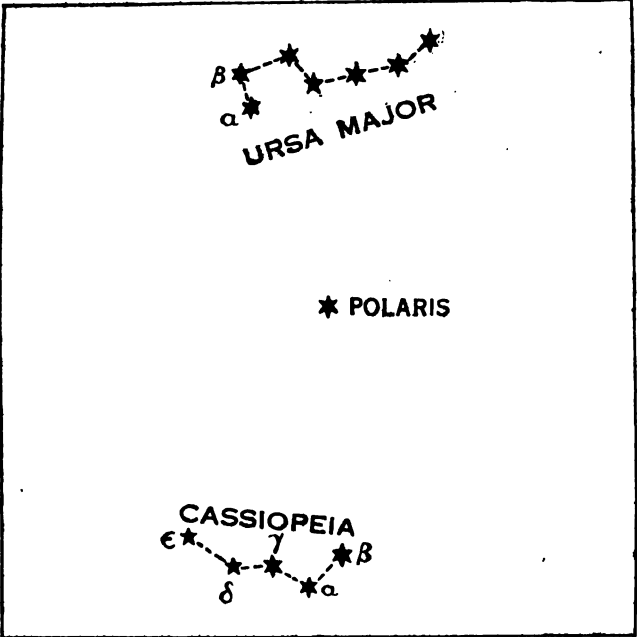


FIGURE IX



Arcturus has a good marker near it in the semicircle of stars called the *Northern Crown*, and *Spica* has the kite-shaped quadrilateral *Corvus*.

*Denebola* forms with *Arcturus* and *Spica* an equilateral triangle.

70. As an additional aid in finding these first three important single stars, it is pointed out that if a *star* is to be found at a *certain place* in the heavens at a *certain hour* on a *certain night*, it will be found in that *same place* the *next night about four minutes earlier* and on the next *four minutes earlier still*, or at the end of a month in that same place about *two hours* earlier, and so on for each successive month. Now, the "Pointers" ( $\alpha$  and  $\beta$  of the Big Dipper) are to be found high on the meridian at midnight on March 7 any year. At this time *Denebola* will also be near the meridian (a little to the east) and in the south. Follow the sweep of the Dipper handle and high up in the heavens almost to our east will be *Arcturus*, with *Spica* still on the sweep of the handle in the southeast, completing the equilateral triangle.

71. Hold the chart directly above your head, north to north, west to west, etc., and you should have no trouble in finding these stars. Remember the stars are to be found in this portion of the heavens and as stated at 10 o'clock on April 7, at 8 o'clock on May 7, etc. After May 7, therefore, we may expect to find them getting lower and lower in the western heavens as the summer advances until September, when the Dipper is to be found low down under the Pole; *Denebola* and *Spica* will have set before night comes on.

72. In looking for the stars during the *summer months*, therefore, face the west and hold the chart in front of you, north to the north and *east side up*. See table in paragraph 77 for the date on which *Arcturus*, *Spica*, and *Denebola* transit at *midnight*.

73. *Vega*, *Altair*, and *Deneb*.—The upper half of Figure X shows the Dipper once more and the important stars *Vega*, *Altair*, and  $\alpha$  Cygnus (also called *Deneb*).

*Vega* is to be found on the meridian at midnight July 1, *Altair* July 19, and *Deneb* August 2. They all, therefore, transit within about two hours of each other. There should be no difficulty in finding the T of Cygnus and from it *Altair*, and then *Vega*, which is on a line with *Altair* and its two accompanying stars.

In the early summer months, in the hours before midnight, we will find these stars in the eastern heavens. In the fall we will look for them in the west.

74. *Perseus*, *Andromeda*, the *Great Square*, and *Pleiades*.—In line with the "Pointers" on the other side of the North Star, and beyond Cassiopeia about as far as it is beyond the North Star, we find  $\alpha$  and  $\beta$  of Pegasus. These five stars are all on a line (great circle), and all cross the meridian together, but, of course, when the *Big Dipper* is high in the heavens, *Pegasus* being on the other side of the Pole is out of sight in ordinary latitudes. When *Pegasus* is high in the heavens, the Dipper is below the North Star. It is to be expected, then, that  $\alpha$  and  $\beta$  Pegasi will be on the meridian at midnight on September 7, just *six months* after the "Pointers" made their *upper transit at midnight* and on the *same night* as they make their *lower transit at midnight*.

The stars on these charts, therefore, are to be looked for in the early hours of the summer evening in the east; high in the heavens in the early fall; and in the west along Christmas time.

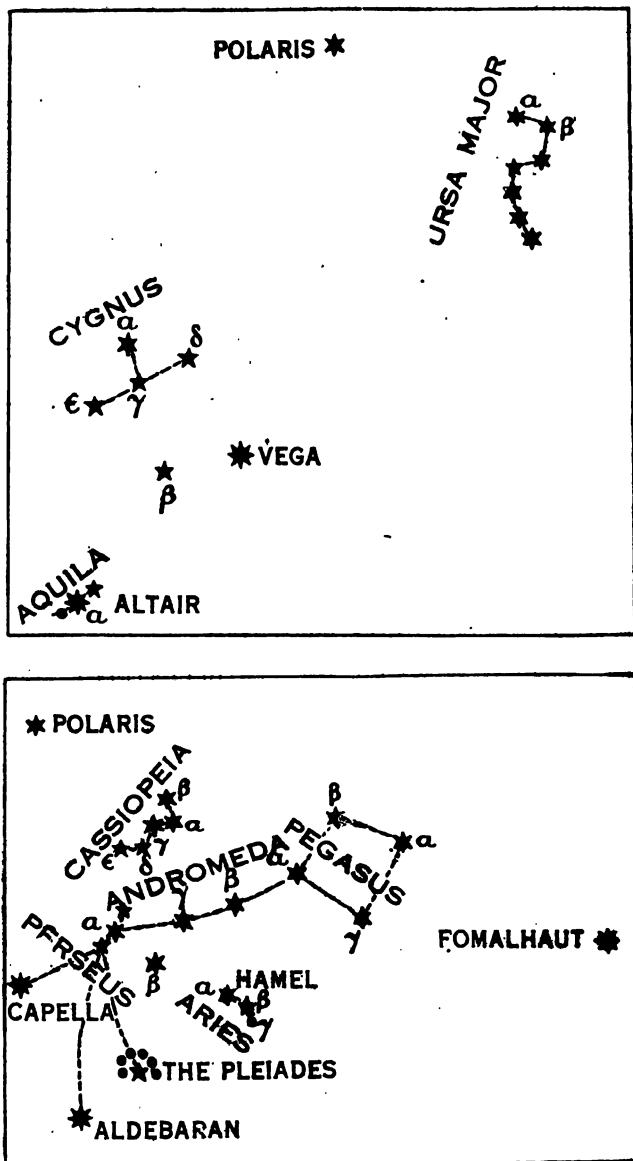


FIGURE X

75.  $\alpha$  and  $\beta$  Pegasi point directly at Fomalhaut, which, therefore, also crosses the meridian at midnight on September 7. These three stars form as perfect a set of pointers to the Pole as do the "Pointers

of the Dipper and may be of great use, therefore, when the pointers, low in the heavens, are obscured by clouds.

76. *Capella, Aldebaran, Castor, and Pollux* (Fig. XI).—Aldebaran is to be found on the meridian at midnight of November 29, Capella on December 9, Castor on January 13 and Pollux on January 16. In the fall months and early winter we will find them in the east in the hours before midnight and in the west in the later winter months. A

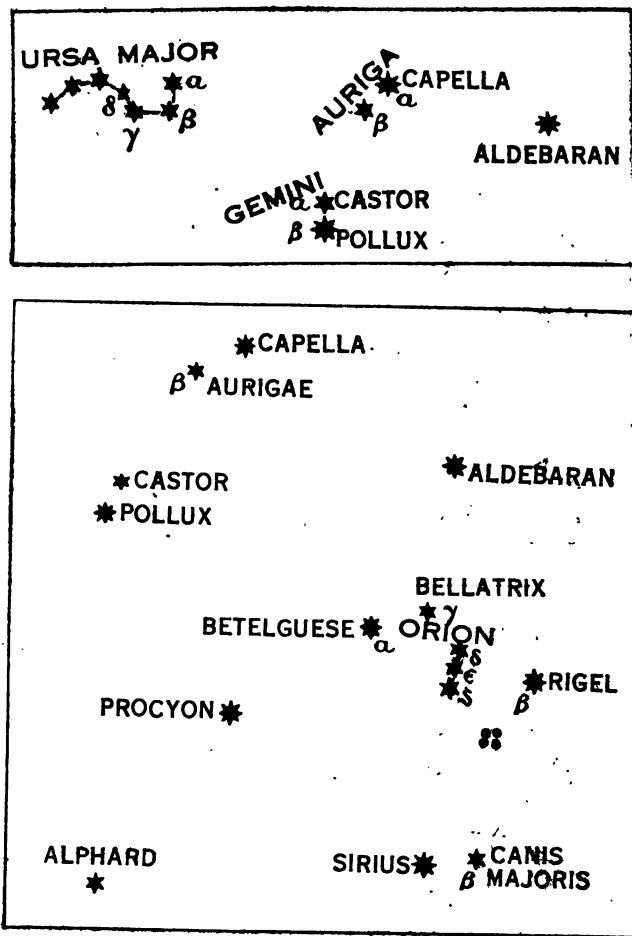


FIGURE XI

line drawn from the pole star perpendicular to the line from the "Pointers" passes through Capella. This line also passes directly through Rigel, a bright star in the constellation of Orion. These two stars, therefore, cross the meridian together and form another excellent set of north pointers.

The group of stars in the constellation of Orion are particularly brilliant, perhaps the most conspicuous of all star groups in the

winter heavens. Rigel, the stars in the belt of Orion, Bellatrix, and Betelgeuse are very near the celestial equator. Betelgeuse and  $\alpha$  Aurigæ transit together as do Rigel and Capella. We therefore have in the winter this double line running from the vicinity of Orion to the North Star.

*Sirius*, the brightest star in the heavens, is practically in line with the belt of Orion and also in line and about equidistant from the belt is Aldebaran.

77. *Date of midnight transit and declination of stars* shown in Figures IX-XI.

| Date.           | Declination. | Star.     | Date.            | Declination. | Star.       |
|-----------------|--------------|-----------|------------------|--------------|-------------|
| January 1.....  | 16.5° S.     | Sirius.   | July 19.....     | 8.5° N.      | Altair.     |
| January 13..... | .....        | Castor.   | August 2.....    | 45.0° N.     | Doneb.      |
| January 15..... | 5.5° N.      | Procyon.  | September 5..... | 30.0° S.     | Fomahaut.   |
| January 16..... | 28.0° N.     | Pollux.   | October 22.....  | 23.0° N.     | Hamel.      |
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78. The time of transit for any other night may be found approximately from the rule that the star transits four minutes earlier each successive night, about two hours each successive month, or 24 hours earlier (same date) at the end of the year.

79. The declination of a star is its angle, measured in the meridian from the equator. The latitude of a place on the earth is its angle measured in the meridian from the equator. Both are noted as north if north of equator, or south if south of equator. If the declination of a star is greater than the latitude of a place, it will pass the meridian to the north of the place. If less, it will pass the meridian to the south. Of course, if the declination is south and the latitude north, the star will always be to the south, and similarly, if the north declination of star is small and the latitude of the place high.

It is evident from the foregoing that by use of the additional sets of north-pointing stars, and with a little practice in studying the times of the year and hours of the nights when certain stars are to be found in the meridian to the north or south of us, we should seldom have any difficulty in knowing approximately at least our points of the compass.

If headquarters have, as we understand they have in France, tables from which the true azimuth of a star can be predicted for any hour of the day, and if orders based on these tables are to be issued, we must know the prominent stars. To learn them requires observation and practice, nothing else.

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Now that large-scale maps, such as 1:20,000 or 1:10,000, are used extensively by batteries in the field, map reading has become an important part of an officer's

work. From the map lines of fire are obtained, aiming points picked out, the position of targets identified, and ranges obtained.

Three distinct elements must be considered with respect to any point on the ground that is to be identified on the map, viz, (1) direction, (2) distance, and (3) shape of ground or relative height. It is not safe to decide on a point which appears to fulfill two of these conditions without examining as to the third.

#### (1) DIRECTION.

In measuring angles a semicircular celluloid protractor (Steward's) will be found useful and fairly accurate. If several points are to be identified in a given zone, a well-defined *distant reference point* must be selected and identified on the map. Using the protractor, measure the angle between the reference point and the object on the ground, then plot it off on the map.

#### (2) DISTANCE.

The approximate distance may be found in two ways:

1. By estimation.
2. By noting whether it is farther off or closer than other points easily identified or already known.

As a rule the latter method will be the more satisfactory. The scale of the map should be kept clearly in mind when considering distances to objects.

#### (3) SHAPE OF GROUND.

This condition, though considered last, is not of least importance, since a *careful study* of the contours will fix the position of an object on the map with far more certainty than will an estimated distance. It sometimes helps to examine all the features surrounding an object and then draw a rough plan of what is expected to be found on the map.

Often a *thick, well-defined hedge* indicates a road. What looks like a wood may be only scattered trees. A low ridge or embankment may conceal a hedge, so the first hedge visible beyond may be the second hedge shown on the map.

Watch the smoke of a distant railway train; it not only helps to identify the line of the railroad, but may be useful as a reference point for other objects. Finally, even the good maps may have mistakes, usually in connection with the roads.

#### PRACTICAL WORK.

81. The ability to read maps as above described can only be acquired by practice in the field. The following practical work should be executed by each member of the class in the field. If the training period permits, this character of the work should be continued until all are proficient in *reading ground from a distance*. A ridge in or near the training area will be selected from which a reasonably good view can be had. The members of the class with their sketching equipment and maps will be deployed along the ridge, so that as nearly as may be they have the same view. Before the lesson hour the instructor will have had placed several conspicuous objects; red or white flags will do if nothing else is at hand. A prominent object in the foreground will be designated by the instructor as the *reference point*, and each student after locating his position on the map and orienting will draw a ray to this point. He will then be required to sight and draw rays to the several flags. He will then be required to draw a small circle at the point on each ray where he believes the flag to be. He will then be required to draw a profile from his map along each of the rays. The drawing of each profile will require about 30 minutes of a beginner's time. There should not be so many required of him as to absorb the entire lesson period.

## TO DRAW THE PROFILE.

82. Look along the ray very carefully and find the lowest contour which the ray crosses and also the highest. Suppose the lowest to be 520 and the highest to be 640. The highest point on your profile will then, of course, be 640 feet and the lowest 520. The difference will be 120 feet. Suppose the contour interval is 20 feet; 20 goes into 120 six times. There are, therefore, six contour intervals between the highest and lowest point. Take a sheet of paper, the long edge of which is long enough to reach from your position on map to the position of flag. With your alidade as a ruler, draw six lines parallel to the long edge of the paper at equal distances apart and from the edge. This distance may be any convenient one, but should not be less than one-half inch, if practicable. (A method of drawing the lines parallel to each other, which suggests itself, is to lay off half-inch spaces along the short edges of the paper and connect them.) Now lay the long edge of the paper on the ray. Mark the edge of the paper as elevation 520 (the lowest elevation) and the highest line as 640; mark the intermediate ones 540, 560, 580, 600 and 620. Now, beginning at your station, look along the ray very carefully, and every time the ray crosses a contour (say the first one met is the 620) run a light line up to the corresponding parallel line (620 in this case) and make a cross there. Do the same at the next contour, and continue until you reach the position of the flag. Now connect the crosses in *succession*, beginning at the first one, by straight lines. The result will be a *profile* or *vertical section* of the ground between your position and the flag's (providing you located the flag correctly). Now compare your profile with the ground between you and the flag. Does your profile help you to tell whether you located the flag correctly? Did you overestimate the distance and plot the flag's position in a valley beyond the hill where you really could not see it?

83. Draw a *straight line* on your profile sheet from your position to the flag's position. Does this line clear all *intervening points* on the profile? If not, you could not see the flag where you have plotted it. This latter little problem is what is commonly called a *visibility problem*.

84. Each sketcher will now be required to outline on his map the areas (included between the rays to two flags) which are invisible to him. To do this, he will find it desirable to draw a number of profiles. He should draw no more than absolutely necessary, and these for the sole purpose of checking a decision which he has made by comparison of the map with the ground.

## LESSON XII.

## VISIBILITY.

85. A problem frequently arising in map reading is that of determining *what points are visible from a given point*. A point is visible when the gradient to it, if rising, is greater, and if falling, is smaller than the gradient to any intermediate point.

For this comparison gradients are conveniently represented by the quotient of distance in feet divided by the difference of elevation in feet. The point will be visible when this quotient is smaller, if

compelled to draw in contours at very small vertical intervals. In putting in the troublesome contour lines he has very likely rubbed out roads, houses, most of his fences, and all of his trees. The resulting sketch is apt to be characterized more by its intense *blackness* than by its clearness and military value.

A military sketch must show the *essential military* features of the area and as many of the less important military and other features as the scale of the sketch and the skill of the sketcher make possible. Just what amount of detail should be shown on a sketch in any particular case is a matter of judgment. As one's skill in sketching and training in military tactics proceeds, his ability to determine these questions for himself will grow.

53. A sketch to be of value must be clear. The essential features must be brought out with bold strokes. Do not fill up the sketch with rude conventional signs for trees, grass, and corn. Do not fill it up with a mass of crowded contour lines. While the normal system requires 10-foot contours for a 6-inch scale, and 20-foot contours for a 3-inch scale, this system is not to be followed slavishly. If the country is so steep that 10-foot or 20-foot contours will crowd each other, use a larger interval.

Break contours at the railroads and *roads*, so that these important lines of communication will stand out. Break them at cliffs and write the words "cliff 60 feet high." Break them at streams and write "stream 50 feet wide, banks 40 feet high, unfordable except as indicated." Omit no important *landmarks*.

54. The user of the sketch must be able to locate himself on the sketch and for that reason landmarks must appear upon the sketch at frequent intervals (if they exist in fact). A tumbled-down shack in a sparsely-settled region, a group of cottonwood trees in a treeless waste, a waterhole in a semiarid country, a group of large buildings of a public or semipublic institution in the vicinity of a town will serve to help the user locate himself. A stone bridge may name a battlefield.

55. The conventional signs as adopted for use by all United States Government departments, as well as the special sketching signs given in the Field Service Regulations, follow paragraph 155. They must be learned.

56. At least three lesson periods must now be spent in sketching.

## LESSON VIII.

### MAP READING IN THE FIELD.

57. Map reading is essentially the reverse of map making. One who has been practiced in sketching by the plane-table method should have no difficulty in reading and using a large scale sketch of a small area. The essential features stand out almost at a glance. But a map of a large area of ground can not be read at a glance. It must be measured and studied in much the same way as the ground itself would have to be measured and studied before we become familiar with the country represented.

Scale.—As in making a sketch we need a "*working scale*," so in studying a map we need a "*reading scale*." It is not sufficient in *reading* a map for military purposes to glance at the scale given on

the map and then to glance at two points and guess at the distance between them. The *units* of distance most used in our service are the *yard* and the *mile*. It will be useful, therefore, to prepare our *reading scale* in yards or miles. Pages 67 and 68 give scales for the usual range of topographic maps.

58. **Examples.**—To prepare a *reading scale* of yards for a map on a scale of 1:80,000. Here 1 yard on the ground is represented by  $\frac{1}{80,000}$  of a yard on the map. 1,000 yards on the ground by  $\frac{1,000}{80,000} = \frac{1}{80}$  of a yard or  $\frac{36}{80} = 0.45$  of an inch. Lay off a line 4.5 inches long and divide it into 10 parts and you have your scale. If a smaller unit than 1,000 yards is desired, divide the left unit into 10 equal parts.

59. To prepare a reading scale of miles for a map on a scale of 1:100,000. Here 1 mile on the ground is represented by  $\frac{1}{100,000}$  of a mile on the map. One mile is 5,280 feet, or 63,360 inches. Therefore the map representation of 1 mile on the ground is  $\frac{63,360}{100,000}$  or 0.634 of an inch. Lay off a line 6.34 inches long. It will represent 10 miles. Divide it into 10 equal parts and each part will represent 1 mile.

#### ORIENTATION AND DIRECTION.

60. To one who does not know his own position on the map or who does not hold it properly oriented when in use, a map is a hindrance rather than a help. One who is responsible for guiding troops by a map must keep his position on it by constant reference to the map. Too frequently in maneuvers, and even in actual war, is the map hidden away in a dispatch case. Then, after the column has already gone astray, frantic efforts are made by all concerned to recall the various textbook methods for orienting a map and for locating one's position upon the map.

#### PRACTICE WORK IN ORIENTATION.

61. It is useless to describe methods in a training manual unless the class is actually practiced in them. An indoor reading of the method of making a sketch or of orienting a map will do a beginner little good.

The following methods of orientation and resection should be tried out in the field by the class under the eye of the instructor:

*First method.*—Take a map of the training camp with the magnetic meridian marked upon it. Set up a sketching board on its tripod. Put the map on the board. Shift it until the magnetic meridian on the map becomes parallel to the meridian line of the needle trough. Pin the map down with thumb tacks. Orient the sketching board and resect from two points in view as described in paragraph 46.

*Second method.*—Using a compass, but not the sketching board. Lay the map on the ground. Lay the sight line of the compass along the magnetic meridian of the map. Rotate map and compass together until needle points north. If sight line of compass has



been kept along magnetic meridian of map, the map is oriented. Your location may be found by resecting as described in paragraph 46.

*Third method.*—No compass or no magnetic meridian. True meridian given; position unknown. Point the hour hand of your watch (held face upward) at the sun, if in the Northern Hemisphere. The line drawn from pivot to the point midway between the outer end of the hour hand and XII on the dial will point toward the south. Shift your map to correspond. This will give a very rough orientation. You may now be able to identify two or three distant points on the ground and their representations on the map. If you can do so, resect by the method explained in paragraph 46 or paragraph 47. Your resection will not be accurate, but it will serve to aid you in locating yourself.

62. While the last method is a good instruction method, there is no excuse in campaign for an officer not to have the magnetic meridian on his map. If the magnetic meridian is not shown on the map, ascertain the magnetic declination and draw the meridian on. The magnetic declination, it must be remembered, is the angle which the magnetic needle makes with the true north at the point. If the declination is east, it means that the north end of the needle settles to the east of true north. If west, the north end of the needle settles west. If the *magnetic declination* can not be readily ascertained, you can determine it approximately in the following manner:

#### DETERMINATION OF MAGNETIC DECLINATION.

63. In the explanation of this method, the term *magnetic azimuth* as here used is the horizontal angle from the north point of the *needle* measured *clockwise* around the *circle* to the *object* sighted. To read azimuths correctly, a box or pocket compass should be graduated *counter-clockwise*. If yours is not so graduated, better add a rough graduation in the counter-clockwise direction.

Observe the magnetic azimuth of the sun, a planet, or a bright star at *rising* and *setting* on the same day or at *setting* on one day and *rising* the next. Add these two azimuths together. Take the difference between this sum and 360°. One-half of this difference is the declination of your compass—east, if the *sum* of the *azimuths* is less than 360°; west, if it is greater. In using this *method* the observations are best taken when the object is *just above* the *true horizon*, or at a *gradient of zero*. This can usually be done if a high point is chosen for observation. *If this can not be done*, be careful to take both observations with the object at the same gradient (as determined with clinometer). *This is most important with the sun*. Under the least favorable conditions an inequality of 1° in the gradients at the time of observation on the sun may introduce an error of ½° in the result.

In using a star, choose one which rises nearly east from the point of observation. If this be done the inequality of a degree in the gradients will be immaterial. Both observations need not be made at the same point, but should not be more than 10 miles apart in east and west or north and south directions. (See also par. 68.)

## LESSON IX.

## DAY GUIDING BY MAP AND COMPASS.

64. The following condensed quotation from a recent supplement to the British Manual of Map Reading and Sketching is taken from the International Military Digest, March, 1916:

After mastering the *conventional signs*, map reading is only a matter of observation and *common sense*, a fact which leads people to underestimate its difficulty and the need for *continual practice*.

When finding the way by road, it is important to consider the *time factor* in attempting to identify points of the road in advance, and *not place sole reliance* upon *cross-roads*, or *side roads*, etc., which may have changed since the map was published. The speed of march may be obtained from a speedometer or by a rough approximation of the marching rate of the column. \* \* \*

Orienting the map by pointing at the sun [a common textbook method and at times a valuable one] may lead to an error in the direction of as much as  $7^{\circ}$  or  $8^{\circ}$ . Therefore, some *permanent point*, as a *church steeple* or a *straight* piece of road, should be sighted on.

When a *point* of the country has been identified on the map, time often will be saved by using it as a *reference point* in referring to others. Such points may be noted as *so many degrees* from it, or in line with it, or just to the right or left. A protractor will assist in laying off angles and measuring bearings on the map.

On a small-scale map many details are not shown, but much may be inferred from what is shown.

In *night movements practice* is *essential*, and although it is not difficult to march by compass bearing, much assistance can be obtained by the ability to recognize a *few stars* in *different parts* of the heavens.

65. After the remarks given above have been discussed, the instructor should practice the members of the class in following a course along roads and across country from the map. In order that this practice may not be done in a perfunctory manner, it is desirable to require the student officers to traverse a course outlined by the instructor, and note on the map all features which may be altered. If the map is so nearly correct that this method is impracticable, flags bearing special numbers may be erected along the course and the student officers required to locate the flags on their sheets. It will be particularly good practice if a group of flags representing a trench are so located that they can be found only by following a compass bearing across country for a distance of several miles.

Such practice will convince all of the great difficulties in guiding by compass alone. A judicious use of the map and of prominent physical features will simplify the matter in open country.

Before starting, the course should be carefully protracted onto the map and note taken of the *prominent physical features through which* or *near which* the line passes. Before starting, identify one of these points on the ground and march on it. If you must descend into a valley to lose sight of the feature, take some point in the valley which is in line to march on. Thus, continue from feature to feature. In close country this is not so simple. Here it may be necessary for you to actually plot on your map, or an enlargement of it, your course as you go. Make your courses as long as possible.

## LESSON X.

## NIGHT GUIDING BY MAP, STAR, AND COMPASS.

## 66. The following is taken from the Artillery Journal:

As an aeronaut in Ladysmith, I had plenty of opportunities of foreseeing the great power aeronautics would have in warfare in the future, and that most of the effective fighting would be done at night.

At that time the regulations described night operations as extremely hazardous, and warned the commander who undertook such operations that he did so at his own peril and was responsible for the results. Various expedients were suggested to enable the troops to keep their directions, such as that the route should be previously reconnoitered and marked by tins, pieces of paper, and other devices; but how the reconnoitering party was ever to carry out this operation nobody has yet been able to understand. We found the *colonials* never required this artificial help, and could move about on a *starlit night* as easily as in *daylight* and as fast as the nature of the ground permitted, \* \* \* and ascertained from various *colonials*, Basutos, Indians, and Arabs that they could instinctively read the heavens as a compass, this knowledge having been transmitted from father to son for generations. \* \* \*

Although the system was only perfected in June, 1915, *soldiers* of all ranks have begun to realize the simplicity and wonderful utility of being able to read the *universal compass*, the *heavens*, and we begin to hear how useful this knowledge has been found for guiding supporting troops up to the first-line trenches, etc.

The heavens can not go wrong, and on a starlit night you can rely absolutely upon them to take you to your destination, *once you grasp* the rudiments of the system; you only *require* to know three or four first magnitude stars, for their exact position is given for every hour of the night in Marching and Flying without a Compass (Tilney, lieutenant colonel, F. R. C. S.)

## TO FIND THE STARS.

67. *The Dipper and Cassiopeia*.—The star plans given here, and parts of the descriptions, are taken from The Star Pocket Book by Capt. Weatherhead, British Royal Navy.

*Ursa Major* (called the Big Dipper), shown in the upper portion of Figure IX, is the most important of the constellations. It is at once the easiest to distinguish, the easiest to find the North Star by, and the best *starting point* from which to learn the other stars. The "Pointers"  $\alpha$  and  $\beta$  point to *Polaris* (the North Star) at all times as the Dipper circles the Pole. On the opposite side of *Polaris* and at about the same distance from it is the constellation of *Cassiopeia*. Its form is that of the letter W.

The great importance which attaches to *Polaris* (the North Star) is that it is never more than  $2^\circ$  away from the point where the axis of the earth if extended would pierce the heavens. It therefore appears to the eye to be always in the same place, and it is, except for a maximum variation of about  $2^\circ$ .

68. As the *latitude* of any place is equal to the *altitude* of the Pole, when the Dipper and Cassiopeia are on either side of the North Star (east and west), the elevation of the North Star will give a reasonably correct figure for the latitude of the place of observation. When the Dipper and Cassiopeia are above or below the North Star, a compass reading to the North Star will give the *declination* of your compass to within the *least reading* of your compass.

69. *Arcturus, Spica, Denebola*.—The lower half of Figure IX shows the *Big Dipper* again. By continuing the sweep of the *Dipper handle*, you will find the bright star *Arcturus* about  $30^\circ$  from the end of the handle. Continue on with the curve and you will find *Spica* about  $30^\circ$  farther on.

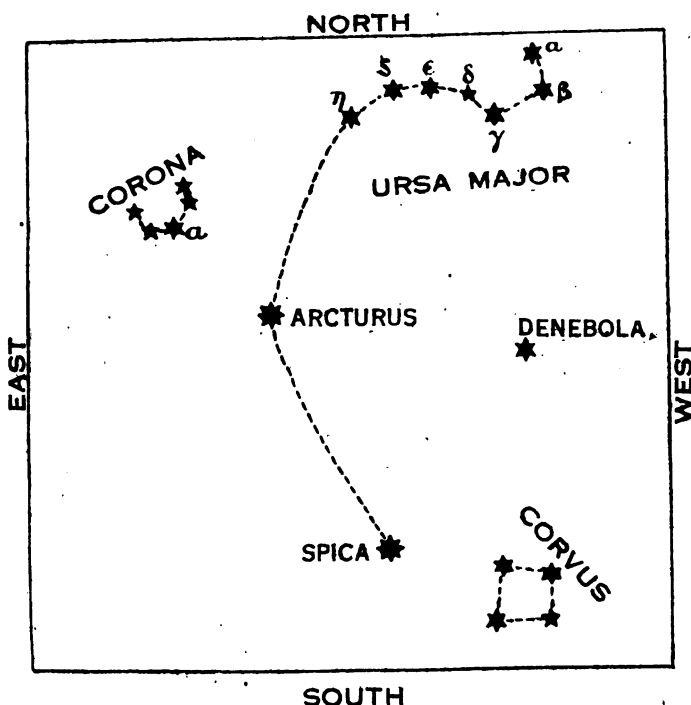
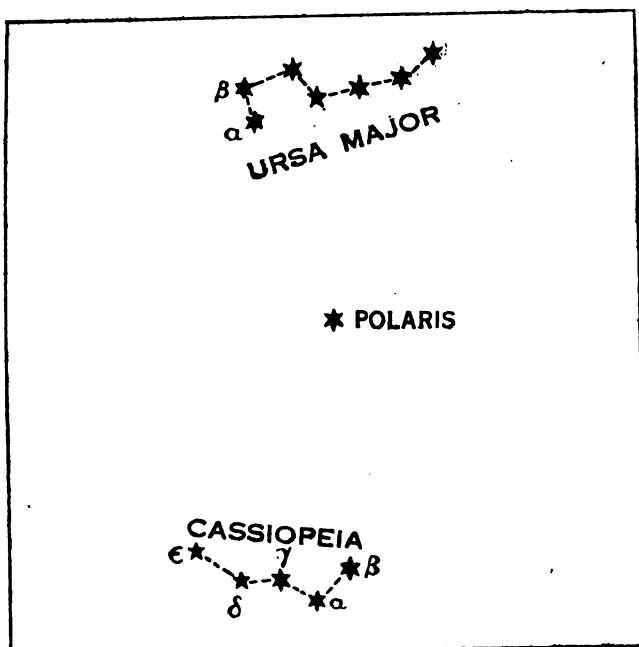


FIGURE IX

of the Dipper and may be of great use, therefore, when the pointers, low in the heavens, are obscured by clouds.

76. *Capella, Aldebaran, Castor, and Pollux* (Fig. XI).—Aldebaran is to be found on the meridian at midnight of November 29, Capella on December 9, Castor on January 13 and Pollux on January 16. In the fall months and early winter we will find them in the east in the hours before midnight and in the west in the later winter months. A

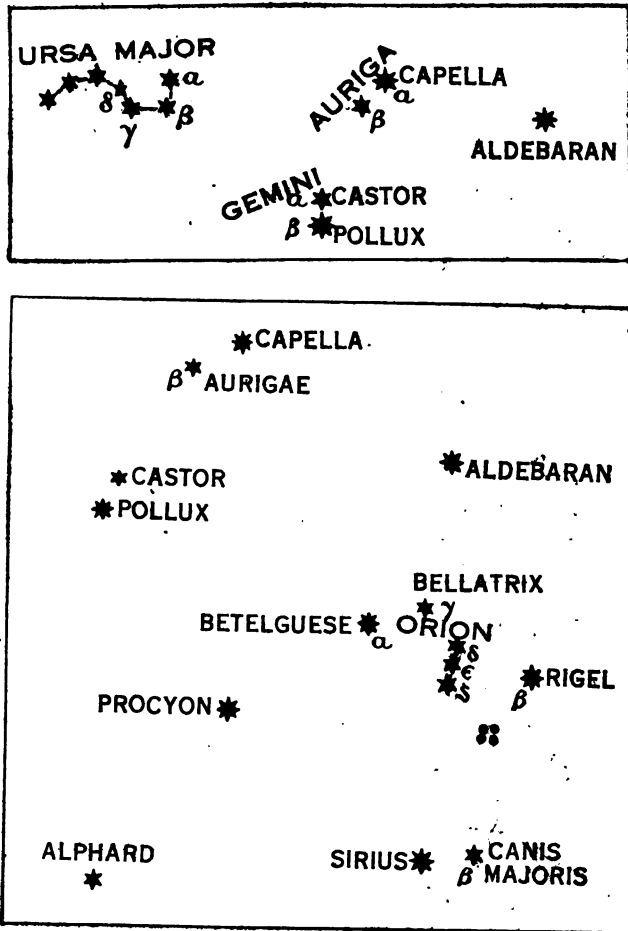


FIGURE XI

line drawn from the pole star perpendicular to the line from the "Pointers" passes through Capella. This line also passes directly through *Rigel*, a bright star in the constellation of Orion. These two stars, therefore, cross the meridian together and form another excellent set of north pointers.

The group of stars in the constellation of Orion are particularly brilliant, perhaps the most conspicuous of all star groups in the

The stars on these charts, therefore, are to be looked for in the early hours of the summer evening in the east; high in the heavens in the early fall; and in the west along Christmas time.

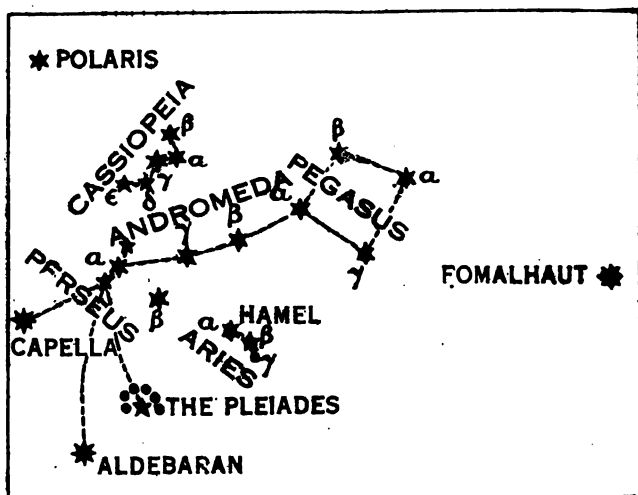
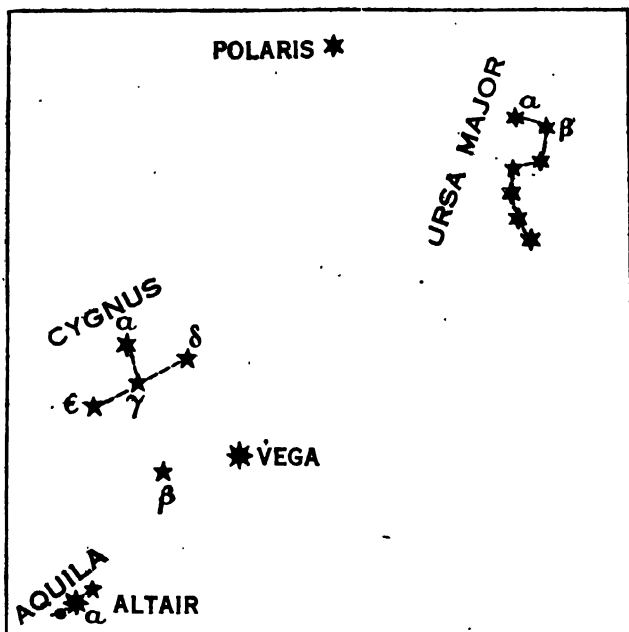


FIGURE X

75.  $\alpha$  and  $\beta$  Pegasi point directly at Fomalhaut, which, therefore, also crosses the meridian at midnight on September 7. These three stars form as perfect a set of pointers to the Pole as do the "Pointers

of the Dipper and may be of great use, therefore, when the pointers, low in the heavens, are obscured by clouds.

76. *Capella, Aldebaran, Castor, and Pollux* (Fig. XI).—Aldebaran is to be found on the meridian at midnight of November 29, Capella on December 9, Castor on January 13 and Pollux on January 16. In the fall months and early winter we will find them in the east in the hours before midnight and in the west in the later winter months. A

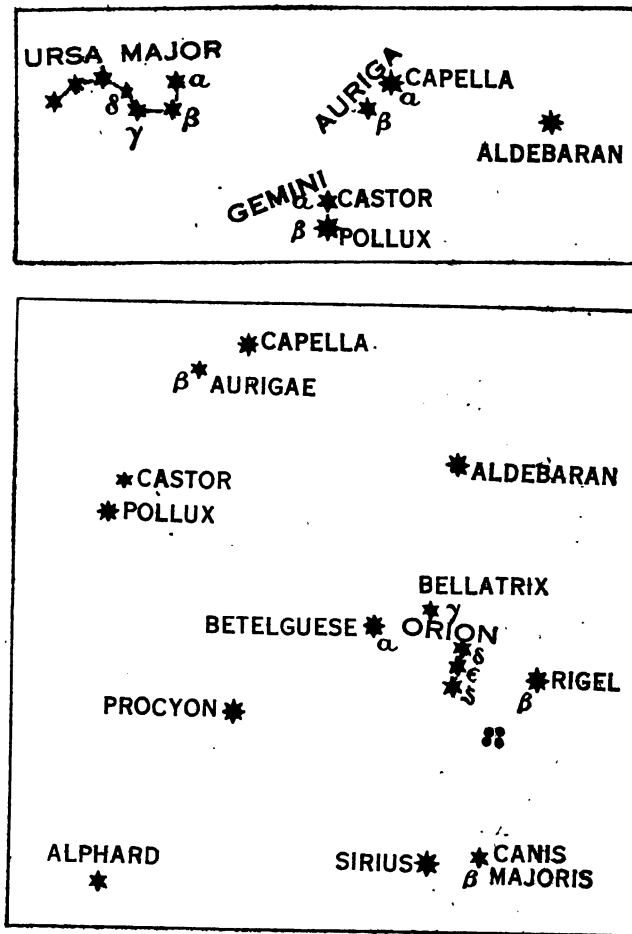


FIGURE XI

line drawn from the pole star perpendicular to the line from the "Pointers" passes through Capella. This line also passes directly through *Rigel*, a bright star in the constellation of Orion. These two stars, therefore, cross the meridian together and form another excellent set of north pointers.

The group of stars in the constellation of Orion are particularly brilliant, perhaps the most conspicuous of all star groups in the

winter heavens. Rigel, the stars in the belt of Orion, Bellatrix, and Betelgeuse are very near the celestial equator. Betelgeuse and  $\alpha$  Aurigae transit together as do Rigel and Capella. We therefore have in the winter this double line running from the vicinity of Orion to the North Star.

*Sirius*, the brightest star in the heavens, is practically in line with the belt of Orion and also in line and about equidistant from the belt is Aldebaran.

77. *Date of midnight transit and declination of stars shown in Figures IX-XI.*

| Date.           | Declina-<br>tion. | Star.     | Date.            | Declina-<br>tion. | Star.       |
|-----------------|-------------------|-----------|------------------|-------------------|-------------|
| January 1.....  | 16.5° S..         | Sirius.   | July 12.....     | 8.5° N..          | Altair.     |
| January 13..... | .....             | Castor.   | August 2.....    | 45.0° N..         | Deneb.      |
| January 15..... | 5.5° N..          | Procyon.  | September 5..... | 30.0° S..         | Fomahaut.   |
| January 16..... | 28.0° N..         | Pollux.   | October 22.....  | 22.0° N..         | Hamel.      |
| March 7.....    | .....             | Pointers. | November 29..... | 16.0° N..         | Aldebaran.  |
| March 19.....   | 15.0° N..         | Denebola. | December 9.....  | 46.0° N..         | Capella.    |
| April 12.....   | 11.0° S..         | Spica.    | December 9.....  | 8.0° S..          | Rigel.      |
| April 25.....   | 19.5° N..         | Arcturus. | December 12..... | 6.0° N..          | Bellatrix.  |
| July 1.....     | 39.0° N..         | Vega.     | December 19..... | 7.5° N..          | Betelgeuse. |

78. The time of transit for any other night may be found approximately from the rule that the star transits four minutes earlier each successive night, about two hours each successive month, or 24 hours earlier (same date) at the end of the year.

79. The declination of a star is its angle, measured in the meridian from the equator. The latitude of a place on the earth is its angle measured in the meridian from the equator. Both are noted as north if north of equator, or south if south of equator. If the declination of a star is greater than the latitude of a place, it will pass the meridian to the north of the place. If less, it will pass the meridian to the south. Of course, if the declination is south and the latitude north, the star will always be to the south, and similarly, if the north declination of star is small and the latitude of the place high.

It is evident from the foregoing that by use of the additional sets of north-pointing stars, and with a little practice in studying the times of the year and hours of the nights when certain stars are to be found in the meridian to the north or south of us, we should seldom have any difficulty in knowing approximately at least our points of the compass.

If headquarters have, as we understand they have in France, tables from which the true azimuth of a star can be predicted for any hour of the day, and if orders based on these tables are to be issued, we must know the prominent stars. To learn them requires observation and practice, nothing else.

## LESSON XI.

### USE OF MAPS IN POSITION WARFARE.

80. The following condensed quotation from an article in the British Journal Royal Artillery is taken from the International Military Digest:

Now that large-scale maps, such as 1:20,000 or 1:10,000, are used extensively by batteries in the field, map reading has become an important part of an officer's



used in surveying for the measurement of angles, distance, and elevation. The following plan of procedure is suggested for a topographical survey of an area too large to permit of the use of reconnaissance methods and yet not large enough to justify geodetic methods. The time allotted to this training course and the personnel of the class will determine whether instruction can be given in this part of the manual.

## LESSON XX.

### TOPOGRAPHICAL SURVEY OF AN AREA APPROXIMATELY 100 SQUARE MILES.

117. In this work, as indeed in all map work or sketching, it "must be accepted as an axiom that however large or however small may be the area to be surveyed, it must be treated as a whole, and that all over the area a *number of carefully determined points* must be fixed," and these points adjusted among themselves to form an accurate framework on which the less accurate work may be hung.

The accuracy of the entire map will depend upon the accuracy of the framework or control. The framework may be located by *triangulation* or by *transit traverses*. A combination of the two will be the ordinary rule.

#### TRIANGULATION.

118. Paragraphs 187 to 189 give the methods to be followed in measuring the *base line*. It should be remembered that an error in the base line will be reproduced in the triangulation. Thus, if the base measurement is  $\frac{1}{1000}$  larger than it should be and the farthest point of the triangulation is actually 10 miles from the base, the triangulation will place the point at a distance of  $\frac{1}{100}$  mile, about 50 feet too far. This would not be serious if the work is to be carried no further.

#### ANGLE MEASUREMENT.

119. If *possible*, all of the angles of each triangle should be measured. The procedure at each station is as follows: Level carefully with the telescope level and see that the plate levels and other adjustments are satisfactory. For each principal angle: Set the A vernier to read zero and, with the telescope direct, set with the lower motion carefully on the left-hand station. Read and record both verniers. Unclamp above and set on the right-hand station. Read and record the A vernier for the *approximate angle*. Find the number of whole times 60 will go into this approximate angle and call this M. Then—

|   |                      |
|---|----------------------|
| Unclamp below and set on the left-hand station  | } Second repetition. |
| Unclamp above and set on the right-hand station |                      |
| Unclamp below and set on the left-hand station  | } Third repetition.  |
| Unclamp above and set on the right-hand station |                      |

Plunge the instrument, and without disturbing the vernier setting,

|   |                      |
|---|----------------------|
| Unclamp below and set on the left-hand station  | } Fourth repetition. |
| Unclamp above and set on the right-hand station |                      |
| Unclamp below and set on the left-hand station  | } Fifth repetition.  |
| Unclamp above and set on the right-hand station |                      |
| Unclamp below and set on the left-hand station  | } Sixth repetition.  |
| Unclamp above and set on the right-hand station |                      |

Read and record both verniers. The mean of the "seconds" of the two verniers will be taken with the degrees and minutes of the A

vernier as the vernier reading. To this must be added  $360^\circ$  multiplied by M as above determined. This large angle is then divided by 6. This is the value of the angle for one set of readings. A second set should now be taken. In the second set the vernier at the start should be set at  $35^\circ$ . If the values from the observed sets do not check out, the observations are immediately repeated, if they do take the mean.

120. In reading vertical angles, level the instrument with the telescope level. Measure and record the HI. Read, direct, the vertical angles. Plunge the telescope and reread the vertical angles. Relevel the instrument and repeat the direct and reverse observations. The recorder notes the point observed and the vertical angle for each station, landmark, or flag.

121. After the angles which pertain to the triangulation system have been read and recorded as above described, a series of "pointings" are taken to all spires and other prominent landmarks in view, record of each object "pointed" being kept in such a manner that there will be no difficulty in identifying it later, when "pointed" from another station. These pointings are taken as follows:

Set A vernier at zero, and with the telescope direct, set carefully with the lower motion on any *principal station*. Then, unclamping above, read the angles to the successive landmarks in turn around the horizon, closing and reading in the original zero line. Set B vernier at zero and, with the telescope reversed, again set by lower motion on some principal station. Unclamp above and read landmarks as before, closing on the zero line. In case either reading on the closing line or direct and reverse reading on any landmark do not check within one minute, repeat the entire operation.

#### THE STATION ADJUSTMENT.

121. After all the *main angles* have been satisfactorily observed, closing the horizon, their sum should equal  $360^\circ$ . The difference between  $360^\circ$  and the sum will be divided equally and applied as a correction to each angle, so that the resultant sum is  $360^\circ$ . This adjustment is made in the notebook, and the final values checked.

#### REDUCTION TO CENTER.

122. In triangulation of the character being described, it frequently happens that angles are taken to some point, such as a tree, where it is impossible to erect the transit. In such a case the instrument is set up at the nearest convenient point, called a *satellite station*, at a short distance from the tree, and the angles taken from this station can be afterwards reduced to the true values at the object itself.

From the satellite station which we will call S, the round of angles will be read as usual, taking care to include the tree which we will call T. Measure the distance from S to T carefully. Let A and B represent two stations from which T has been observed, A being on the same "hand" of B as is S from T, in this case the left. We measured the angle ASB. The angle desired is ATB.

$$(a) \text{ ATB} = \text{ASB} + \text{SAT} - \text{SBT}.$$

To find SAT and SBT we need to know the length of AT and BT approximately. To determine them approximately, we can plot the triangle ASB, lay off ST in direction and distance as observed and measure AT and BT. This should be done at a large scale. Now—

$$(b) \sin SAT = \sin TSA \frac{ST}{AT} \text{ and}$$

$$(c) \sin SBT = \sin TSB \frac{ST}{BT}$$

From (b) find  $\sin SAT$  and from it the angle SAT.

From (c) find SBT, substitute these values in (a), and we find  $ATB$ . (See fig. 14.)

#### ADJUSTMENT OF ANGLES OF TRIANGLES.

123. In securing the triangulation control for an area of 100 square miles or so, the purpose of which is primarily the construction of a map on a reasonably small scale, the computations necessary for the adjustment of quadrilaterals are not justified. Each triangle, therefore, will be adjusted as a single figure as completed and the computed sides considered as correct, unless, of course, an actual mistake is discovered. It should be realized, therefore, that the fewer of these main control triangles we use, the better for the work. If the country is suited to triangulation, we may wish to have a number of small triangles to control the actual taking of the topography, but these *should not* be made a part of the main triangulation system. They should be adjusted *to it*, not with it. Except for station adjustment of angles, which is of course desirable, nothing should enter into the adjustment of any of the main triangles but the angles at the vertices of *each triangle*.

124. It is evident, therefore, that if the triangulation net is extended to the sides as well as forward that each vertex located to the side must depend for its adjustment upon the side used for a base for its determination and no interadjustment between adjoining side triangles must be attempted. Do the work carefully and you will have confidence in the resulting system of control.

124. The angles of any one of the main triangles are to be adjusted as follows: Add them together. The difference between the sum and  $180^\circ$  is the error. (This should not be greater than 30 seconds and will be less if care has been taken to use rigid points to sight on and light conditions have been favorable.) Distribute the error equally (not proportionately) among the three angles so that their sum will be  $180^\circ$ .

#### AZIMUTH.

125. The initial meridian of the triangulation should be a true north and south line. Azimuths in this work are reckoned from the initial meridian or lines drawn parallel to it; from the south point, in the direction S-W-N-E and from  $0^\circ$  to  $360^\circ$ .

## COMPUTATION OF SIDES.

125. The base line is the only side of the triangle whose length is known. The other sides are to be found from the law of sines, that is—

$$\frac{\sin A}{\sin B} = \frac{a}{b} \quad \frac{a \sin B}{\sin A} = b$$

$$\frac{\sin A}{\sin C} = \frac{a}{c} \quad \frac{a \sin C}{\sin A} = c$$

Assuming  $a$  to be the *base* and the angles  $A$ ,  $B$ , and  $C$  to have been measured, the calculations are arranged as follows:

- (1)  $\log a$  (1400.74) = 3.1463575.
- (2)  $\text{colog } \sin A$  ( $57^\circ 42' 16''$ ) = 0.0729874.
- (3)  $\log \sin B$  ( $61^\circ 17' 53''$ ) = 9.9430639.
- (4)  $\log \sin C$  ( $60^\circ 59' 51''$ ) = 9.9418088.
- Sum of (1) (2) (3) =  $\log b$  = 3.1624088.
- Sum of (1) (2) (4) =  $\log c$  = 3.1611537.

## COMPUTING THE COORDINATES.

127. The next step in the computations is to put the results in a form which permits accurate plotting and which enables a record to be *kept* of the position of each trigonometrical point. The system used will in this work be rectangular coordinates.

128. If practicable, the origin of coordinates should be so located that the entire area to be surveyed will be north and east of it. The coordinates of all points of the area will then be plus. This is to be desired.

129. It is to be understood that in rectangular coordinates the *initial meridian*, that is, the north and south line through the origin, is the *only true north and south line of the survey*. All azimuths are referred to it and the convergence of meridians is neglected. This is allowable in small areas. Through the origin of coordinates, two lines are imagined, one line north and south, which is the initial meridian, the other perpendicular to that line at the origin. The location with respect to the origin of any point is established when its *departure* (perpendicular distance from the initial meridian) and its *latitude* (perpendicular distance from the east and west line axis) are *known*.

130. The sign of departure when east of the initial meridian is plus. The sign of a latitude when north of the origin of coordinates is plus. It is usual to speak of the initial meridian as the  $Y$  axis, and the other as the  $X$  axis. Differences in latitudes are, therefore, spoken of as differences in  $Y$ , and differences in departure as differences in  $X$ .

131. If the coordinates of the point of origin are *known* or assumed, the coordinates of any other point which is tied to it by angle and distance may be found by adding, algebraically, the difference in  $X$  and the difference in  $Y$  to the coordinates of the point of origin. The difference in coordinates between the origin and the other point will be obtained as follows:

Difference in  $X$  = distance to point  $x \sin$  azimuth.

Difference in  $Y$  = distance to point  $x \cos$  azimuth.

The coordinates of any new point may similarly be determined from those of any other point whose coordinates are known and to which the unknown point is tied by angle and direction.

## LESSON XXI.

### TRAVERSE CONTROL.

132. The purpose of the higher or triangulation control just described is to establish a few points in the area with a considerable degree of precision upon which to hang the control of lower order. If the country does not lend itself to triangulation, these few points may be established by a traverse control.

133. If a railroad or reasonably level road runs through the area, it is quite possible to traverse it and measure it by stadia with an accuracy of 1 in 500. If the distance across the area is 10 miles (52,800 feet) the total error in the line would be about 100 feet, probably quite as good a "fixation" as would be made by rapid triangulation. There is a disadvantage, however, in the single-line traverse for main control in that there is no check on mistakes in distance.

134. If the triangulation system has established a known point on which to close the traverse, well and good; but if there have been no points established by triangulation, the main traverse must be run as a loop, closing on itself or be remeasured as a base line. The following procedure is preferred for this class of traverse: Through the origin a true north-and-south line will have been laid out. The first set up is over the point of origin, and instrument is set to read zero pointing to a pin in the meridian south of the origin. This pin is the orientation station for the first set up.

135. At the first station.—Party arrives at the first known position.

I. Transit is set up carefully over the station, with tripod screws unclamped. Level approximately; center the instrument accurately, with the plumb-bob just above the mark. Clamp the tripod legs.

II. Level with telescope level. Lower the needle. Measure and record height of instrument.

III. Set the "A" vernier to read the azimuth to the orientation point. If the A and B verniers do not agree in minutes, so set "A" that the mean of the minutes on A and B will be the correct azimuth.

IV. With the lower motion, sight accurately on the orienting station, clamping securely below.

V. Read and record magnetic bearing. Recorder makes note of declination. (Even with local attraction, the needle will check the front with the back sights from the same station.)

VI. Unclamp above and take side shots, if any, reading (1) stadia; (2) control vernier "A," (3) vertical angle. In taking these side shots, clamp the alidade lightly.

VII. After the last side shot, sight again on the orienting station, checking the vernier reading. Plate levels are observed to see that the instrument has not gotten out of level.

VIII. The front rodman, having chosen the new station with respect to the conditions of having a good line further on, topographic control and proper distance from the instrument, is signaled "up." He presents the edge of his rod vertically over the new mark.

IX. At the instrument sight carefully with the upper motion on the new station, clamping firmly. Signal the front rodman, who then presents the flat stadia vertically over the mark. The rod rests on the mark, not on the ground.

X. Read and record (1) the stadia intercept; then set the horizontal wire on the stadia number corresponding to the HI. Glance at the plate levels to see if the instrument is still level. Read and record in order (2) control vernier "A," (3) vertical angle, (4) check vernier "B," (5) magnetic bearing (needle). The recorder repeats all readings as given, notifying the observer if the vernier readings or the magnetic reading do not check. (See par. 139.)

XI. Signal down the front rodman. Raise and clamp the needle. Put telescope in carrying position. Loosen the lower motion. Observer with instrument and recorder move to forward station. Rear rodman stays at the station.

136. At the second station.—

I. Set up accurately as before, level with telescope level. Unclamp the needle. Measure and record the HI.

II. Check the reading of the "B" vernier, which at this station is control. If there has been a slip, reset the "B" vernier at the same reading the "B" vernier had on the last foresight. Signal "up" the rear rodman to present the edge of his rod vertically over the old station.

III. With the upper motion still clamped and the telescope direct (not "plunged") sight carefully with the lower motion on the rear station, clamping firmly.

IV. Signal the rear rodman to present the flat of his rod vertically over the mark. Read and record the stadia intercepts, the recorder noting the check with the former fore shot.

V. Set the horizontal wire on the stadia number corresponding to the present HI, glancing at the plate levels.

VI. Read and record in order (2) control vernier "B," (3) vertical angle, (4) check vernier "A," and (5) magnetic bearing. Recorder notes if the verniers check, if the vertical angle checks with former front shot. If the vertical angle does not check, remeasure the HI, relevel with the telescope level, check the vertical circle adjustment and reread the vertical angle. Take this value as final, the recorder making special remarks to that effect in the notes.

VII. Signal down the rear rodman. Read the necessary side shots as before, clamping the alidade (upper motion) lightly. The first side shot should be well-defined landmark, preferably at least 800 feet distant as an orientation check. On this shot read and record both verniers and the magnetic bearing.

VIII. After taking the last side shot, call up the front rodman who has chosen the new forward station and who presents his rod as before.

IX. Check the azimuth on the orienting point (first side shot), noting that the instrument is still level.

X. Sight carefully on the forward station, clamping the alidade (upper motion) firmly. Then read and record as before (1) stadia, (2) control vernier ("B" for this station), (3) vertical angle, (4) check vernier "A," (5) magnetic bearing. The "B" vernier has remained control for this station.

XI. Clamp the needle, loosen the lower motion, put the instrument in carrying position and move forward again.

137. At succeeding stations.—Proceed as above. "A" and "B" alternate as the control vernier. In this way, the azimuth is carried forward without introducing errors of collimation, and errors due to eccentricity, inclination of the horizontal axis and vertical circle adjustment, are automatically balanced and corrected.

138. If, on closing on a triangulation station or closing the traverse on point of beginning, the azimuth is not out sufficiently to indicate a mistake, the error in azimuth will be divided by the number of stations and distributed, the changes being noted in ink in the note book. It will be noted that the control vernier gives the degrees of azimuth. The minutes taken will be the mean of the minutes of the two verniers. -

139. Method of recording traverse notes.

*L. A. traverse from  $\triangle$  Asan to  $\triangle$  Agana.*

| Station.          |                     | Stadia.  | Azimuth. |        | V. A.     | Diff. El. |
|-------------------|---------------------|----------|----------|--------|-----------|-----------|
| From—             | To—                 |          | Control. | Check. |           |           |
|                   |                     | H. Dist. |          |        |           | Elev.     |
|                   | $\odot$ 5           | 525      | 152 06   | 332 06 | — 0 01    |           |
| $\odot$ 4         | $\odot$ 3           | 820      | 320 41   | 140 21 | — 0 41    |           |
|                   | $\odot$ 4           | 820      | 140 41   | 320 41 | + 0 40 30 |           |
| $\odot$ 3         | $\odot$ 2           | 935      | 314 57   | 134 57 | — 0 06    |           |
|                   | $\odot$ 3           | 935.5    | 134 57   | 134 57 | + 0 06 30 |           |
| $\odot$ LAZ       | $\odot$ 1           | 936      | 134 57   | 134 57 | + 0 07    |           |
|                   | $\odot$ 1           | 347      | 310 28   | 130 28 | + 0 05    |           |
|                   | $\odot$ LAZ         | 348      | 130 28   | 310 28 | — 0 04 30 |           |
| $\odot$ LAI       | $\triangle$ Asan    | 349      | 45 10    | 225 10 | + 3 25    |           |
|                   | Mean                | 134.5    | 225 10   | 45 10  | 0 24 30   |           |
| $\triangle$ Asan— | $\triangle$ Chachao | 134      | 179 32   | 259 32 | + 1 11    |           |

140. The azimuth error distributed, the differences in X and Y are computed as stated in paragraph 131.

Care must be taken to give the computed latitudes and departures their proper signs. With azimuths reckoned from the south point as zero and in the direction of the movement of the hands of a clock;

For azimuth between 0 and 90, latitudes are negative and departures are negative.

For azimuth between 90 and 180, latitudes are positive and departures are negative.

For azimuth between 180 and 270, latitudes are positive and departures are positive.

For azimuth between 270 and 360, latitudes are negative and departures are positive.

141. If the azimuths and lengths of courses had been exactly determined in the field and no error has been made in computation, the survey would close, that is, the sum of all the plus latitudes (northings) would equal the sum of all the minus latitudes (southings) and the sum of all the "eastings" would equal the sum of all the "westings." Such exactness is, of course, not attainable and the sum of all the "northings" will not equal the sum of all the "southings," nor the "eastings," the "westings."

142. The total error in latitude is the difference between the sum of the northings and the sum of the southings. Similarly the total error in departure is the difference between the sum of the eastings and the sum of the westings.

143. As the errors in latitude and departure are those due to distance alone (the error in azimuth having been distributed before computations), the corrections should be applied according to the lengths of the courses. The rule is: The correction to be applied to the latitude of any course is to the total amount of the error in latitude as the latitude of that course is to the sum of all the latitudes (without regard to algebraic signs). A similar rule determines the correction in departure for each course. The corrections to latitudes and departures of each of the courses having been applied, the total latitudes and departures (coordinates) of a station are found by adding algebraically to the latitude or departure of the initial point of the traverse, the algebraic sum of all the latitudes or departures of the preceding courses. These coordinates are used for the plotting of the stations.

144. The main control traverses having been run, computed, and adjusted as above described, the stations of the traverse are plotted in ink, station numbers and elevations being noted in pencil. This done, a careful tracing of all the data on the projection sheet is made on vellum, cut to a size to fit the engineer sketching board. Each topographer is given one or more of these field sheets to fill in. When practicable, the areas assigned to a topographer will be those over which he and his party have been engaged in running the main traverses. Boundaries of these field sheets should be roads, railroad or trails. If this be impracticable, then well defined physical feature, as streams or cutting through brush and timber.

#### VERTICAL CONTROL.

145. Over the main traverse lines it is advisable in most cases to run a line of levels. (Par. 205.)

#### SUBSIDIARY CONTROL.

146. Each topographer now proceeds to complete the control of his area. His procedure will be as follows: Beginning at a convenient "fixed" point in his area, he runs, or causes to be run by his assistants, flying transit and stadia, compass and notebook, or sketching board traverses; using stadia or aneroid or clinometer for carrying elevations, as may be required by the length and importance of the line and as preferred by the individual. In this manner the topographer searches out the complete network of roads, trails, and streams for the entire field sheet on which he is engaged. This network should be so complete that the contour sketcher will need do no adjusting in his work. This will require that the distances between subsidiary traverse lines or other fixations should not exceed 1 mile on the scale of 1 mile to the inch or in general 1 inch on the map whatever the scale.

147. It is to be understood, of course, that the subsidiary traverses run by the topographers between points of higher control, etc., must not be plotted on the topographers record sheet until they have been properly adjusted. In long important lines, the adjust-



ment will be made by latitudes and departures, as described for main traverse lines. In the shorter lines, these computations are not justified and the graphical methods indicated in figures 12 and 13 will be used.

148. Figure XII shows method of graphical adjustment for a traverse run between two points, the positions of which are already plotted on the *record sheet*. Proceed as follows:

Plot the traverse, as actually measured in the field. In plane table work, of course, this is already done. Draw a line  $A B$  from the beginning point to the ending point of the plat. Now from the record sheet measure the straight line distance between the *record* positions of  $A$  and  $B$ . Measure off this distance from  $A$  on line  $A B$ . Call the end of the distance  $b$ .

Take any convenient point  $O$  and draw  $O A$  and  $O B$ . Now from  $b$  draw line parallel to  $O A$ . Where this line crosses  $O B$  is new position ( $B'$ ) for  $B$ . From  $B'$  draw line parallel to  $A B$ . Where this line intersects  $A O$  is new position of  $A$ .

To find new position of station 1, draw line from  $A'$  parallel to  $A 1$  and where it intersects  $O 1$  is new position ( $1'$ ) of 1. From 1 draw line parallel to 1-2, etc.

The traverse  $A', 1', 2' \dots B'$  is now adjusted and can be traced off onto record sheet.

149. Figure XIII shows *method when a circuit is run from a known point back to the same point*. Plat the traverse as measured in the field. The point  $A'$  should be at  $A$ , but, due to errors, does not so plat. On a long straight line  $O A$  lay off from  $O$ , in succession, the lengths of the courses ( $A-1, 1-2, 2-3$ , etc., + ——— 13- $A'$ ). From the end of this line lay off in any convenient direction the line  $A B$  equal to the error in closure  $A'A$ . Connect the outer end of this offset line to  $O$ . Now from each succeeding station point on the *long line*, draw a line parallel to the *offset line*  $A B$ .

Returning to the *plat* of the *traverse*, draw through each plotted station a line parallel to the final closure line  $A'A$  and in the direction of the closing station. On each line lay off its respective offset length, giving new positions for each station. Connect these new stations and the traverse is adjusted.

#### SKETCHING.

150. The field sheet which has been thus prepared consists of a network of traverses along roads, trails, streams, and across country with the horizontal detail along these traverses, with stations and easily identified objects shown in their proper adjusted locations and with their proper adjusted elevations given. It is the contour sketcher's task to go over the area assigned to him, sketching the drainage, culture, and forms of relief; generalizing the features to suit the scale and purpose of the map. The course in sketching will have taught the sketcher *how* to sketch rapidly. He must, on this work, follow similar methods, but "watch his step," as the map must answer severe tests. Especial care must be taken to see that all prominent landmarks are so located that they may be later used as orientation points in sketching or map reading.

ART. 20.

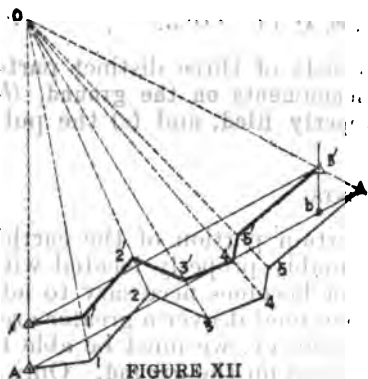


FIGURE XII

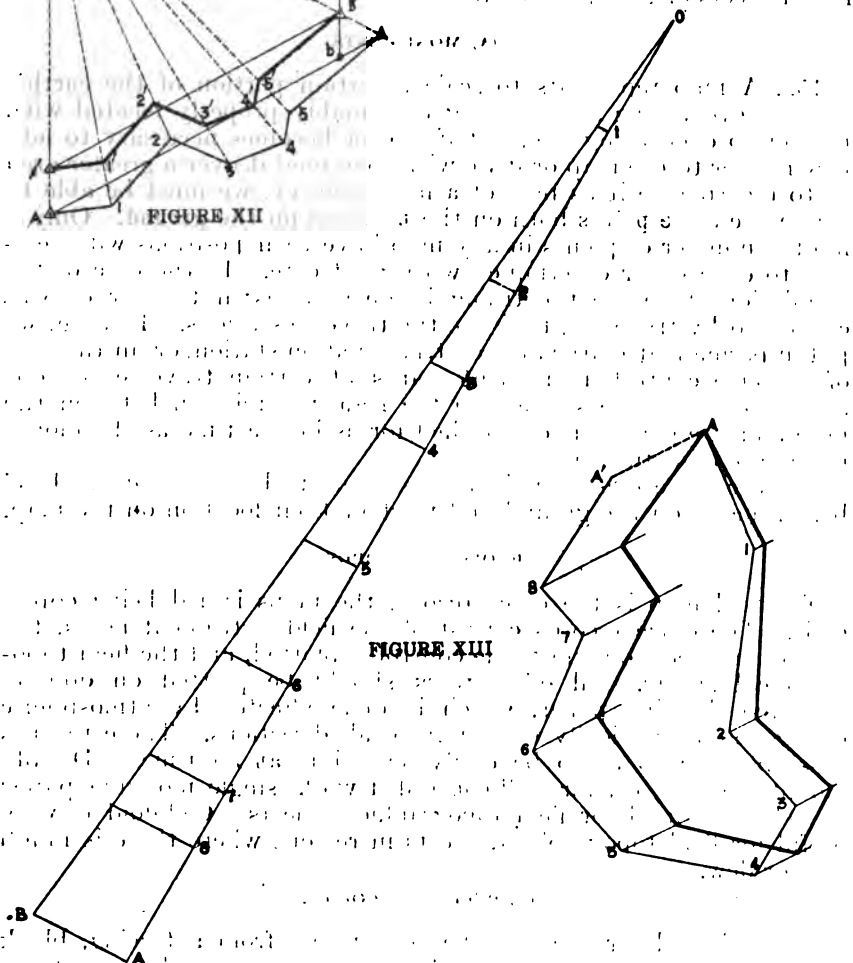


FIGURE XIII

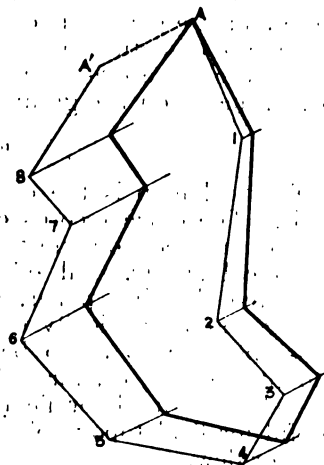
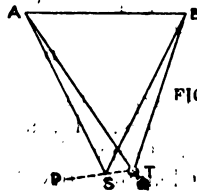


FIGURE XIV



## LESSON XXII.

## MONUMENTS, OFFICE RECORDS, AND DRAFTING.

151. Any properly made survey consists of three distinct parts. These are: (a) **Permanent marks or monuments on the ground**, (b) **complete records of the field work, properly filed**, and (c) **the published sheets or copies issued for use**.

## (A) MONUMENTS.

152. A map represents to scale a certain portion of the earth's surface, everything shown being presumably properly located with respect to everything else, but if it ever becomes necessary to add new matter to the map or if we wish to extend it over a greater area or to incorporate it as part of a larger survey, we must be able to locate the **same points both on the map and on the ground**. Only a limited number of points in any map have their positions with relation to each other determined with great care. In the case of triangulation these are the triangulation stations; if the survey was controlled by traverses, they are the traverse stations. If, then, we put in permanent marks at each triangulation station, or, in the case of traverse control, permanent marks at certain traverse stations and **also show these stations on the map**, the relation between the map and the ground is established for as long a time as the monuments are undisturbed.

For the same reasons it is also essential to leave *permanent level* bench marks on the ground and to show their location on the map.

## (B) OFFICE RECORDS.

The real map is the office record, the maps issued being copies of it. The office records consist of the field-instrument notes, the projection sheets on which the control is plotted, and the field topographical sheets. All office work should be plotted on double-mounted drawing paper, which is little affected by atmospheric changes and practically uniformly in all directions. These records must be filed so as to be easily accessible at all times. Double mounted paper, or, for well-controlled work, single mounted paper or vellum is used for field topographical sheets. Celluloid is very useful for field topographical sheets in regions where there is much rain or dew.

## (C) PUBLISHED COPIES.

Copies issued for use may be blue prints from a tracing, black prints from a paper negative, or lithographic copies. For any large issue the usual military practice will be to print from zinc plates. (*See Map reproduction.*)

## DRAWING.

153. The essential requirements of a good topographical drawing are *accuracy* and *clearness*. By accuracy is meant a faithful exhibit of measurements and observations made in the field, or of data taken from other maps. Clearness involves absence of confusion or crowding, and neatness in execution. *Beauty* and *pictorial effect* are ob-

tainable by skilled draftsmen only, and while always desirable, are rarely necessary. Persons who are not skilled draftsmen should not attempt pictorial effect, as it will detract from accuracy and clearness without substituting anything of equal value.

*Avoid unnecessary haste* in plotting and drawing. If possible, take time to check carefully all azimuths and distances plotted and be sure they are exact. There should be no approximation on the drawing board. Although an observer may have simply guessed a distance to be 550 yards in the absence of other information, the plotter should be careful to lay it down at exactly 550 yards.

Start with clean paper and keep it as clean as possible. In the office, wipe off the instruments before using, especially rulers, scales, and triangles. Dust the drawing carefully before beginning work. Dust again when stopping and cover with a cloth or paper. If necessary, dust the drawing and wash the hands occasionally while at work.

**Make all ink lines firm and very black.**—A drawing to be made in ink is usually drawn first in pencil, and in such cases a very hard pencil (4H or 6H) is best. If the pencil drawing is to be traced, a softer and blacker pencil should be used, but must be kept well pointed.

India ink in stick form gives the best results, but the time required for proper grinding precludes its extensive use in military field work. The prepared india inks in liquid form are ready for use and are satisfactory. They must be kept well corked when not actually filling a pen. If the ink gets thick in the bottle so that it will not run freely from a fresh-filled pen, add a little water.

**Papers.**—Manila paper of cream or buff tint, usually called *detail paper*, is suitable for sketches and drawings which are to be traced or used in the field. Only the better grade stands erasing, and that imperfectly. This paper comes in rolls 36, 42, and 54 inches wide. It may be ordered by the pound or yard.

White drawing paper may be had in rolls or sheets mounted on muslin or unmounted. Whatman's cold-pressed fine-grain is most generally useful. It comes in sheets of names and sizes as follows: Royal, 19 by 24 inches; Imperial, 22 by 30 inches; Double Elephant, 27 by 40 inches; Antiquarian, 31 by 53 inches. Roll papers are 27 to 63 inches wide.

Sheet papers unmounted and kept flat are best for field topographical use.

If a blot drops on the drawing, take a piece of blotting paper, tear a corner or edge to expose a fresh surface, and hold it in the blot without touching the drawing until the surplus ink is absorbed. Then press a dry blotter firmly on the spot and let it dry thoroughly before attempting to erase. A piece of newspaper may be used instead of blotting paper, but should be slightly moistened to hasten the absorption. For a large blot several pieces may be required.

**Erasers** for ink are of steel or rubber. A steel eraser or penknife must be very sharp to give good results. An eraser of gritty rubber is most generally used. It is best to use an erasing shield of thin metal or celluloid, which exposes the area to be erased through one of the openings and protects the rest.

*Tracing linen* is usually *dull back*, having one side glazed and the other dull. Erasing can be done on the glazed side only. The glazed side is used for ink and the dull side for pencil work. The glazed side requires preparation before use to remove excess of paraffin, which prevents ink from running well and clogs the pen. Rubbing hard with fresh blotting paper is the simplest method.

*Tracing paper* is alike on both sides. It will not erase. Most varieties are less transparent than tracing cloth.

In tracing, it is helpful to use a dull-pointed instrument in the left hand—a stylus or top of a penholder—to press the linen against the drawing at the point where the pen is resting.

#### ENLARGEMENT AND REDUCTION.

154. The simplest method is by squares. Divide the original into squares of 2 inches or less by lines drawn parallel to the borders. Divide the paper on which the copy is to be made into squares with sides corresponding to the same distance on the scale of the copy that the side of a square on the original itself does to the scale of the original. If a plotting scale of the original be placed on the side of a square on the original and the plotting scale of the copy on the side of a square of the copy the readings should be the same. The square on the copy will be larger if the drawing is to be enlarged and smaller if it is to be reduced. The ratio between the sides of the squares on the original and the copy is the ratio of reduction or enlargement. This ratio must not be confused with the ratio of areas of the two maps, which is different and not important.

Select a square of the original and reproduce its contents in the corresponding square of the copy, or take a feature of the original, as a road or stream, and trace its course through several squares.

Usually the position of a point in a square or on one of the sides can be *estimated* with sufficient accuracy. Important points may be located by measurement of distances from the nearest sides of the squares, using the scale of the map and the scale of the copy, respectively.

Instead of drawing the squares on the original, they may be drawn on tracing linen or paper laid over it, or fine threads may be stretched to form the squares. Every drawing board should have a scale of inches on each edge marked with fine saw-cuts or with small tacks to facilitate the drawing of squares.

#### CHARACTER OF WORK.

155. All lines must be clear, sharp, and distinct, drawn or printed in jet black, waterproof ink. Colors will not be used except when clearness of representation absolutely demands their use; special pains will be taken to avoid them in drawings intended for publication. So far as practicable, uniformity of size must be maintained in figures or letters presenting a particular kind of information, such as soundings, elevations, names of proprietors, names of minor towns, names of counties, etc., and figures and letters must be clear, distinct, and readily legible, especially on drawings intended for publication, in which case the letters and figures must be made of size large enough to avoid blurring and obscurity when reduced by

photolithography. The use of type for letters and figures and of films or rollers for representing typographic features is recommended.

The title should be placed in the lower right-hand corner, unless use of this space for other matter is absolutely unavoidable. If practicable, the size should not exceed 5 inches by 5 inches. The use of such words as "Map of," "Plan of" is thought to be unnecessary. The approval of the officer in charge will be placed near, and preferably at the side of the title. At the upper left-hand corner (and outside of the border, if a border is used) the words "War Department" will be placed; and at the upper right-hand corner, in similar position, the wording "Corps of Engineers, U. S. Army," will be placed. When the title is not placed as above, a brief title will be placed outside the border, on lower right-hand corner, to identify the drawing.

A graphical scale should be shown in all cases, and a statement of the scale may be added when useful. Drawings submitted for publication must be prepared with a view to reduction to the smallest practicable compass, and they must bear a statement in pencil, on the lower margin, of the amount of reduction contemplated. All maps are usually reduced at least one-third.

The true meridian should be shown on all maps or charts of land or water areas, if known, and the magnetic declination should also be given.

In the case of topographic or hydrographic surveys, a brief description should be placed upon the map or chart, in tabular form, of the principle triangulation points or bench marks, including the general location and character of the monuments or bench marks, the coordinates and the elevation. Whenever possible the direction of water flow of all waterways must be indicated by arrowheads pointing in the direction toward which the water moves. Tidal flow must be indicated by double or multiple arrowheads.

The following are the standard topographical symbols and styles of lettering to be used on all maps:

## ABBREVIATIONS.

|                           |                                 |                      |
|---------------------------|---------------------------------|----------------------|
| A.....Arroyo.             | G. S.....General store.         | Pt.....Point.        |
| abut.....Abutment.        | gir.....Girder.                 | q.p.....Queen-post.  |
| Ar.....Arch.              | G. M.....Gristmill.             | R.....River.         |
| b.....Brick.              | I.....Iron.                     | R. H....Roundhouse.  |
| B. S.....Blacksmith shop. | I.....Island.                   | R. R....Railroad.    |
| bot.....Bottom.           | Jc.....Junction.                | S.....South.         |
| Br.....Branch.            | k.p.....King-post.              | s.....Steel.         |
| br.....Bridge.            | L.....Lake.                     | S. H....Schoolhouse. |
| C.....Cape.               | Lat.....Latitude.               | S. M....Sawmill.     |
| cem.....Cemetery.         | Ldg.....Landing.                | Sta.....Station.     |
| con.....Concrete.         | L. S. S....Life-saving station. | st.....Stone.        |
| cov.....Covered.          | L. H....Lighthouse.             | str.....Stream.      |
| Cr.....Creek.             | Long.....Longitude.             | T. G....Tollgate.    |
| d.....Deep.               | Mt.....Mountain.                | Tres....Trestle.     |
| cul.....Culvert.          | Mts.....Mountains.              | tr.....Truss.        |
| D. S....Drug Store.       | N.....North.                    | W. T....Water tank.  |
| E.....East.               | n. f.....Not fordable.          | W. W....Water Works. |
| Est.....Estuary.          | P.....Pier.                     | W.....West.          |
| f.....fordable.           | pk.....Plank.                   | w.....Wood.          |
| Fi.....Fort.              | P. O....Post office.            | wd.....Wide.         |



Indicate character and span by abbreviations.



Meaning wooden king post bridge, 40 feet long, 20 feet wide, and 10 feet above the water.



Indicate character by abbreviations.



Meaning a stream 15 feet wide, 8 feet deep, and not fordable.

House =

Church =

School house = S.H.

Woods 

Orchards 

Cultivated Land 

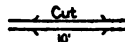
If boundary lines are fences they are indicated as such.

Brush, crops or grass, important as cover or forage 

Cemetery 

Trees, isolated 

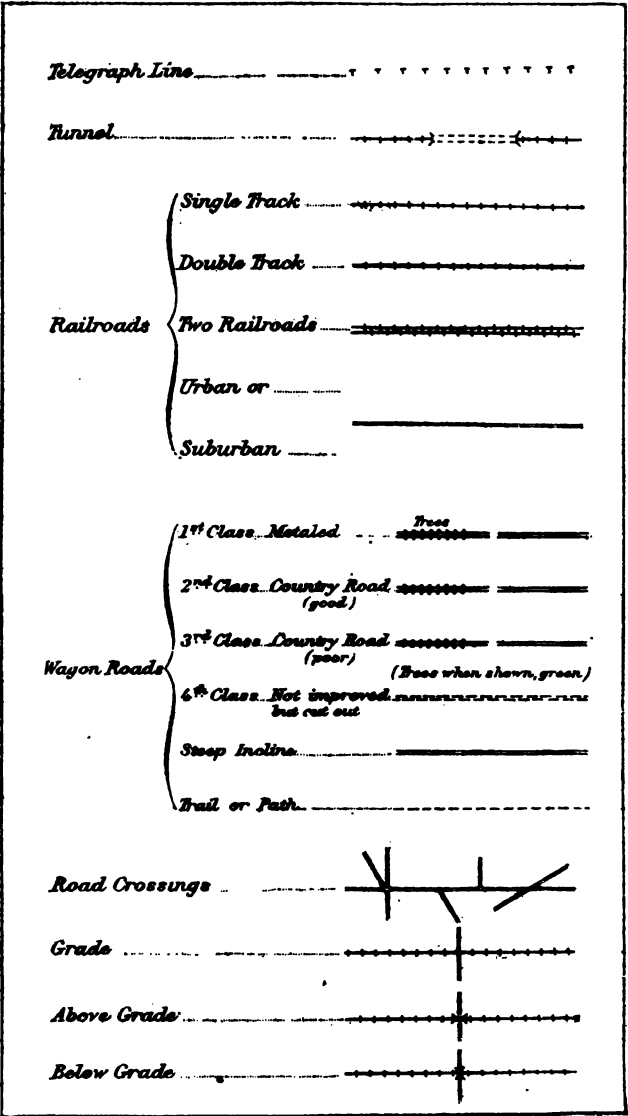
Cut and fill —




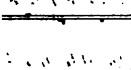






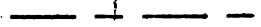
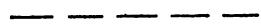
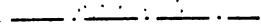

cut 10 feet deep




















fill 10 feet high





|  |  |
|--|--|
| <i>City or Village</i> _____             | <br>Pop. 2625             |
| <i>Capital</i> _____ ●                   | <i>County Seat</i> _____ ●   |
| <i>City or Village</i> _____ ●           |  |
| <i>Buildings</i> _____                   |                           |
| <i>Triangulation Station</i> _____       |                           |
| <i>Plane-table Station</i> _____         |                           |
| <i>Common Survey Station</i> _____       |                           |
| <i>Bench Mark</i> _____                  | <br>B.M.<br>1362          |
| <i>Mines and Quarries</i> _____          |                           |
| <b>BOUNDARY LINES</b>                    |  |
| <i>State Line</i> _____                  |                          |
| <i>County or Province</i> _____          |                         |
| <i>Township or Barrio</i> _____          |                         |
| <i>Reservation</i> _____                 |                         |
| <i>Lettering on Boundary Lines</i> _____ | <br>NEW YORK<br>VERMONT |

|  |   |
|--|---|
| Medical Corps  |    |
| Ordnance   |    |
| Signal Corps   |    |
| Engineer Corps                                       |    |
| Gun Battery  |    |
| Mortar Battery                                       |    |
| Fort   | <div> <div>True plan to be</div> <div>shown if known</div> </div>  |
| Redoubt  |   |
| Camp   |    |
| Battle   |    |
| Trench   |    |
| <b>OBSTACLES</b>                                     |   |
| <i>NOTE: When color is used execute these in red</i> |   |
| Abatis   |    |
| Wire Entanglement                                    |    |
| Palisades  |    |
| Contact Mines  |    |
| Controlled Mines                                     |    |
| Demolitions  |    |

  
 Pop. 2625

*City or Village* \_\_\_\_\_

*Capital* —●—    
 *County Seat* —●—    
 *City or Village* —●—

*Buildings* \_\_\_\_\_

*Triangulation Station* \_\_\_\_\_▲

*Plane-table Station* \_\_\_\_\_□

*Common Survey Station* \_\_\_\_\_○

*Bench Mark* \_\_\_\_\_
 BM  
1362

*Mines and Quarries* \_\_\_\_\_✕

### BOUNDARY LINES

















*State Line* \_\_\_\_\_










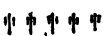




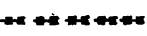



*County or Province* \_\_\_\_\_

*Township or Barrio* \_\_\_\_\_

*Reservation* \_\_\_\_\_


*Lettering on Boundary Lines* \_\_\_\_\_
 
 NEW YORK  
VERMONT

|  |   |
|--|---|
| Medical Corps  |    |
| Ordnance   |    |
| Signal Corps   |    |
| Engineer Corps                                       |    |
| Gun Battery  |    |
| Mortar Battery                                       |    |
| Fort   | <div> <div>True plan to be</div> <div>shown if known</div> </div>  |
| Redoubt  |   |
| Camp   |    |
| Battle   |    |
| Trench   |    |
| <b>OBSTACLES</b>                                     |   |
| <i>NOTE: When color is used execute these in red</i> |   |
| Abatis   |    |
| Wire Entanglement                                    |    |
| Palisades  |    |
| Contact Mines  |    |
| Controlled Mines                                     |    |
| Demolitions  |    |

|                                |        |   |
|--------------------------------|--------|---|
| <i>Regimental Headquarters</i> | -----  |    |
| <i>Brigade</i>                 | "----- |    |
| <i>Division</i>                | "----- |    |
| <i>Corps</i>                   | "----- |    |
| <i>Infantry in line</i>        | -----  |    |
| <i>Infantry in column</i>      | -----  |    |
| <i>Cavalry in line</i>         | -----  |    |
| <i>Cavalry in column</i>       | -----  |    |
| <i>Mounted Infantry</i>        | -----  |    |
| <i>Artillery</i>               | -----  |    |
| <i>Sentry</i>                  | -----  |    |
| <i>Vidette</i>                 | -----  |    |
| <i>Picket, Cav. and Infy.</i>  | -----  |  |
| <i>Support</i>                 | "----- |  |
| <i>Wagon train</i>             | -----  |  |
| <i>Adjutant General</i>        | -----  |  |
| <i>Quarter-master</i>          | -----  |  |
| <i>Commissary</i>              | -----  |  |

*Gage of Letters*  
(in Decimillimeters)

|  |    |
|--|----|
|  | 5  |
|  | 6  |
|  | 7  |
|  | 8  |
|  | 9  |
|  | 10 |
|  | 12 |
|  | 13 |
|  | 14 |
|  | 15 |
|  | 18 |
|  | 20 |
|  | 22 |
|  | 25 |
|  | 30 |
|  | 35 |
|  | 40 |
|  | 45 |
|  | 50 |
|  | 55 |
|  | 60 |

*Thickness of letter  $\frac{1}{4}$  of height.*  
*Slope of letter 3 parts of base to 8 of height.* 

**HYP SOGRAPHY**

*Mountains, Plateaus, Lines of Cliffs  
and Canyons (all capital letters)*

ABCDEF GHIJKLMN OPQRSTU  
VWXYZ

*Peaks, small Valleys, Islands and Points  
(with Cap. initials)*

ābcdefghijklmnopqrstu vwx yz

**PUBLIC WORKS**

*Railroads, Tunnels, Bridges, Ferries, Wagon-roads,  
Trails, Fords and Dams (capitals only)*

ABCDEF GHIJKLMN OPQRSTU VWXYZ

**CONTOUR NUMBERS**

*Heavy contours 1234567890*

*Light contours 1234567890*

**MARGINAL LETTERING**

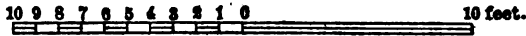
ABCDEF GHIJKLMN OPQRSTU  
VWXYZ

*(with Cap. initials)*

ābcdefghijklmnopqrstu vwx yz

1234567890

1<sup>st</sup> R. F. —  $\frac{1}{100}$  — 8.33 to 1" — 633.6 to 1 mile.



2<sup>nd</sup> R. F. —  $\frac{1}{120}$  — 10' to 1" — 528" to 1 mile.



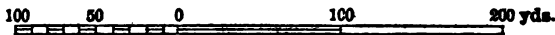
3<sup>rd</sup> R. F. —  $\frac{1}{500}$  — 41.66 to 1" — 126.7 to 1 mile.



4<sup>th</sup> R. F. —  $\frac{1}{600}$  — 50' to 1" — 105.6 to 1 mile.



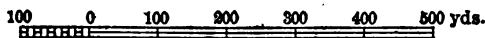
5<sup>th</sup> R. F. —  $\frac{1}{4224}$  — 352' to 1" — 15" to 1 mile.



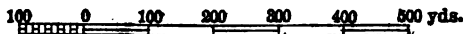
6<sup>th</sup> R. F. —  $\frac{1}{5280}$  — 440' to 1" — 12" to 1 mile.



7<sup>th</sup> R. F. —  $\frac{1}{10000}$  — 833.3 to 1" — 6.34 to 1 mile.

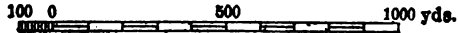


8<sup>th</sup> R. F. —  $\frac{1}{10560}$  — 880' to 1" — 6" to 1 mile.

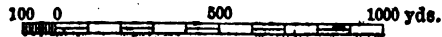




$$9^{\circ} \text{ R. F.} = \frac{1}{20000} = 1666.7 \text{ to } 1'' = 3.17 \text{ to } 1 \text{ mile.}$$



$$10^{\circ} \text{ R. F.} = \frac{1}{21120} = 1760' \text{ to } 1'' = 3.00 \text{ to } 1 \text{ mile.}$$



$$11^{\circ} \text{ R. F.} = \frac{1}{52800} = 4400' \text{ to } 1'' = 1.2 \text{ to } 1 \text{ mile.}$$



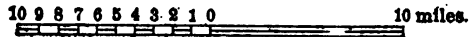
$$12^{\circ} \text{ R. F.} = \frac{1}{63360} = 5280' \text{ to } 1'' = 1.00 \text{ to } 1 \text{ mile.}$$



$$13^{\circ} \text{ R. F.} = \frac{1}{126720} = 10560' \text{ to } 1'' = 0.50 \text{ to } 1 \text{ mile.}$$

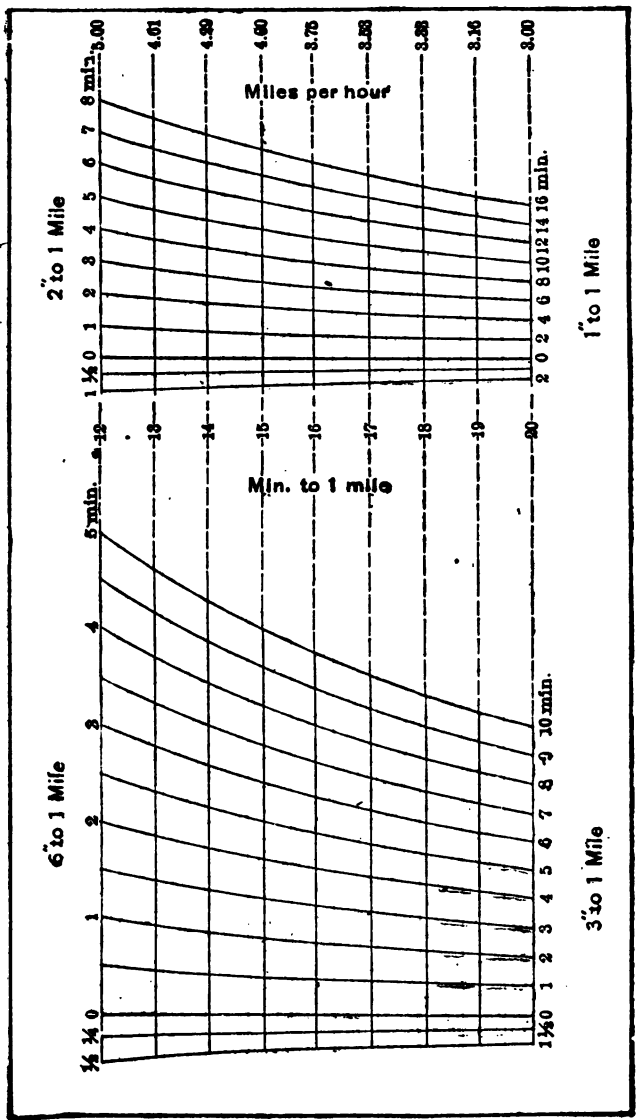


$$14^{\circ} \text{ R. F.} = \frac{1}{633600} = 52800' \text{ to } 1'' = 10 \text{ miles to } 1''.$$



$$15^{\circ} \text{ R. F.} = \frac{1}{1584000} = 132000' \text{ to } 1'' = 25 \text{ miles to } 1''.$$





impression on the zinc plate. Absolute contact between plate and negative is most important and consequently the printing frame and glass are heavy and considerable pressure is applied. While the sensitized plate is affected by light, it is entirely practicable to carry out the above-mentioned operations without hurry in the light of an ordinary room, without damage to the plate. It is only really sensitive to the rays of sunlight or intense artificial light.

The plate is now exposed to sunlight or artificial light and by this action the albumen reached by the light rays is rendered insoluble in water, while that not so acted upon remains soluble. The time of exposure is dependent upon so many conditions that it must be arrived at by a beginner by experiment. As a guide it may be stated that a zinc plate sensitized as above and exposed under a perfect negative to the rays of the sun during July and August between 10 in the morning and 3 in the afternoon in the central part of the United States will take a 1½-minute exposure if the drawing to be produced consists of ordinary heavy lines.

After exposure the plate is taken from the frame and laid on a level surface and immediately rolled up with etching ink. The surface upon which the plate is laid must be absolutely a plane or distortion will result. An ordinary lithograph stone makes a most excellent bed for this purpose, but a heavy block of wood with care may be made to serve. The exposed plate is evenly coated with the etching ink, rolling it up in two directions at right angles to each other. Very little ink is used and the yellow of the film should always show through the ink.

Etching ink is a trade preparation resembling ordinary black lithographic ink, but it has a greater proportion of resinous material and less coloring matter. A very small quantity, about as much as can be placed on a 5-cent piece, is worked up with the mixing knife and then spread upon the ink slab (which must be plane surface) and rolled out with the roller until both slab and roller show an even coating of ink. If the ink is too hard to work up it may be thinned with a drop of aniseed oil, but great care must be used to thin the ink only enough to make it work, otherwise it will not have sufficient body when applied to the plate. Rollers must be frequently washed with turpentine to keep in proper condition.

The preparations for applying etching ink are supposed to have been made prior to exposing the plate, as any delay in working up the plate should be avoided.

We now have a zinc plate covered with a dichromatized albumen film, portions of which, corresponding to the lines, etc., on the original drawing, have been rendered insoluble in water by the action of light. The whole surface has then been given a coating of ink. The plate is now washed, rubbing the surface gently with a tuft of cotton. If the plate has been correctly exposed, the albumen corresponding to the whites of the original drawing will be readily removed, taking with it the ink, and there will be left the reverse of the drawing in ink lines on an otherwise clean zinc plate. If the plate has been underexposed the lines will begin to disappear early in the washing and another plate with longer exposure should at once be tried. If overexposed the ink will smear over the plate and the whites will not come up. A slight overexposure may sometimes

be corrected by adding a few drops of stronger ammonia to the water in the washing tray.

As the zinc plate will usually be larger than the negative used in exposure the outer edges will have been exposed and rendered insoluble and will show a black frame around the reproduction. This must be removed by scrubbing with pumice stone and a cotton tuft.

Take the plate from the tray and dry it by patting it with a damp chamois skin; do not wipe it as the lines may smear. Look carefully over the reproduction, and if there are any lines missing paint them in by means of a little etching ink moistened with turpentine and applied with a red sable brush. Also remove any unnecessary ink spots on the plate. Be careful in this work not to touch the plate with the arm or hand for fear of smearing.

From this point on the development of the plate is the same as in the autographic process and will not be again described.

#### PRINTING FROM ZINC PLATES.

160. While the plates have been etched so as to give the image a slight relief the main principle involved in the printing from zinc plates is that "grease attracts grease and is repelled by water."

The gummed plate, having dried, is wiped over with a damp rag to remove surplus dry gum. After that it is gone over before each rolling up with a rag moistened in water with a little dextrin in it to keep the plate from drying too rapidly. The proper proportion is usually obtained by taking about one part of the solution for gumming plates and mixing it with eight parts of water.

A small portion of lithographic ink is thoroughly worked up with an ink knife. (This ink slab may be a piece of polished marble or a lithographic stone.) The ink is then thoroughly distributed by the roller. Never put ink directly upon the roller. Do not put varnish in the ink, but be careful to have the roller saturated with varnish.

The roller being now inked up, the plate, which must be on a perfect plane surface, is wiped over with the damp rag (dextrin mixture), and the roller is passed once over and back, quickly if the ink is soft and liquid, slowly if the ink is very stiff. The gummed portion of the plate takes moisture from the rag and will reject the greasy ink upon the roller. The lines being greasy reject the wetting and take the ink. When first working up a plate it should be inked and wiped several times, and it may then be necessary to make a half dozen impressions before a satisfactory one is secured. If an ordinary sliding contact hand press is used, the plate can be inked on whatever is used as the bed of this press. If the clothes-wringer press is used, a separate surface will have to be provided for inking up the plate. To get an impression the paper is laid upon the plate immediately after rolling up, it is passed through the press, and when taken off it will show the impression.

Avoid flat and glossy paper for printing purposes. If you have to use it fan the plate dry after each rolling up or the paper will stick.

If in rolling up some of the whites take ink, it is because, due to carelessness, the entire plate was not covered in the wiping with the damp rag. Go over it again with the damp rag and then give it a very quick roll and the ink will be removed. If the plate blocks up

and the lines of the impression become blurred, gum the plate with a rather thick solution of dextrin, and, while the dextrin is still liquid, wash off the plate with turpentine, being careful that no pressure is exerted upon the lines. The ink being removed keep the plate for several minutes under running water in order to remove the turpentine. Then gum up with the ordinary solution of dextrin and let the gum dry. The plate prepared in this way can be kept for years.

There is almost no limit to the number of impressions that can be obtained from the good plate which is taken proper care of. In the choice of papers to be used, some discretion is necessary if very particular results are to be obtained, and the papers should be selected after experiment has established their suitability.

*Direct methods.*—It may not always be practicable to make a brown print negative of the drawing to be reproduced, owing to lack of paper, nor may it be possible to make and strip a photographic negative. The reproduction can be made directly from a tracing, or if the drawing be on opaque paper this may be rendered translucent by the application of "banana oil," or a mixture of 3 parts castor oil and 10 parts alcohol. The impression on the zinc plate may be obtained by one of the following methods:

(a) 1. Prepare sensitizing solution:

|                           |           |
|---------------------------|-----------|
| Albumen.....              | 1 oz.     |
| Water.....                | 6 oz.     |
| Ammonium bichromate.....  | 27 grams. |
| Ammonia, 28 per cent..... | 6 drops.  |

2. Sensitize a polished plate by "flowing" twice with the solution.
  3. Dry by whirling over heat, being careful not to heat plate any more than is absolutely necessary.
  4. Let plate cool.
  5. When printing from tracing, give 40 seconds at 8.30 a. m., with good sunlight, decreasing time as sun gets stronger so that by 10.30 a. m. time will be from 25 to 30 seconds.
  6. When printed, roll up with stiff etching ink. Put on thin coat of ink and smooth out with smooth leather roller. Ink and roller should be free from dust, or pin holes will result.
  7. Place plate under water tap until all lines are clear. Going over surface with a tuft of cotton while holding under tap will assist in removing ink from lines.
  8. Immerse four seconds in solution of 2 ounces nitric acid to 3 gallons water.
  9. Remove from solution and wash thoroughly to remove acid.
  10. Dry plate by patting with chamois skin. Dry back of plate with rag.
  11. Warm slightly over stove to complete drying of lines.
  12. Roll up with the same etching ink, using "composition" roller. Put on medium coat of ink and roll into lines with smooth leather roller, or by continued rolling with composition roller without the addition of any more ink.
  13. When lines show black through coating of ink place plate in a 10 per cent solution of 28 per cent acetic acid and water. Rock tray for one or two minutes, then start removing ink from ground of plate by dragging medium-sized tuft of cotton over surface. Plate should be clear in five to seven minutes.
  14. When clean remove and rinse, then dry by whirling over heat, let cool, then powder up, burn in, etch, and print as usual.
- (b) 1. Expose a sensitized zinc plate under the drawing.
2. Develop in the usual manner. This gives white lines on a black ground.
  3. Etch the plate long enough in the nitric acid bath to give a slight depth to the lines.
  4. Wash and dry.
  5. Rub ordinary asphaltum paint into these etched lines and dry.

6. Scour whole surface of plate with charcoal stick. The lines which contain the asphaltum paint, being deeper than the remainder of the plate, are not affected by the charcoal stick. Thus there is obtained a polished plate bearing the impression in depressed lines filled with asphaltum paint.
  7. Etch the plate again. This takes down the whites and leaves the asphaltum lines in relief.
  8. Gum up and dry, ready for use.
- Excellent results may be obtained by this method, which, however, takes a little longer than when using a negative, on account of the time required to scour the plate.

**Field expedients.**—It is entirely possible that work which will give satisfactory rough results in the field can be done with a much reduced apparatus. For instance, it has been found that impressions can be gotten without the press by simply laying the paper on the inked zinc plate and passing a rubber roller over it so as to press upon all parts. There is a tendency for the paper to shift and give a blurred impression, but this can be sufficiently avoided by a little care, thus disposing with the press.

It has also been found that a satisfactory exposure can be made by placing the negative upon the sensitive side of the zinc plate, fastening it in any convenient manner, then bowing the sensitive side of the plate to the front, which will stretch the negative and give fair contact. During exposure the plate must be so moved as to give all portions an even illumination. The above are, of course, makeshifts and will not give such results as are usually desired, but they may save the day in an emergency.

**Negatives.**—If the original be a tracing the best negative is a brown print. This negative is made in the usual manner on thin paper and is placed brown face down upon the zinc plate.

**Photographic negatives:** 1. Make the usual photographic negative on a "stripping" plate, strip off and place, reversed, upon a clear plate. To print on the zinc plate, place film side down, thus giving reversed impression. 2. Expose a "process" photographic dry plate in the camera backward—that is, with the emulsion side away from the lens, correcting the focus for the thickness of the plate. Develop as usual. To print on the zinc plate, place emulsion side down. 3. The most satisfactory method of producing photographic negatives for lithographic work is the "wet-plate" process. This, however, is not adapted to field purposes. 4. The cameragraph: This apparatus will make at a single operation a positive negative brown print by which to transfer any drawing to a zinc plate. It consists of a copying board on which to place the map or drawing to be reproduced, a camera fitted with a reversing prism, and special attachments for carrying a roll of brown print paper, a developing and a fixing bath. To produce a negative, sufficient paper therefor is fed down from the roll into the focal plane and the exposure made. By means of a mechanical attachment this exposed piece is cut off the roll and is then fed through the developing and fixing tanks, removed, and dried. Full directions for operation come with the cameragraph.

## PART II.

### DETERMINATION OF AZIMUTHS.

161. The compass is the standard instrument for the determination of azimuths in topographical reconnaissances. It consists of case, needle, dial, pivot, and stop.

The dial may be fixed to the case or it may be movable, that is, moving with the needle to which it is attached. The stop raises the needle from the pivot and clamps it against the glass cover. A good compass must have a needle sufficiently magnetized to settle accurately and a pivot which is true. If the needle becomes too weak, it may be remagnetized by rubbing gently from pivot to point on a permanent or electromagnet, each end of the needle to be rubbed on the pole of the magnet which attracts it. In returning the needle for another stroke, carry it a foot or more from the magnet. The pivot may be polished with Putz pomade or a similar substance on a soft stick. If possible, turn in a defective compass and get one in its place.

A needle loses part of its magnetism if kept for a long time out of the plane of the magnetic meridian. In storing a compass, therefore, care should be taken to see that the needle is in the magnetic meridian with the N. end of the needle pointing north.

A symmetrical needle tends to point downward toward the nearer magnetic pole of the earth. This displacement from the horizontal is called dip, and is measured in degree of arc. Immediately over the magnetic poles the needle stands vertically or has a dip of  $90^\circ$ . Near the Equator, where North and South Poles of the earth exert an equal influence, the needle will be horizontal, or the dip 0.

For reading azimuths the needle must be kept in a horizontal plane, which is done by a small movable counterweight (to overcome the dip). For considerable changes in latitude, as in passing from the United States to the Philippines, the counterweight will require adjustment to keep the needle horizontal, and in passing from the Northern to the Southern Hemisphere, the counterweight must be changed to the other end of the needle.

There are two adopted forms of compass for topographical reconnaissance, one in which the dial is fixed to the case and one in which the dial moves with the needle to which it is fixed.

### THE BOX COMPASS.

162. The dial or face on which the graduations are marked is rigidly attached to the case. The type of box compass best adapted to running courses by azimuth is constructed as follows: The graduations read counterclockwise continuously from 0 to  $360^\circ$ ; the instrument reads 0 when pointing south and  $180^\circ$  when pointing north; the E. and W. points, if marked, are reversed.

To determine the azimuth of a line point the north and south line of the case along the line (the north point away from the observer) and read the N. end of the needle. The dial is graduated to single degrees, but when the needle is stationary the reading can be estimated to half degrees.

Many box compasses are not graduated in the manner above described. To use such compasses for azimuth reading they should

be altered to conform to the conditions cited. This is ordinarily done by pasting paper over the stamped numbers on the dial and renumbering in ink or pencil.

#### THE PRISMATIC COMPASS.

163. The dial containing the graduations is attached to the needle and moves with it. It is read by means of a small prism, adjustable for focus. This prism is mounted on a hinge joint and can be turned down for carrying. The line of sight of the instrument is determined by front and rear sights, which fold down when not in use, at the same time stopping the needle. The needle may be compensated for dip by a bit of sealing wax on the under side of the dial card. The graduations on the dial should be numbered so as to read azimuths, as above described, beginning at the south point. If the graduations are not so numbered, they should be altered as follows: The zero should be at the north end of the needle (which is on the under side of the dial) and the graduations should run clockwise continuously to 360°. It is to be noted that with such numbering the instrument will not read azimuths if used as a box compass. The index is a point on the case, and as the dial is movable the graduations are numbered clockwise, instead of counterclockwise, as in the box compass. Readings should be made through the prism.

To determine the azimuth of a line with this instrument, adjust the prism until the graduations on the dial are distinct, raise the front sight; look through the slit in the prism plate and bring the front sight in line with the forward station; when the needle comes to rest, read the azimuth through the prism.

#### COMPASS ERRORS.

164. The magnetic and the true meridian generally do not coincide. The angle between them at any point is called the **magnetic declination at that point**. If the needle points east of the true meridian, it is called an **east declination**; if west, a **west declination**. Magnetic declination varies in amount and direction at different points on the earth. The figure facing par. 166 (p. 80) is a chart, called an **isogonic chart**, which for the epoch gives, by curved lines connecting points of equal declinations, the approximate declination of points on the earth. **At no point is the declination constant**. It is subject to the following variations: The **daily variation** consists of a swing from the extreme easterly position at about 8 a. m. to the extreme westerly position about 1.30 p. m.; the mean position occurring about 10 a. m. and 5 p. m. The **daily variation** is from 5' to 15' of arc. The **secular variation** is a long slow swing, covering many years. In the United States all **east declinations** are now gradually decreasing and all **west declinations** gradually increasing at the rate of about 3' per year. The **annual variation** is very small (less than 1' per year) and need not be considered in surveying work. The **Lunar declination** is still smaller. All of the foregoing variations are periodic in character. **Irregular variations** due to so-called magnetic storms are uncertain in character and can not be predicted. Such variations are sometimes large. **Local attractions** may greatly disturb the needle, and often come from unknown sources. The



observer should have them constantly in mind and endeavor to keep all magnetic influences, such as magnetic bodies, electric wires, etc., at a distance from the instrument when the needle is being read.

The geometric axis of a needle may not coincide with its magnetic axis, hence the readings of two compasses at the same station may differ slightly.

165. A simple way to detect—not measure—such disturbances is to take frequent back azimuths. If the position of the needle is normal at both stations, the azimuth and back azimuth will differ by  $180^\circ$ . If there is local attraction on the course, it will usually be stronger or cause a greater deflection at one station than at the other, and the azimuth and back azimuth will not differ by  $180^\circ$ .

Another way is, when taking the bearing to a station, to select a well-defined point beyond and on the same course. On arriving at the new station take a bearing from there to the selected point ahead. If it is the same as the first bearing to that point, there probably is no local disturbance. If the two bearings to the same point differ, there probably is local disturbance.

Corrections for abrupt deflections of the needle due to local attractions must not be distributed uniformly over the traverse. A course in which local attraction is detected or suspected should be noted, and if, on closing, an azimuth correction is necessary, it should be applied to the suspected courses.

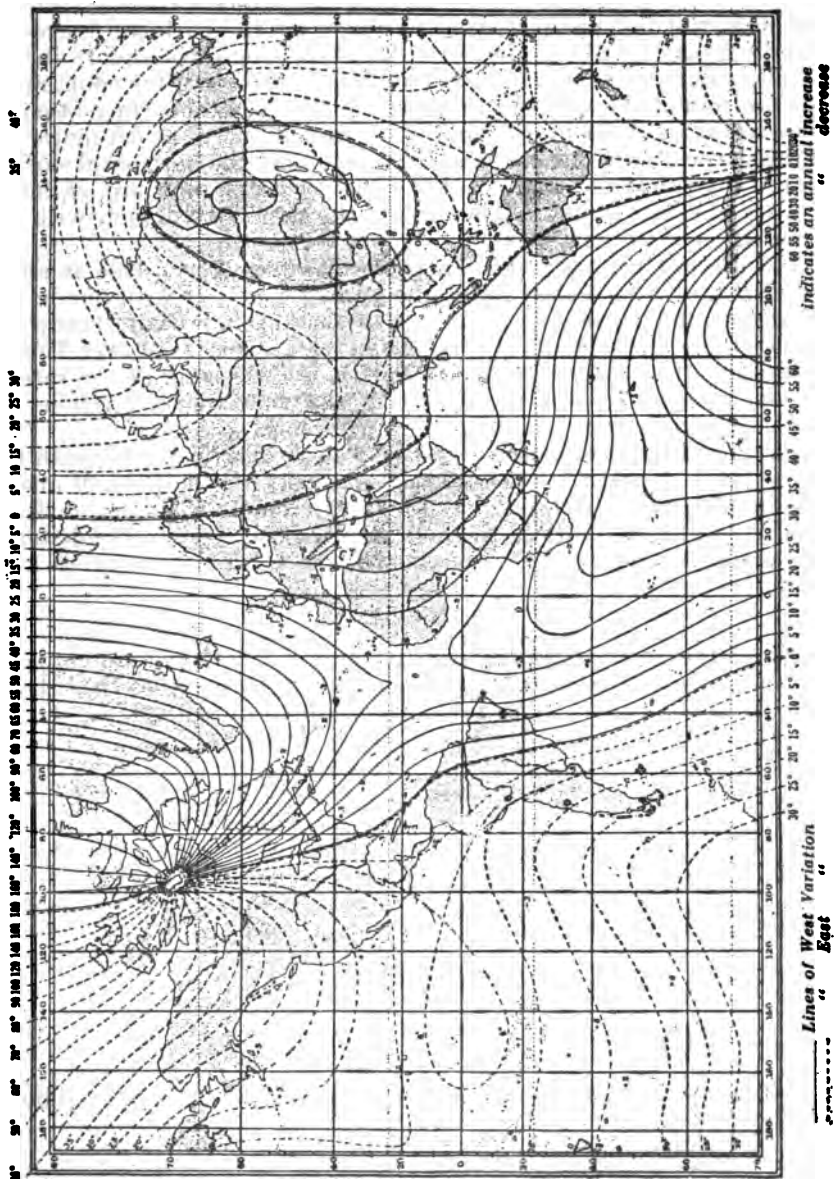
#### USE OF COMPASSES.

166. A good needle requires time to settle, even when the case is firmly supported, and the user should cultivate the knack of catching it at the middle of its swing, which is the desired reading. If the compass can be supported, it is always better to do so. Then the sight can be carefully taken and the position of the eye changed to read the needle. Wait till the swing gets down to  $4^\circ$  or  $5^\circ$ , which it will usually do in a few seconds. Then catch the highest and the lowest readings on the same swing and take their mean for the true reading. If the first swings are very large, catch the needle with the stop near the middle of the swing and release it quickly. This will suddenly check the swings and shorten the time in which the reading can be taken.

In using the box compass without a support, hold it sufficiently below the eye so that the swing of the needle can be seen. Point the line of sight in the required direction, catch the needle with the stop in the middle of the swing, and hold it stopped until the reading is taken. Stop readings are less accurate than sight readings, due to the difficulty in stopping the needle at the middle of the swing and to the tendency to displace the needle slightly in lifting it off the pivot. When the stop is used, press it firmly and quickly.

With the prismatic compass the stop is not used except to check the swings. Utilize a support if practicable. The prism having been adjusted for focus, level the case so as to bring the scale into focus, and when the swing becomes small read the extremes and take the mean.

**APPROXIMATE ANNUAL CHANGE IN MINUTES OF ARC.**



TO DETERMINE THE DECLINATION OF THE COMPASS.

167. **First method; from the sun.**—Prick a small hole in a piece of tin or opaque paper and fix securely over the south edge of a table or other surface perfectly level, so that the sunlight coming through the hole will fall on a convenient place on the surface, figure 15. The hole may be 2 feet above the table for long days and 18 inches for short ones. Half an hour before to half an hour after noon, mark the position of the spot of sunlight on the horizontal surface at equal time intervals of about 10 minutes. Draw a curve, as *bd*, figure 15, through the points marked, and from point *c* in the horizontal surface and in a vertical line with the hole, *a*, sweep a circular arc, *ef*, intersecting *bd* in two points. The form of the curve *bd* will vary with the declination of the sun.

168. **Second method; from Polaris.**—The true North Pole is about 1 12' distant from Polaris on a line joining that star with one in the handle of the dipper, and another in Cassiopeia's chair, figure 16. One of these stars will always be above the horizon, wherever Polaris is visible. The polar distance of Polaris is decreasing at the rate of 19'' per year. It also varies during the year by as much as 1'. Both variations may be neglected in this work.

Imagine Polaris to be the center of a clock dial, figure 16, with the line joining 12 and 6 o'clock vertical and with the position of one of the lines described (from Polaris to star in handle of dipper, or from Polaris to star in chair) as the hour hand of the clock. The distance in angular distance of Polaris from the true north may be taken from the following table:

TABLE I.

169. **Table showing the angular distances of Polaris in different positions with respect to the pole.** Epoch 1911; polar distance 70'. Latitude 0° to 18° north. This table may be used until 1930.

| Clock reading of— |              | Angular distances. | Clock reading of— |              | Angular distances. |
|-------------------|--------------|--------------------|-------------------|--------------|--------------------|
| °Cass.            | Z Ursae Maj. |                    | °Cass.            | Z Ursae Maj. |                    |
| XII:30            | VI:30        | E 18               | VI:30             | XII:30       | W 18               |
| I                 | VII          | 35                 | VII               | I            | 35                 |
| I:30              | VII:30       | 49                 | VII:30            | I:30         | 49                 |
| II                | VIII         | 61                 | VIII              | II           | 61                 |
| III               | IX           | 70                 | IX                | III          | 70                 |
| III:30            | X            | 61                 | X                 | III:30       | 61                 |
| IV                | X:30         | 49                 | X:30              | IV:30        | 49                 |
| V                 | XI           | 35                 | XI                | V            | 35                 |
| V:30              | XI:30        | 18                 | XI:30             | V:30         | 18                 |

For higher latitudes multiply the tabular readings by the following:

|                          |      |
|--------------------------|------|
| Latitude 19° to 30°..... | 1. 1 |
| Latitude 31° to 37°..... | 1. 2 |
| Latitude 38° to 42°..... | 1. 3 |
| Latitude 43° to 46°..... | 1. 4 |
| Latitude 47° to 50°..... | 1. 5 |
| Latitude 51° to 53°..... | 1. 6 |
| Latitude 56° to 57°..... | 1. 7 |
| Latitude 58° to 59°..... | 1. 8 |
| Latitude 60° to 61°..... | 1. 9 |

170. It is well to keep track of the position of Polaris by noting it frequently and taking the corresponding clock time. Then, if on a cloudy night a glimpse of Polaris is had, the observation may be taken, even though the other stars can not be seen.

171. For practical details of the observation, the following may serve as a guide: Select a clear space of level ground not too near buildings or any other object which might cause local disturbance of the needle. Drive a picket, leaving its top smooth and level, about 18 inches above the ground. Six feet north of the picket suspend a plumb line from a point high enough so that Polaris, seen from the top of the picket, will be near the top of the line, figure 17. The cord should be hard and smooth, about one-tenth inch in diameter. The weight at the bottom of the line should hang in a vessel of water or in a hole dug in the ground to lessen its vibration. Drive a second picket in range with the first one and the plumb line a short distance north of the latter. Make a peep sight by punching a hole one-tenth inch in diameter in a piece of paper and hold it on the top of the first picket; adjust it so that the star is behind the plumb line when looking through the peep. Note the position of one of the stars on the imaginary clock face at the moment the observation is taken. Mark the position of the peep on the top of the first picket and lay a straightedge or stretch a cord from that point touching the plumb line to the second picket. Place the north-and-south edge of the compass box against the cord or straightedge and read the needle.

The compass azimuth read is the magnetic azimuth to Polaris at the instant of observation. To find the magnetic azimuth of the true meridian, correct the compass reading by the angular distance of Polaris as given in Table I, adding the correction if marked W; subtracting, if marked E. This method will give results true to within one-fourth of a degree.

From an examination of the table it will be seen that when either S, Cass, or Z Ursae Major are at XII or VI, no angular distance is given. At these times, Polaris is on the true meridian and the magnetic azimuth to Polaris is the true azimuth. For a rough check on the magnetic declination, an observation on Polaris, taken when either the dipper or Cassiopeia is above the pole (near 12 o'clock on the imaginary clock dial) will give the magnetic azimuth of the true meridian direct to within less than the least reading of the ordinary compass.

#### THE SEXTANT.

172. This instrument is shown and its parts indicated in figures 18 and 19. The former is a very compact form, called the pocket sextant. The larger form, figure 19, has telescopes of different powers and also a telescope tube without lenses, which is used for reconnaissance work at short ranges. The pocket sextant has a telescope for use in astronomical and long-range terrestrial work. For ordinary reconnaissance and surveying, the pocket sextant is used without the telescope, the sight being taken through a small hole in a shutter which closes the telescope opening.

The adjustments are as follows: For the index glass, place the vernier at about  $30^\circ$  of the limb and examine the arc and its image in the index glass. If the arc and image appear continuous, the glass is in adjustment. If the image appears above the arc, the mirror

leans forward; if below, it leans backward. Adjust with screws if provided, or with slips of paper inserted between the mirror and its frame.

**For the horizon glass.**—Set at zero and observe a well-defined distant point, using the telescope. If the direct and reflected images coincide, the horizon glass is in adjustment. If not, adjust it until

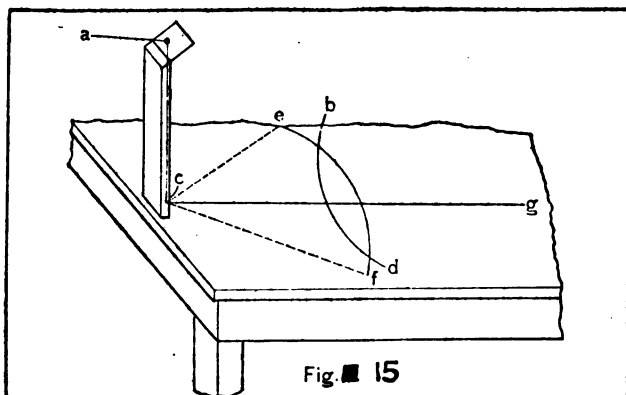


Fig. 15

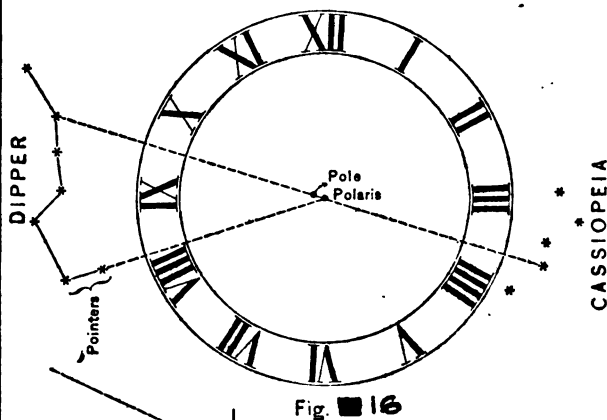


Fig. 16

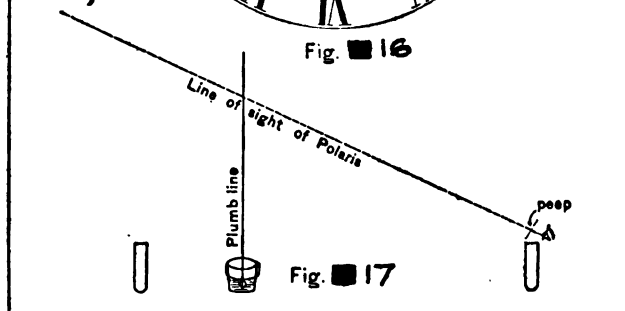
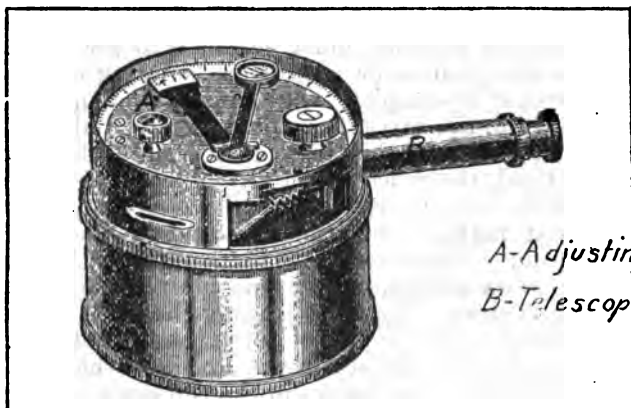


Fig. 17

they do, or if that can not be conveniently done, move the arm a short distance from zero until coincidence occurs. Read the vernier and apply that reading with its proper sign to all angles measured. Such a reading applied as a correction is called the **index error**. If

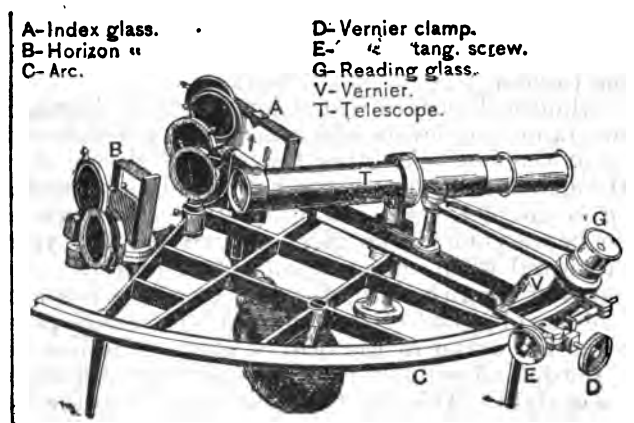
the index error is off the arc, that is, between zero and the end, it is additive. If on the arc, subtractive.

In the pocket form the horizontal glass only is adjustable. To adjust the pocket sextant, select a distant object with a clearly defined straight outline. Set the vernier carefully at the zero of the arc and look at the object through the peephole and the lower portion of the horizon glass. Turn the sextant about the line of sight



*A-Adjusting key*  
*B-Telescope tube*

*Fig. 18 Pocket Sextant*



A-Index glass.  
B-Horizon "  
C-Arc.

D-Vernier clamp.  
E-" tang. screw.  
G-Reading glass.  
V-Vernier.  
T-Telescope.

*Fig 19*

as an axis until the straight line appears to be perpendicular to the straight bottom edge of the horizon glass. If the instrument is not perfectly adjusted for this position, the straight line of the observed object will appear broken, in which case unscrew the smaller milled head A of the top plate, and using its small end as a key, turn the single adjusting screw in the cylindrical surface while looking at the object through the peep. The part of the image seen in the mirror will appear to move, and by turning the key in the

proper direction the two parts may be brought together. Next turn the sextant about  $60^\circ$  about the line of sight, and if the straight line again appears broken, use the key to slightly loosen one of the two adjusting screws in the top plate while looking through the instrument. If this brings the two parts nearer in line, the proper screw has been selected; if not, try the other one. Then turn the two adjusting screws in the top plate by corresponding amounts and in opposite directions and continue turning them alternately till the straight line becomes continuous. The two screws are opposed to each other, and care must be taken to use no considerable force and to always unscrew one before screwing up the other. When the adjustment is complete, the line should remain continuous and straight while the sextant is slowly revolved about the line of sight. If the index arm is then moved back and forth by turning the large milled head, the reflection of any object may be made to pass exactly over that object as seen through the clear glass.

**For adjusting at night,** screw the telescope in place. Pull its inner tube well out. Remove the sunglass from the eyepiece. Focus the telescope on a bright star by pushing in the tube till the image of the star is clear. Then, by turning the large milled head, make the star's reflected image pass through the field of view. If it does not pass exactly over the stationary image of the star, adjust the horizon glass with the two screws in the top plate till one image will pass exactly over the other. Next set the vernier accurately to the zero of the arc, and with the single adjusting screw in the cylindrical surface make the two images appear as one. The instrument is then completely adjusted. The daylight method is most convenient, but it is well to test the adjustment by the star method before attempting to do any astronomical work.

In the cylindrical surface just below the zero degree end of the arc are two projecting levers which move colored glasses to be used in looking at the sun. At other times these glasses should be depressed through the opening in the bottom plate by first sliding the brass stud in the plate and then pushing the two levers. The telescope also has a colored sun glass secured on the eye end which must be removed when observing any other object.

**Adjustment of the line of sight.**—Two parallel wires are placed in the focus of the objective of the telescope, the middle point between which marks the center of the field of view. The line joining this point and the optical center of the objective is the axis of the telescope or the line of sight. This line should be parallel to the frame of the instrument. To test the adjustment, turn the telescope in its collar until the wires are parallel to the frame. Select two objects which are at a considerable distance apart, as the sun and moon when distant  $100^\circ$  or more from each other. Point the telescope to the moon and bring the image of the sun tangent to it on one of the wires. Move the instrument until the images appear on the other wire. If they are still tangent, the telescope is adjusted; if otherwise the adjustment is made by two screws in the collar, loosening one and tightening the other. In some instruments the adjustment of the parallelism being supposed to be carefully attended to by the makers, the screws are wanting. With a properly adjusted instrument, two images seen in contact on the wires will overlap in the center

of the field. If the two images are tangent on the lower wire and appear to separate on the wire farthest from the frame, the object end of the telescope droops toward the frame.

#### ERRORS OF THE SEXTANT.

173. To whatever division of the arc the index may point when the mirrors are parallel, this division is the point of beginning of all angle measurements. In other words, it is the temporary zero, and the difference in arc between this temporary zero and the actual zero of the arc is the index error. Due to unequal expansion and contraction, this index error will not remain the same. It should, therefore, be determined anew each time the instrument is to be used. To measure it, bring the mirror to parallelism by producing a perfect coincidence of the direct and reflected images of a distant point or star; read the vernier, giving the result the proper sign—minus if coincidence occurs when the index is on the same side of zero as the greater part of the arc; plus if on the same side of the small portion of the arc, called “off the arc.” Another error which must be looked out for, is that due to “eccentricity.” This error is caused either by an original defect in the instrument or by a bending of the frame by varying temperatures or by accidental blows.

To determine this error, measure with a transit the angle between two distant points having the same elevation. Make several readings of the same angle with the sextant and take the mean. The difference between the transit determination and the mean of the sextant determination, will be the effect of the eccentricity for that particular reading of the sextant. The operation should be repeated for the whole arc at short angular distances and the results tabulated. From time to time this tabulation should be checked to see that no change has occurred.

#### USE OF THE SEXTANT.

174. When angles between terrestrial objects are to be taken with the sextant, the index is set at zero, and holding the instrument in the right hand so that the plane of the frame coincides with the plane through the objects to be observed, with the telescope on the upper side if the angle is approximately horizontal and on the left side if the angle is vertical, sight the left-hand object. There will be a slight lack of coincidence in the two images due to parallax, even if the instrument has been adjusted for index error by sighting at a star. Move the index arm until there is coincidence and read the vernier. Use this reading as index error. Now keeping the left-hand object in the field by sighting through the transparent part of the horizon glass, move the index arm with the left hand until the other object appears in the mirror portion of the horizon glass opposite the first point. Bring the second point exactly opposite by the tangent screw. Test the coincidence of the images by twisting the instrument so as to make the reflected image move back and forth across the direct image. Read the vernier and apply index and eccentricity correction. In rapid work the telescope is not used; sight is taken through the telescope ring. Make it a rule to commence taking angles from the object farthest to the left, then from the next farthest, and so on, always working from left to right. Avoid very large or very



small angles. Though the angles measured with the sextant are seldom horizontal angles, it is usual to plot them as such in filling in a topographical or hydrographic survey. The errors due to obliquity will be nondiscernible in work plotted with the ordinary protractor.

#### THE ENGINEER'S TRANSIT.

175. This instrument is shown, and the names of its parts indicated in figure 20.

**To set up the transit.**—Place the tripod with the legs extended far enough to give a stable base and so as to make the top surface of the

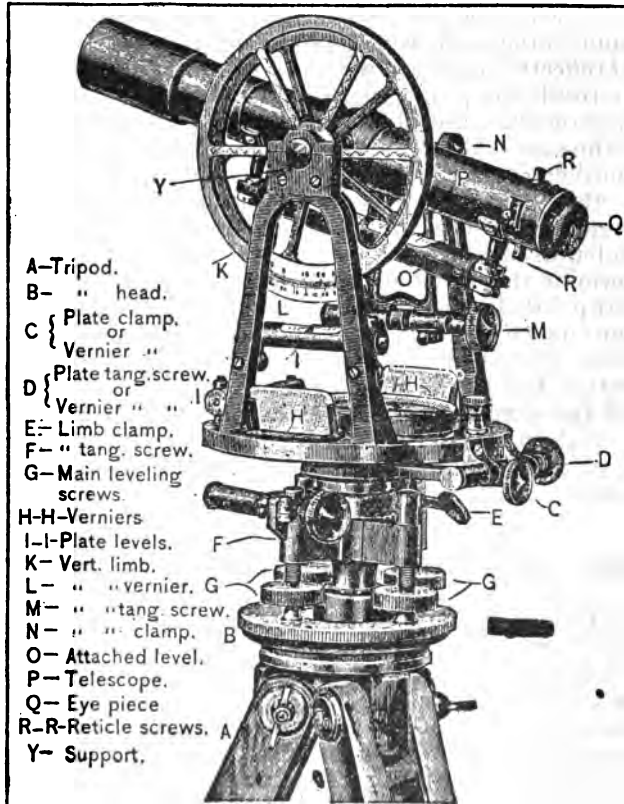


FIG. 20.

tripod head horizontal or nearly so. On level ground the legs will be equally extended. On inclined ground, two legs on the lower side should be on the same level and relatively close together. The third leg is moved straight uphill at right angles to the line of the lower two; the amount this leg is thrown uphill is that sufficient to bring the tripod head roughly level. If the instrument has not already been screwed to the tripod, remove the tripod cap and screw on the instrument in its place. Hang the plumb line on the hook (depending through the tripod head). Level the instrument as follows: Unclamp the vernier plate and turn the transit so that one

of the plate levels is parallel to one pair of leveling screws. The other plate level will be parallel to the other pair. Bring the bubbles of the levels to the center in succession by means of the leveling screws. Always turn one of a pair down as the opposite one is turned up and avoid more pressure of the screws against the plate than is necessary for a firm bearing. If a screw turns hard at any time it is either sprung or has been set up too tight. In turning a pair of leveling screws always move the thumbs toward each other or away from each other. The bubble will follow the motion of the left thumb. If the screws are too tight, unscrew either but not both.

With the level bubbles in the centers of their tubes, the plate will be level if the bubbles are in adjustment. Turn the transit slowly in azimuth and watch the bubbles. If they remain in the centers, the plate is level and the levels are also correct. If either bubble leaves the center, the amount of its motion indicates the amount by which it is out of adjustment. If the amount is small, it may be neglected; if large, the adjustment should be made as hereafter described. For short lines the level error may be neglected if the entire bubble remains in sight during the entire revolution. Adjust the leveling screws in this case so that the travel of the bubble will be equal on both sides of the center.

**Parallax.**—Having leveled the instrument, point the telescope at the sky. Focus the eyepiece until the cross hairs appear sharply distinct. This should eliminate parallax. To test the adjustment, point the telescope at some terrestrial object and bring it to a proper focus by means of the focusing screw of the object glass. Bring the intersection of the cross hairs on some well-defined point of the image. Now move the head laterally, watching the intersection. If there is no relative motion of the cross hairs and the image, parallax has been eliminated. The eyepiece once adjusted for parallax need not again be focused for the same observer unless it has been disturbed. The test, however, should be occasionally repeated. The object glass must be focused for each separate sight. The instrument is now ready for use or adjustment.

The adjustments of the transit are: (1) To make the plane of the plate bubbles truly perpendicular to the vertical axis of the instrument; (2) to make the line of sight truly perpendicular to the horizontal axis; (3) to make the horizontal axis of the telescope truly perpendicular to the vertical axis of the instrument. These three adjustments are made to depend on the principle of reversion, the effect of an error being doubled by a reversal of the instrument. The adjustments should always be made in the order given.

(1) **Adjustment of the bubble tubes.**—One level tube is adjusted at a time. Clamp the lower limb. Bring the bubble in the center of its tube with the leveling screws. Revolve the vernier plate  $180^\circ$ . If the bubble axis is not truly perpendicular to the axis of revolution, the error will be indicated by the bubble leaving the center of the tube. The movement of the bubble measures double the error. Correct the error by bringing the bubble (by means of the small capstan screws on the tube) halfway back to the center. If it is brought exactly halfway back, the error is eradicated. Verify the adjustment by recentering the bubble, as before, with the leveling screws and revolving  $180^\circ$ . If the bubble again leaves the center, there is some error remaining. Correct this residual error as before and verify.

Two attempts should be sufficient to correct all the error. Adjust the other bubble tube in the same manner. While adjusting one bubble see that the other is centered.

(2) **Adjustment of the line of sight.**—Clamp the lower limb. First make the vertical hair perpendicular to the horizontal axis. To do this sight the vertical cross hair on some well-defined point, clamp both plates, rotate telescope about horizontal axis. If point does not appear to travel along vertical hair, loosen screws (R) holding cross hair ring, and by lightly tapping on one screw rotate ring until above condition is fulfilled. **Tighten screws and proceed with second part of adjustment as follows:** See that lower limb is clamped, unclamp the upper or vernier plate. Direct the intersection of the cross hairs at a sharply defined point A, 200 or 300 feet away; clamp the vernier plate, then plunge the telescope (revolve on its horizontal axis), and have an assistant set a point B (a marking pin or a pencil mark on a vertical wall) in line with the intersection of the cross hairs and at approximately the same distance away (points A and B should be at about the same elevation), but in the opposite direction. Unclamp the vernier plate and revolve the telescope in azimuth (about the vertical axis) until the intersection of the cross hairs is again accurately on point A; clamp the vernier plate, and again plunge the telescope and set a point C in line with the intersection of the cross hairs and beside the point B. The distance between the points B and C is four times the error. Mark a point D one-fourth of the distance between B and C, measured from C. Move the cross-hair ring by loosening the reticle screw on one side of the telescope and tightening the one on the opposite side until D is at the intersection of the cross hairs. To verify, repeat the whole operation. Two attempts should be sufficient for accurate adjustment.

(3) **Adjustment of the horizontal axis.**—The plate bubbles being truly perpendicular to the vertical axis of revolution and the line of sight being truly perpendicular to the axis of the trunnions, set up and level the transit. Clamp the lower limb and release the vernier plate. Now with the cross hairs bisect some sharply defined point A, at a very high angle (gable of a house near by); clamp the vernier plate. Depress the telescope and mark down, at a convenient point under the point A and at about the level of the telescope, the point B in line of sight. Now unclamp the vernier plate and revolve the instrument in azimuth (about vertical axis), plunge the telescope (revolve about horizontal axis), and sight at A. The telescope is now inverted (bubble up). Depress the telescope and set a point C in the line of sight and beside the point B. The distance between B and C measures twice the error. Correct for one-half the error by the adjusting screw underneath one end of the horizontal axis.

**Adjustment of the telescope level.**—If there is a level attached to the telescope, it may be adjusted by the "peg" method after the other adjustments are made, as follows: Set up midway between two stakes, which have their tops at about the same elevation, level the transit, and with the bubble of the attached level at the center read a rod on each stake. The difference in the readings is the true difference in level of the tops of the stakes. Move the instrument toward one of the stakes, and set it up so that the eyepiece is about over the center of the stake. Place the rod on the stake near the eyepiece, and set the target in the middle of the field as seen through the

**object glass.** Set up the rod on the far stake with a target set at the reading just taken through the object glass, plus or minus the difference of level between stakes—plus if lower, minus if higher. Bisect the target with the cross wires. **The line of sight must now be horizontal,** and, keeping the vertical motion clamped so as to retain the pointing, adjust the bubble of the attached level to the center by means of the small screws at the movable end of its tube. Both line of sight and axis of bubble are now horizontal, and therefore parallel.

Note that the position of the intersection of the cross wires in the field is a matter of convenience mainly. It is best to have it near the middle of the field, and it can be placed there by inspection with all needful precision before making the adjustment of the line of sight.

**Vertical circle adjustment.**—While the line of sight and attached bubble are still horizontal, the screws holding the vernier for the vertical arc should be loosened and the vernier moved until the reading is zero. If the vernier is not adjustable, the reading of the vernier when the attached level and line of sight are horizontal may be taken as the index error and applied to all readings (or the line of sight may be adjusted to the vernier when reading zero; this will involve a retest of all previous adjustments).

An instrument may at times appear to be out of adjustment because some part is loose.—The object glass may be partly unscrewed or an adjusting screw may be only partly tightened. Level bubbles or cross wires occasionally become loosened; therefore, before commencing the adjustment of an instrument, look out for such defects. When it is thought that an adjustment has been completed, always test the instrument before using. All adjusting screws should be screwed tight enough to hold, and yet not so tight as to injure the threads or put a severe strain on any other part. Especial care should be taken not to strain the cross-wire screws.

To eliminate effects of errors in adjustment, the instrument should be used as follows: To avoid errors in plate bubbles, level up, turn  $180^\circ$  in azimuth, and bring bubbles halfway back by means of leveling screws. This makes vertical axis truly vertical, and the bubbles should remain in the same parts of their respective tubes as the instrument is turned about the vertical axis. Errors in the line of sight and horizontal axis are avoided by using the instrument with its telescope direct, and then in its reversed position and taking the mean of the results, whether the work is running lines or measuring angles. Errors of eccentricity are eliminated by taking the mean of the reading of two opposite verniers. Errors of graduation are nearly eliminated by reading the angle in different parts of the circle, or by measuring the angle by repetition. Where only one vernier is read in determining an angle, always read the same one.

#### USE OF THE TRANSIT.

176. To measure a horizontal angle, set up over the vertex of the angle to be measured and direct the telescope along one of the sides of the angle. Clamp limb and plate—if the latter is set at zero it is more convenient—and with the tangent screw of the limb bring the intersection of the cross hairs on a definite point of the line. Read each of the two verniers and record, calling one vernier **A** and one **B**.

Unclamp the plate—not the limb—and direct the telescope along the other line. Clamp and bring the cross hairs to a definite point with the vernier tangent screw. Read and record as before. Take the differences of the two readings A and B, respectively. If these differences are the same, it is the value of the angle. If not, take the mean of the differences as the value. For greater accuracy, the method of repetition is used. After the first measurement is made, unclamp the limb—not the plate—and resight on the first point by means of the limb tangent screw and proceed as before. The reading of the vernier is now twice the angle. Continue the repetitions until the desired number are made. The last reading divided by the number of measurements is the value of the angle. To guard against errors, it is well to read and record after each measurement.

**To measure a vertical angle.**—Point the instrument, clamp the horizontal motions, and make the readings on the vertical limb. For greater accuracy when there is a complete vertical circle, revolve the instrument through  $180^\circ$ , plunge the telescope, and take new readings. If the results differ, use the mean.

**To run out a straight line.**—Set up accurately over the initial point. Point the telescope in the required direction and establish a second point. These two determine the line which is to be run out. Set up over the forward or second point; lay the telescope on the initial point; clamp limb and plate, plunge telescope, and set a point forward. If the adjustments are good, this third point will be in line with the first and second and the line may be prolonged by repeating the steps taken at the second point.

If the adjustments are not good, set a third point as before. Then unclamp the limb and turn  $180^\circ$  in azimuth and lay on the initial point. Clamp and plunge again and set another third point beside the first one. Take the middle point between the two for the true third point. This method eliminates errors of adjustment, except those of the plate levels. These are so easily observed and corrected that they should never exist when close work is required.

#### TRAVERSING.

177. The transit must be set at each station with a  $0-180^\circ$  line of the azimuth circle parallel to its position at preceding stations. This is called **carrying an azimuth**. The direction chosen for the  $0-180^\circ$  line is usually the true N. and S., or as near it as data at hand will permit.

Having observed the second station from the first, proceed to the second, set up, and set one of the verniers at its reading from the first to the second station, plus  $180^\circ$ , or at the back azimuth. Point at the first station and clamp the limb. The line  $0-180^\circ$  is now in a position parallel to that at the first station. Unclamp the plate, direct the telescope to the third station, and proceed as before.

Also see paragraph 135.

#### A VERNIER.

178. A vernier is an auxiliary scale by means of which the principal scale can be read more closely than can be shown by actual subdivisions on the principal scale.

Consider **AB**, figure 21, as part of a scale of equal parts. Construct the auxiliary scale or vernier **CD**, the total length of which is equal

to 9 of the smallest divisions of the principal scale, but divided into 10 equal parts instead of 9, which makes each division of the vernier  $\frac{1}{10}$  the length of the division of the scale.

When the zero division of the vernier, indicated by an arrow, is coincident with a division, as 31, of the scale, the reading is 31 and it is obvious that the first division of the vernier is to the left of 32 in the scale by  $\frac{1}{10}$  of the distance between 31 and 32. Similarly, the second, third, etc., division of the vernier is 2, 3, etc., tenths to the left of the 33, 34, etc., division of the scale. To make any division of the vernier, as 2d, 3d, 5th, or 8th, coincide with the division of the scale next ahead of it the vernier must be moved to the right 2, 3, 5, or 8 tenths of the length of one division of the scale, and the arrow will then be opposite a point on the scale 2, 3, 5, or 8 tenths of the distance from 31 to 32, or at 31.2, 31.3, 31.5, or 31.8. The quantity obtained by dividing the value of one division of the scale by the number of divisions of the vernier is called the **least count of the vernier**. Only one intermediate vernier division can coincide with a scale division at the same time and the number of the coincident vernier division, counting from the arrowhead, is the number of times the least count must be added to the last scale division passed by the arrow to get the true reading.

To read any vernier note the value of the last scale division passed by the zero of the vernier and to it add the least count multiplied by the number of the coincident vernier division.

Mistakes will be avoided and the reading facilitated by estimating in advance the fractional part of the division of the principal scale.

A vernier constructed as described is always read ahead of the zero, or in the direction in which the scale graduations increase, and is called a **direct vernier**. Verniers may also be constructed by dividing the length of a certain number of divisions of the scale, as 11, into equal parts one less in number, as 10. The principles of operation and method of reading are the same, except that the coincident line is to be found behind the zero of the vernier, or in the direction in which scale graduations decrease. This form is called **retrograde**. It is but little used.

If the scale is graduated in both directions, as is often the case, the vernier is doubled, the zero in the middle and each side forming a direct vernier for the graduations increasing in the same direction. This form is called **double direct**, figure 22. The most compact form is that shown in figure 25, called the **folded vernier**, in which the graduations are numbered from the middle to one end and continue from the other end to the middle. This is read as a direct vernier in either direction. If the coincident line is *ahead* of the middle or in the direction of *increasing graduation*, take its number from the middle as zero. If it is *behind* the middle, or in the direction of *decreasing graduation*, take its number from the nearest end, counting the end line as numbered on the vernier.

Verniers are also constructed on cylindrical surfaces and on conical surfaces. The principles and method of reading are the same for all.

179. The plane table is shown and its parts indicated in figure 26. The adjustments of the instrument are entirely analogous to those of the transit. The plate levels are carried either on the alidade or on the declinator. In reversing for level tube adjustment, care must be taken to have the alidade or the declinator, as the case may be,

cover the same part of the board in both positions by marking two corners on the paper by faint pencil lines.

**To set up the plane table over a known station.**—In the following discussion, it is assumed that a number of stations, the locations of which have been secured by transit triangulation, have been plotted on the plane table sheet as will usually be the case in plane table work. Theoretically before any work can be done on the drawing from any station, the instrument must be so set up that the plotted position of the point is vertically over the corresponding station on the ground; that the board must be truly horizontal; and that the meridian (true

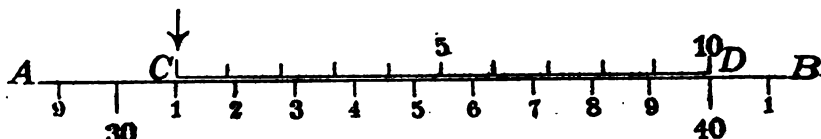


Fig. 21.

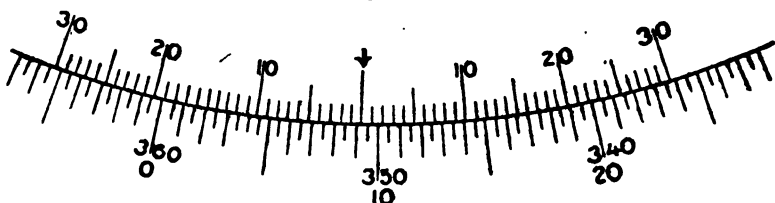


Fig. 22.

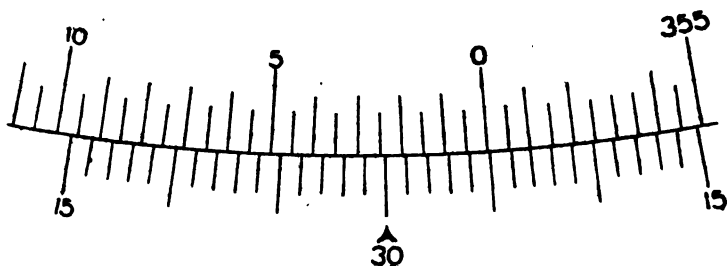


Fig. 23.



Fig. 24.

or magnetic) of the point on the paper must lie in the plane of the meridian of the corresponding station. In the figure, there is shown a device for plumbing any point on the paper over the corresponding point on the ground. Such a refinement is necessary only in very close work on a very large scale. For maps on a scale of 6 inches to the mile or smaller it is sufficient to place the point over the station by the eye.

The board is leveled by the leveling screws or as in some instruments by manipulation of the board by the hands, the board being mounted on the tripod by a ball-and-socket joint. Wilson says that the inclination of the board from the true horizontal plane or the

amount which it is out of level affects the location in azimuth far less than would be at first estimated. For an inclination of  $15^\circ$  the azimuth is affected only  $1^\circ$ . For an inclination of about  $3^\circ$ , the error in azimuth would amount to about less than  $2\frac{1}{2}$  minutes (about 4 feet in a mile). An undue amount of time should not, therefore, be spent in leveling when orientation is to be secured from nearby stations and short side shots only are to be taken.

The third requirement for a proper set up is met by orienting the board, after it has been set over the station and leveled. By orienting is meant the adjustment of the board in azimuth so that the line from the station point to any other point shall be parallel to the corresponding line between the two stations in nature. To orient the board, therefore, place the edge of the ruler of the alidade on the station point and any other distant point. Unclamp and swing the board in azimuth until the line of sight of the alidade intersects the other station. Check by a sight on another station or so.

If the magnetic meridian has not been plotted on the paper, place the declinator on the board, after orientation, and allow the needle to come to a rest. Draw a line the full length of the declinator side and mark the north end. The magnetic meridian will assist in orienting the board when plotted stations can not be seen and will always be valuable as a check.

**Locations by intersection.**—The plane table finds its greatest use in quickly securing a secondary control for topographical work. In open, hilly country, this control is most rapidly made by locating a number of points by intersection and resection. Points are located by intersection by setting up the plane table and orienting as described above over a known station and drawing rays to natural or artificial signals, being careful to number each ray and note in a notebook the object sighted by each numbered ray. A second known point is then visited, the plane table set up and oriented, and a series of rays to the same signals drawn. The intersection of corresponding rays locates the signals.

All stations which are important in the propagation of the plane table triangulation, should be checked by a third ray drawn from a third known station. Where it is difficult to get a third intersection, locations by two rays will serve for tertiary points of control. But if such a station is occupied by the instrument for propagation of the triangulation, the location and orientation should be checked by resection methods. It is sometimes desirable to locate a plane table station from a line only one end of which can be occupied by the table. Let A and B represent the points on the ground at the ends of the line: C is the signal which is to be located, and *ab* represents the line plotted on the plane table sheet. Set up at A, the end of the line which is accessible, and orient the table by sighting B with the alidade along *ab*. Then, centering the alidade on *a*, draw an indefinite line toward C. This line should be drawn the full length of the alidade. The table is then taken to C and oriented by means of the line just drawn. Since the position of *c* on the indefinite line is now known it is necessary to estimate its position on the map and to use this point in setting the table over C. If the alidade is now centered on *b* and sighted toward B, a resection line may be drawn, and this line will cut the first indefinite line thus locating the point *c* desired. The position of *c* found by this method should be

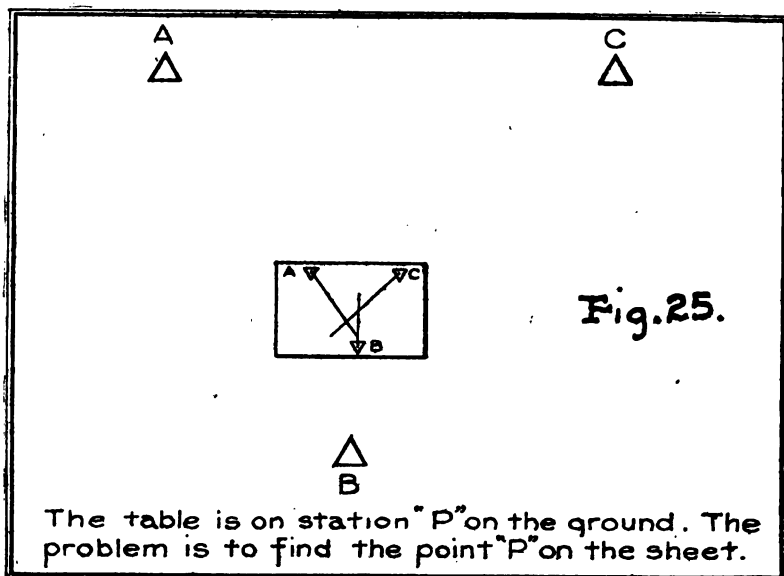


checked if possible by resection lines from other points whose positions are known to be correct.

#### THE THREE-POINT PROBLEM.

180. The plane table may be set up at any place where three triangulation points (plotted on the sheet) can be seen and the position of this plane table station can be determined and plotted on the sheet by observations from this point. The following is one of the graphical solutions:

If three signals A, B, and C have their plotted positions at  $a$ ,  $b$ , and  $c$ , and if the table be set up at any point and oriented correctly, the resection lines drawn from  $a$ ,  $b$ , and  $c$  will pass through  $d$ , the plotted position of P. Since there is no means of accurately orienting the table, the position of  $p$  being unknown at the start the table



must be oriented approximately by the compass. If the plane table is not oriented exactly, the three resection lines will not ordinarily pass through a common point but will form a triangle known as the triangle of error (fig. 25). From this triangle of error the true position of  $p$  may be estimated, and by a second trial a new triangle of error may be obtained which is smaller than the former. By successive trials the triangle may be made so small that it is almost a point. In practice very few trials are necessary, the triangle often being reduced to a point in the second trial.

If the table is on the circumference of the circle through the three points, its position is indeterminate. When point  $p$  is inside the triangle ABC it is in a favorable position for an accurate location. If the table is outside this triangle there are certain positions of the signals which are not favorable, especially when the angles subtended by the sides of the triangle formed by the signals are small and the

middle signal is farthest from  $p$ , but if the middle signal is near  $p$  the location of  $p$  is good.

If  $P$  lies inside the triangle  $ABC$  then  $p$  will lie inside the triangle of error and vice versa. If a circle is passed through  $a, b$  and the intersection of the resection lines from  $a$  and  $b$  it will pass through the true position of  $p$ ; similarly a circle through  $b, c$  and the intersection of the resection lines from  $b$  and  $c$  may be sketched and in this manner a close estimate of the position of  $p$  made for the second trial. In practice, the circles are not actually constructed. A small portion of the arc of each circle is sketched, so as to indicate the position of  $p$ , preparatory to a second trial. The correct distance of  $p$  from any resection line is proportional to the distance of the plane table from the signal from which that line was drawn.

Tracing-paper solution of the three-point problem. By the use of tracing paper the three-point problem is solved approximately with great rapidity. Setting up the table on the unknown point  $P$ , fasten on it a piece of tracing paper of sufficient size to include the positions of all four points. A fine point is marked upon the tracing paper to represent the position of  $p$ . The alidade is then centered about the point  $p$  and pointed successively at the three known points  $A, B, C$ , and the lines  $pa, pb$ , and  $pc$  are drawn on the tracing paper. The alidade being then removed and the tracing paper released. The latter is then so shifted over the plane table sheet that the line  $pa$  shall pass through the located point  $a$ , the line  $pb$  through  $b$ , and the line  $pc$  through  $c$ . Then with all three lines passing through the known points, the point  $p$  is exactly over its correct position on the plane table paper and may be pricked through to the latter. The point  $p$  is now located and orientation is secured by placing the alidade over  $p$  and any other known point and moving the table in azimuth until the other point is intersected by the line of sight. Check by a sight on two other points. It will usually be found that there is a slight error in the location of  $p$ . In case the location of the point is desired more accurately, draw rays from each of the three known stations, and proceed as in the solution given next above.

#### RANGING IN AND LYING IN.

181. It will often be desirable to locate the table at a point from which only two known points are visible. This may be done by ranging in or lining in or by use of the magnetic meridian and needle. This method depends upon the fact that if the table can be oriented in any way the location of the point where the table is set up can be found by resection rays drawn from any two stations in view or by resection from one point, if station is on a plotted line. Therefore if any line has been drawn on the plane table sheet which represents a physical line on the ground, as a straight fence, a railroad tangent, road tangent, etc., the plane table can be set up at any point along the fence or on the tangent and oriented by laying the alidade along the line on the paper and turning the table until the paper line is parallel to the physical line represented. As soon as the table is satisfactorily oriented, pivot the alidade over any known signal and draw a resection ray from that station. The intersection of this resection line and the line of the fence or tangent is the location of the instrument. Similarly it will often be possible to set up the instrument on

the line through two stations and orient by sighting along the line, locating by a resection line from a third station. Or, set up and orient by the needle and draw two resection rays from two known points. The intersection of these will be the location of the table. These methods are satisfactory only for the location of station from which local topography is to be secured. They are not good for extension of triangulation.

#### PLANE TABLE TRAVERSES.

182. Once the plane table has been set up and properly oriented over any plotted point, any other point in the vicinity may be located by drawing a ray through the station in the direction of the point and laying off to scale on the ray the distance to the point as ascertained by stadia or other method of measurement.

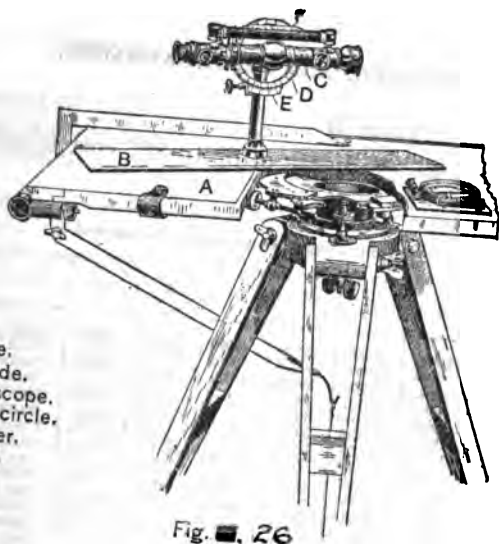
A second point so located on the sheet may, of course, serve as an instrument station, and if the plane table be moved to the second point it may be set up with the plotted position of the point over the actual point on the ground and the instrument oriented by placing the alidade along the ray and moving the table in azimuth until the first point is "backsighted" by the line of sight. With the instrument oriented, a third station may be located from the second in the same manner and by thus proceeding from point to point a plane table traverse may be run and plotted more quickly than can be done by transit and stadia and computation by latitudes and longitudes. As with all other traverses of any considerable length, plane table traverse should not be made a part of the map until they have been adjusted to locations made by more accurate methods. The graphical adjustment described in paragraph 148 is very convenient for the adjustment of plane table traverses. In very large scale work, back flags must be used in order to secure correct orientation and the orientation of the table should be checked whenever possible on triangulation stations. In work on smaller scales better results will be secured if orientation is made by magnetic needle instead of backsights. Whenever local attraction is suspected, backsights should be taken in this work to check the needle orientation.

#### DETERMINATION OF DISTANCES.

183. Distances passed over may be determined by the stride of man or horse, by the time taken by a rated horse, by the revolutions of a wheel, by chain or tape, and by stadia. Distances which are not passed over may be determined by estimation, stadia, or by intersection.

#### REDUCTION TO THE HORIZONTAL.

184. Distances measured along a slope may require a correction before plotting them on a map, as all map distances are, or are supposed to be, measured in a horizontal plane. Such corrections, when made, are called reduction to the horizontal. The following table gives horizontal distances corresponding to sloping distances for gradients up to  $30^\circ$ . The correction for slopes of  $6^\circ$  and less is too small to be plotted on the customary scales and is usually neglected. In flat or ordinary rolling country, the correction will rarely be necessary.



- A-Table.
- B-Alidade.
- C-Telescope.
- D-Vert. circle.
- E-Vernier.
- F-Level.

Fig. 26

Plane Table

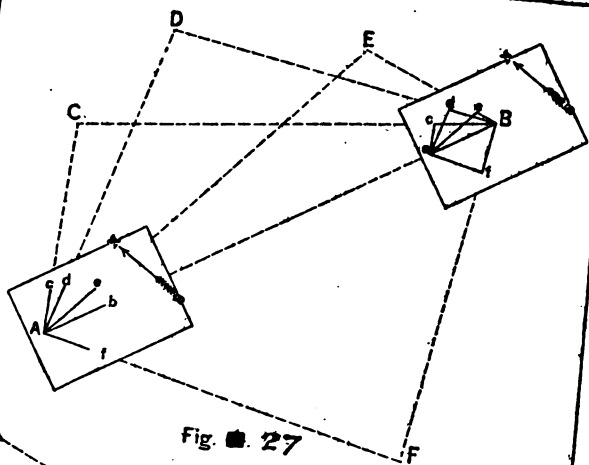


Fig. 27

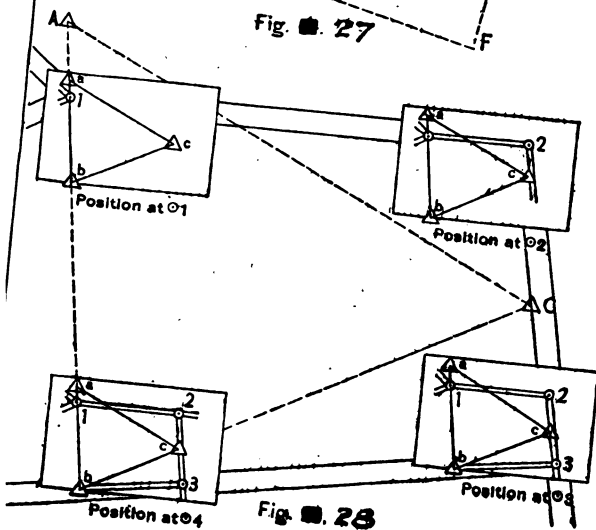


Fig. 28

Traversing and  
Intersecting by  
Plane Table

TABLE II.

185. Horizontal distances for gradients of 0° to 30° corresponding to distances on the slope:

| Gradient in degrees. | Horizontal distances for sloping distances of— |       |       |       |       |       |       |       |       |
|----------------------|--|-------|-------|-------|-------|-------|-------|-------|-------|
|                      | 1  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     |
| 1.....               | 09998  | 19997 | 29995 | 39994 | 49992 | 59991 | 69989 | 79988 | 89986 |
| 2.....               | 09994  | 19988 | 29982 | 39976 | 49969 | 59963 | 59957 | 79951 | 89945 |
| 3.....               | 09986  | 19972 | 29959 | 39945 | 49931 | 59918 | 69904 | 79890 | 89877 |
| 4.....               | 09976  | 19951 | 29927 | 39902 | 49878 | 59854 | 69829 | 79805 | 89781 |
| 5.....               | 09962  | 19924 | 29896 | 39868 | 49810 | 59772 | 69733 | 79695 | 89657 |
| 6.....               | 09945  | 19890 | 29836 | 39781 | 49726 | 59671 | 69616 | 79562 | 89507 |
| 7.....               | 09925  | 19851 | 29776 | 39702 | 49627 | 59553 | 69478 | 79404 | 89329 |
| 8.....               | 09903  | 19805 | 29708 | 39611 | 49513 | 59416 | 69319 | 79221 | 89124 |
| 9.....               | 09877  | 19754 | 29631 | 39507 | 49384 | 59261 | 69138 | 79015 | 88992 |
| 10.....              | 09848  | 19696 | 29544 | 39392 | 49240 | 59088 | 68936 | 78785 | 88633 |
| 12.....              | 09781  | 19563 | 29344 | 39126 | 48907 | 58689 | 68470 | 78252 | 88033 |
| 14.....              | 09703  | 19406 | 29108 | 38812 | 48515 | 58218 | 67921 | 77624 | 87326 |
| 16.....              | 09613  | 19225 | 28838 | 38450 | 48063 | 57676 | 67288 | 76901 | 86513 |
| 18.....              | 09510  | 19021 | 28532 | 38042 | 47553 | 57063 | 66574 | 76084 | 85595 |
| 20.....              | 09397  | 18794 | 28191 | 37588 | 46985 | 56381 | 65778 | 75175 | 84572 |
| 22.....              | 09272  | 18544 | 27815 | 37087 | 46369 | 55681 | 64908 | 74175 | 83446 |
| 24.....              | 09135  | 18271 | 27406 | 36542 | 45677 | 54813 | 63948 | 73084 | 82219 |
| 25.....              | 09063  | 18126 | 27189 | 36252 | 45315 | 54378 | 63441 | 72505 | 81568 |
| 26.....              | 08988  | 17976 | 26964 | 35962 | 44940 | 53928 | 62915 | 71903 | 80891 |
| 27.....              | 08910  | 17820 | 26730 | 35640 | 44550 | 53460 | 62370 | 71280 | 80190 |
| 28.....              | 08829  | 17659 | 26488 | 35318 | 44147 | 52977 | 61806 | 70636 | 79465 |
| 29.....              | 08746  | 17492 | 26238 | 34985 | 43731 | 52477 | 61223 | 69969 | 78716 |
| 30.....              | 08660  | 17320 | 25981 | 34641 | 43301 | 51961 | 60622 | 69282 | 77942 |

The horizontal distance corresponding to any sloping distance and any angle or gradient may be found by multiplying the sloping distance by the cosine of the angle.

#### MEASURING DISTANCES WITH STEEL TAPE.

186. The steel tape furnishes a convenient, rapid, and economical means of measuring any distance for any desired degree of accuracy up to about 1 in 300,000. For topographical surveying a length of 100 feet is most convenient. For base-line measurement the length should be from 300 to 500 feet and its cross section from two to three one-thousandths of a square inch.

The length of a topographical base will depend on the stretch of level or evenly sloping ground available. Such bases have varied in length from  $\frac{1}{2}$  mile to 3 or 4 miles. It is more important to be able to extend the base by well-conditioned triangles than to measure a long base. The ideal site is on level, even ground, from which good views of the surrounding country can be obtained.

#### MEASUREMENT OF BASE.

187. A topographical base should always be measured with a steel tape. This should be carefully compared with a standardized steel tape before and after using. A standardized steel tape is one where exact length for a given temperature pull as well as its coefficient of expansion has been determined by the National Bureau of Standards at Washington, D. C. Any steel tape may be standardized by sending it to that bureau. The manufacturers for a slight extra cost will furnish a certificate giving the temperature and tension at which a tape agrees with their standard (facsimile of that in the national bureau) or they will furnish the tape with the certificate of test made by the national bureau itself. The standardized tape itself should not be used in the field lest it be broken.

For an accuracy of 1 in 5,000 the tape may be used in all kinds of weather, held and stretched by hand, the horizontal position and

amount of pull estimated by the chainman. The temperature may be estimated or read from a thermometer carried for the purpose. On uneven ground the end marks are given by plumb line.

FOR AN ACCURACY OF 1 IN 10,000 TO 1 IN 50,000.

188. The line of the base should first be cleared of trees, bushes, or high grass; small mounds, etc., should be removed.

Each terminal point of the base should, if time allows, be marked by burying a bottle 2 feet underground; accurately centered over this should be built a small masonry pillar, surface flush with the ground. A fine mark should be made in a metal plug sunk into the surface of the pillar.

Having marked the terminal points, set a transit over one of them and direct it on the other, over which a pole should have been fixed; with the transit align stakes at intervals of about 300 yards. By means of this alignment hammer into the ground square-headed stakes, accurately in the line of the base and at tape lengths from each other, starting from one end of the base. The tops of the stakes should be just flush with the ground; on these stakes nail strips of wood or zinc.

In measuring the base, stretch the tape from terminal point to first stake and from stake to stake; the tension should be taken on a spring balance and should be that given for the standardized tape. The end of the tape should be marked by a fine pencil line or knife cut on a wood or zinc strip nailed to top of each stake. The temperature of the tape should be taken at frequent intervals by letting the bulb of the thermometer come in contact with the underside of the tape.

At the other terminal the small space between the last graduation and the end of the base should be measured with a pair of dividers.

Now measure the inclination to horizontal from peg to peg with level or transit. Minor undulations crossed by the tape are to be disregarded.

The base should be measured at least once in each direction; on a dull day, if possible, or in early morning or late afternoon.

**Base calculations.**—The measured length of the base is subject to five corrections:

I. For standard; II. For temperature; III. For inclination; IV. For sag; V. For height above sea.

The following case may be taken as an example (taken from Close):

One tape was kept as a reference tape (the standardized one) and not used for measuring. This, when standardized, had been found to be 0.05 foot short at 62° F.

The tape used (supposed to be 100 feet long) was 0.02 foot long on reference tape at 71° F.

The temperature of tape used in the measurement was 82° F.

Height of base above sea, 4,520 feet.

For 2,300 feet, base had a slope of 1° 15'; remainder level.

I. Standard:

Reference tape was 0.05 short at 62° F.

Steel expands 0.0000625 of its length for 1° F.

Therefore, at 71° it was  $9 \times 100 \times 62.5 / 10,000,000$  longer, or 0.0056 foot longer, or 0.05 less 0.0056 or 0.0444 short of standard.

Reference tape was therefore... 0.0444 short at 71° F.

Tape used..... 0.02 long on reference tape at 71° F.

Tape used was therefore..... 0.0244 short at 71° ..... (a).

## II. Temperature:

Temperature of tape used during measurement was  $32^{\circ}$ ; when compared was  $71^{\circ}$ .

Increase of length,  $11 \times 100 \times 62.5 / 10,000,000$ , or  $0.0069$  ..... (b).

Combining (a) and (b) we find that the tape used was  $0.0175$  short, during measurement; correction for standard and temperature is therefore  $0.0175 \times 5301 / 100$ , or  $0.928$  foot.

## III. Inclination:

For 2,300 feet the base has a slope of  $1^{\circ} 15'$ .

Correction,  $2,300 (1 - \cos 1^{\circ} 15') = 0.55$ .

## IV. Sag:

In the measurement of a base it is desirable that the whole length of the tape should as far as possible be supported by the ground, so that no correction is necessary for the sag of the tape. Where the ground is uneven, it is customary to support the tape at intervals by stakes, but it may happen in the measurement of a base that a ravine has to be crossed. In such a case the sag, i. e., the difference between the length when suspended and when laid on a plane surface, must be determined and corrected for.

If  $s$  = the correction for sag,

$l$  = the length of the tape suspended between two supports (in feet),

$w$  = the weight of the tape in pounds,

$t$  = the tension applied in pounds.

$$s = l w^2 / 24 t^2.$$

## V. Height above sea:

If the base is measured at a mean height ( $h$ ) above sea level, it will require a correction of  $h/R \times$  length of base, where  $R$ , the radius of the earth, may be taken as 20,900,000 feet.

In this case  $h = 4,520$ . Then correction  $= 4,520 \times 5,301 / 20,900,000 = 1.146$ .

Collecting these corrections:

|   |                 |
|---|-----------------|
| I and II, standard and temperature..... | Feet.<br>-0.928 |
| III, inclination.....                   | -0.550          |
| IV, sag.....                            | -0.000          |
| V, height above sea.....                | -1.146          |

|                       |           |
|-----------------------|-----------|
| Total correction..... | -2.624    |
| Measured length.....  | 5,301.240 |

|                               |          |
|-------------------------------|----------|
| Corrected length of base..... | 5,298.62 |
|-------------------------------|----------|

Corrections III and IV must always be negative; I and II may be either positive or negative.

189. For measurements requiring an accuracy greater than 50,000 the precaution taken is more elaborate in the following particulars. The tape is usually supported at intervals of 20 feet by adjustable standards, all standards being aligned and set to uniform grade for each tape length. The correction for sag may then be dispensed with.

For securing steady tension, several devices exist. The simplest is a pointed lever (e. g., a survey sighting rod). A movable collar with a hook or ring and secured by a set screw slides up and down the rod. The end of the tape is secured to this collar at any desired height above the ground. The toe of rod is stuck in the ground and the required tension secured by hauling back on the rod.

For greater accuracy still, the tape ends are secured to movable boxes which are weighted with stones. The ends of the graduation pass over wooden cages spiked into the ground. On the top of the cages are zinc plates for scratching the ends of tape lengths.

For detailed methods of the measurements of lines calling for high accuracy see treatises on surveying.

There are but few localities in the United States that can not conveniently be connected with known positions and distances and therefore, before base-line measurements are undertaken, the records of the Coast and Geodetic Survey, the Lake Survey, the Geological

Survey, the Corps of Engineers, United States Army, and other Government organizations should be examined in order to ascertain what positions in the area surveyed have been determined and are available for use in the work at hand.

#### MEASUREMENT OF DISTANCES BY STADIA.

190. The stadia is primarily intended to secure rapidity rather than accuracy; nevertheless with proper care to eliminate the chief sources of error, a high degree of accuracy may be obtained. Where properly handled, it will produce results as good as, and frequently better than, those with the tape, especially in rough country where variations in the slope of the ground affect taping seriously.

The degree of precision is dependent upon several conditions, chief among which are:

1. Length of sight; 2. Magnifying power of the telescope; 3. Finess of the cross hairs; and 4. Precautions taken to avoid errors due to refraction.

Experiments show that the average error increases rapidly for sights over 800 feet. For short sights errors are less with a 25-power than with a 15-power telescope. On the Mexican boundary survey, the ratio of error between triangulation and taping was 1 in 1,436, and between triangulation and stadia 1 in 1,166. In all there were measured 182.5 miles by stadia which were triangulated and in which the total difference in length was 50 meters, or 1 in 5,873. Experiments show that refraction is a variable quantity, dependent upon temperature of air and ground, that is much greater near the ground than 3 feet above it; also at noon than before or after; that the effects vary for different distances. Twelve miles of stadia measurements with sights averaging 600 feet, in the morning and evening hours, showed an accuracy of 1 in 2,685. The same distances measured at midday showed an accuracy of 1 in 655.

191. To obtain accuracy in stadia work it is best to make short sights, avoid readings near the ground (bottom of the rod), and to avoid working during the midday hours, except on dull, overcast days. For accurate work the most approved practice is to use rods of standard division and to determine the rod interval factor to be applied to the observed distance as a correction. The speed of stadia traverses is far greater than that of taping where the surface of the ground is rough, since sights of one to two thousand feet length can be taken. Under similar circumstances the chain has to be laid down and stretched every hundred feet or less. Over smooth country, traverses may be made by stadia still more rapidly than by taping if the rodmen be mounted and the instrument man rides or drives. On the Mexican survey above cited as many as 16 miles a day were often covered, including the determination of height and the sketching of topography.

#### THEORY OF STADIA MEASUREMENTS.

192. The relation between the size and distance of an object and the size of its image in the telescope is given by the expression

$$Y/Y' = F/X$$

where  $Y$  denotes the height of the object,  $Y'$  that of its image (the distance between stadia wires in this case),  $F$  the focal length of the



object glass, and  $X$  the distance of the object (rod) from the first principal focal point. This point lies in front of the object glass at a distance equal to the focal length (distance between the object glass and the stadia wires). To reduce the measured distance  $X$  to the true distance from the center of the instrument, add to  $X$  a constant equal to the distance of the first principal focal point from the center of the instrument. This constant is called  $c+f$ . Its value varies for different instruments and is usually marked on the inside of the transit box by the makers. It may be directly measured, however, with all the accuracy necessary.  $F$  is the distance from the object glass to the cross hairs when the object glass is focused for a distant object, and  $C$  is the distance from the object glass to the center of the instrument when focused for an average sight. The average value of  $c+f$  for a transit is about 1 foot.

#### GRADUATING THE STADIA ROD.

193. Rods should be of light, straight-grained, well-seasoned wood, 12 to 14 feet long, 5 inches wide, and  $\frac{7}{8}$  inches thick, dressed smooth all around and covered with at least two coats of white paint. To graduate the rod it is necessary to know what space on the rod corresponds to a hundred feet in distance. Measure off  $c+f$  from the plumb bob and set a point. From this point measure off any convenient distance on level ground, as 500 feet. Hold the blank rod in a vertical position at the end of this base, or if possible fasten it rigidly in that position. Have a fixed mark or target on the upper part of the rod on which the upper wire is set. Have an assistant record the position of the lower wire as he is directed by the observer. Some sort of open target is good for this purpose, but any scheme is suitable that will enable the observer to fix the position of the extreme wires at the same moment with exactness. The work should be done when there is no wind and when the atmosphere is very steady; a calm day is best. Repeat the observation until the number of results, or their accordance, shows that the mean will give a good result. Divide the mean space so obtained into five equal parts, thus obtaining the intercept on the rod for 100 feet. By dividing this distance into 20 equal parts diagrams similar to Fig. 24 can be constructed and painted on the rod.

A method of graduation in common use is to divide all rods exactly in feet and tenths. This method has the advantages that the rod may be used as a level rod, that the same accurate template may be used to graduate all rods, etc. By the use of standard templates for patterning the rods large numbers of rods may be painted or repainted each season with much facility and with the minimum risk of mistakes.

194. The stadia is used in connection with a transit having a vertical limb, or a plane table with telescopic alidade having a vertical limb. Distances are read by setting either the upper or lower stadia hairs on a foot mark by means of the vertical arc clamp and tangent screw and counting the feet, tenths, and hundredths between the stadia hairs. The vertical angles are taken by sighting the middle cross hair on a point on the rod whose distance above the foot of the rod is equal to the distance from the horizontal axis of the telescope to the station beneath the transit. The distance is

known as the height of instrument (HI). It is convenient to mark this point on the rod by a rubber band which is adjusted for each set up.

The order of field work is as follows: First read the distance and record it, then set the middle hair on the rubber band and the vertical hair on the middle of the rod. Signal the rodman away and while he is moving to next point read the azimuth and the vertical angle.

#### REDUCTION OF STADIA FIELD NOTES.

195. This is done by means of tables, diagrams, or stadia slide rule rather than by direct use of formulæ. Table III gives, for vertical angles up to  $20^\circ$ , the difference in elevation for an inclined reading of 100 feet. If the inclined reading is 612, the instrumental constant ( $F+c$ ) 1 foot, and the vertical angle  $4^\circ 42'$ , the difference in elevation is  $6.13 \times 8.17 = 50.1$  feet. The horizontal distance is obtained by use of the table of horizontal corrections (Table II), which gives the distances to be subtracted from the inclined reading increased by the instrumental constant,  $c+f$ .

Stadia reduction tables are published (such as the Noble and Casgrain) in which the corrections are made by addition only, instead of multiplication as in Table III. These tables are more convenient than multiplication tables.

The most rapid method of reducing stadia readings is by means of stadia slide rules or computers, such as the Kern, the Colby, the Webb, the Matthes, the Cox, etc. For accurate traverses the readings should be reduced by table and checked by slide rule. For less accurate work the slide rule alone is sufficient.

#### PLOTTING.

196. The plotting of stadia notes which are "cold" is fraught with error. They should when practicable be plotted in the field in the sight of the facts. This may be done by means of a circular protractor and scale, a small plane table or sketching board being used as a plotting board. Some surveyors prefer to use the small plane table as a plane table in conjunction with the transit; the plane table being used to obtain and plot all directions, the transit being used as an auxiliary instrument to read distances and vertical angles.

#### CAUTION.

It is sometimes desirable to take long sights where the intercept of the stadia wires exceeds the length of the rod. In such cases it should be remembered that the middle wire is seldom exactly midway between the upper and lower wires. The sum of the readings between the upper and middle wire and between the middle and lower wire will give closer results than double the reading between the middle and one extreme wire. For accurate azimuth reading, bisect with the vertical wire the edge of the rod instead of the face.

TABLE III.—*Reductions of stadia observations.*

VERTICAL HEIGHTS.

| Minutes: | 0°   | 1°   | 2°   | 3°   | 4°   | 5°    | 6°    | 7°    | 8°    | 9°    | 10°   | 11°   | 12°   | 13°   | 14°   | 15°   | 16°   | 17°   | 18°   | 19°   |
|----------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.       | 0.00 | 1.74 | 3.49 | 5.23 | 6.96 | 8.68  | 10.40 | 12.10 | 13.78 | 15.45 | 17.10 | 18.73 | 20.34 | 21.92 | 23.47 | 25.00 | 26.50 | 27.96 | 29.39 | 30.78 |
| 2.       | 0.06 | 1.80 | 3.55 | 5.28 | 7.02 | 8.74  | 10.51 | 12.21 | 13.89 | 15.56 | 17.21 | 18.84 | 20.44 | 22.02 | 23.57 | 25.09 | 26.59 | 28.06 | 29.44 | 30.83 |
| 4.       | 0.12 | 1.86 | 3.60 | 5.34 | 7.07 | 8.80  | 10.57 | 12.26 | 13.95 | 15.62 | 17.28 | 18.90 | 20.50 | 22.08 | 23.63 | 25.15 | 26.64 | 28.10 | 29.53 | 30.92 |
| 6.       | 0.23 | 1.93 | 3.72 | 5.46 | 7.19 | 8.91  | 10.68 | 12.32 | 14.01 | 15.67 | 17.32 | 18.95 | 20.55 | 22.13 | 23.68 | 25.20 | 26.69 | 28.15 | 29.58 | 30.97 |
| 8.       | 0.29 | 2.04 | 3.78 | 5.52 | 7.26 | 8.97  | 10.74 | 12.38 | 14.06 | 15.73 | 17.37 | 19.00 | 20.60 | 22.18 | 23.73 | 25.25 | 26.74 | 28.20 | 29.62 | 31.01 |
| 10.      | 0.35 | 2.09 | 3.84 | 5.57 | 7.30 | 9.03  | 10.79 | 12.43 | 14.12 | 15.78 | 17.43 | 19.05 | 20.66 | 22.23 | 23.78 | 25.30 | 26.79 | 28.25 | 29.67 | 31.06 |
| 12.      | 0.41 | 2.15 | 3.90 | 5.63 | 7.36 | 9.08  | 10.85 | 12.49 | 14.17 | 15.84 | 17.48 | 19.11 | 20.71 | 22.28 | 23.83 | 25.35 | 26.84 | 28.30 | 29.72 | 31.11 |
| 14.      | 0.47 | 2.21 | 3.95 | 5.69 | 7.42 | 9.14  | 10.91 | 12.55 | 14.23 | 15.89 | 17.54 | 19.16 | 20.76 | 22.33 | 23.88 | 25.40 | 26.89 | 28.34 | 29.76 | 31.15 |
| 16.      | 0.52 | 2.27 | 4.01 | 5.75 | 7.48 | 9.20  | 10.96 | 12.60 | 14.28 | 15.95 | 17.59 | 19.21 | 20.81 | 22.38 | 23.93 | 25.45 | 26.94 | 28.39 | 29.81 | 31.20 |
| 18.      | 0.58 | 2.33 | 4.07 | 5.80 | 7.53 | 9.25  | 11.02 | 12.66 | 14.34 | 16.00 | 17.65 | 19.27 | 20.87 | 22.44 | 23.99 | 25.50 | 27.00 | 28.45 | 29.86 | 31.24 |
| 20.      | 0.64 | 2.38 | 4.13 | 5.86 | 7.59 | 9.31  | 11.08 | 12.72 | 14.40 | 16.06 | 17.70 | 19.32 | 20.92 | 22.49 | 24.04 | 25.55 | 27.05 | 28.50 | 29.90 | 31.28 |
| 22.      | 0.70 | 2.44 | 4.18 | 5.92 | 7.65 | 9.37  | 11.13 | 12.77 | 14.45 | 16.11 | 17.76 | 19.38 | 20.97 | 22.54 | 24.09 | 25.60 | 27.10 | 28.55 | 29.95 | 31.33 |
| 24.      | 0.76 | 2.49 | 4.24 | 5.98 | 7.71 | 9.43  | 11.19 | 12.83 | 14.51 | 16.17 | 17.81 | 19.43 | 21.03 | 22.60 | 24.14 | 25.65 | 27.15 | 28.60 | 30.00 | 31.38 |
| 26.      | 0.81 | 2.55 | 4.29 | 6.04 | 7.76 | 9.48  | 11.25 | 12.88 | 14.56 | 16.22 | 17.86 | 19.48 | 21.08 | 22.65 | 24.19 | 25.70 | 27.20 | 28.65 | 30.04 | 31.42 |
| 28.      | 0.87 | 2.60 | 4.36 | 6.09 | 7.82 | 9.54  | 11.30 | 12.94 | 14.62 | 16.28 | 17.92 | 19.54 | 21.13 | 22.70 | 24.24 | 25.75 | 27.25 | 28.70 | 30.10 | 31.47 |
| 30.      | 0.93 | 2.67 | 4.42 | 6.15 | 7.88 | 9.60  | 11.36 | 13.00 | 14.67 | 16.33 | 17.97 | 19.59 | 21.18 | 22.75 | 24.29 | 25.80 | 27.30 | 28.75 | 30.14 | 31.51 |
| 32.      | 0.99 | 2.73 | 4.48 | 6.21 | 7.94 | 9.66  | 11.42 | 13.05 | 14.73 | 16.39 | 18.03 | 19.64 | 21.24 | 22.80 | 24.34 | 25.85 | 27.35 | 28.80 | 30.19 | 31.56 |
| 34.      | 1.05 | 2.78 | 4.53 | 6.27 | 7.99 | 9.71  | 11.47 | 13.11 | 14.79 | 16.44 | 18.08 | 19.70 | 21.29 | 22.85 | 24.39 | 25.90 | 27.40 | 28.85 | 30.23 | 31.60 |
| 36.      | 1.11 | 2.85 | 4.59 | 6.33 | 8.05 | 9.77  | 11.53 | 13.17 | 14.84 | 16.50 | 18.14 | 19.75 | 21.34 | 22.90 | 24.44 | 25.95 | 27.45 | 28.90 | 30.28 | 31.66 |
| 38.      | 1.16 | 2.91 | 4.65 | 6.38 | 8.11 | 9.83  | 11.59 | 13.22 | 14.90 | 16.55 | 18.19 | 19.80 | 21.39 | 22.94 | 24.48 | 25.99 | 27.49 | 28.94 | 30.32 | 31.70 |
| 40.      | 1.22 | 2.97 | 4.71 | 6.44 | 8.17 | 9.88  | 11.64 | 13.28 | 14.95 | 16.61 | 18.24 | 19.85 | 21.45 | 23.00 | 24.53 | 26.04 | 27.54 | 29.00 | 30.37 | 31.74 |
| 42.      | 1.28 | 3.02 | 4.76 | 6.50 | 8.22 | 9.94  | 11.70 | 13.33 | 15.01 | 16.66 | 18.30 | 19.91 | 21.50 | 23.05 | 24.58 | 26.09 | 27.59 | 29.05 | 30.41 | 31.79 |
| 44.      | 1.34 | 3.08 | 4.82 | 6.56 | 8.28 | 10.00 | 11.76 | 13.39 | 15.06 | 16.72 | 18.35 | 19.96 | 21.55 | 23.10 | 24.63 | 26.14 | 27.64 | 29.10 | 30.46 | 31.84 |
| 46.      | 1.40 | 3.14 | 4.88 | 6.61 | 8.34 | 10.05 | 11.81 | 13.45 | 15.12 | 16.77 | 18.41 | 20.02 | 21.60 | 23.16 | 24.69 | 26.20 | 27.70 | 29.16 | 30.51 | 31.89 |
| 48.      | 1.45 | 3.20 | 4.94 | 6.67 | 8.40 | 10.11 | 11.87 | 13.50 | 15.17 | 16.83 | 18.46 | 20.07 | 21.66 | 23.22 | 24.75 | 26.25 | 27.75 | 29.21 | 30.56 | 31.94 |
| 50.      | 1.51 | 3.26 | 4.99 | 6.73 | 8.45 | 10.17 | 11.93 | 13.56 | 15.23 | 16.88 | 18.51 | 20.12 | 21.71 | 23.27 | 24.80 | 26.30 | 27.80 | 29.26 | 30.61 | 31.99 |
| 52.      | 1.57 | 3.31 | 5.05 | 6.79 | 8.51 | 10.22 | 11.98 | 13.61 | 15.28 | 16.94 | 18.57 | 20.18 | 21.77 | 23.33 | 24.86 | 26.36 | 27.86 | 29.32 | 30.67 | 32.05 |
| 54.      | 1.63 | 3.37 | 5.11 | 6.84 | 8.57 | 10.28 | 12.04 | 13.67 | 15.34 | 17.00 | 18.63 | 20.23 | 21.81 | 23.37 | 24.90 | 26.40 | 27.90 | 29.36 | 30.71 | 32.09 |
| 56.      | 1.69 | 3.43 | 5.17 | 6.90 | 8.63 | 10.34 | 12.10 | 13.73 | 15.40 | 17.05 | 18.68 | 20.28 | 21.86 | 23.42 | 24.95 | 26.45 | 27.95 | 29.41 | 30.76 | 32.14 |
| 58.      | 1.74 | 3.49 | 5.23 | 6.96 | 8.68 | 10.40 | 12.16 | 13.78 | 15.45 | 17.10 | 18.73 | 20.34 | 21.92 | 23.47 | 25.00 | 26.50 | 28.00 | 29.45 | 30.80 | 32.19 |
| 60.      | 1.74 | 3.49 | 5.23 | 6.96 | 8.68 | 10.40 | 12.16 | 13.78 | 15.45 | 17.10 | 18.73 | 20.34 | 21.92 | 23.47 | 25.00 | 26.50 | 28.00 | 29.45 | 30.80 | 32.19 |



## DETERMINATION OF DIFFERENCES IN ELEVATION.

197. In topographical work elevations are referred to a common level surface called the **datum**. The datum is taken low enough so that no point of the area to be mapped will be below it. This makes all elevations positive. For topographic surveys the datum in general use throughout the world is mean sea level. This should always be used where practicable.

The difference in elevation of the two points may be determined: (a) By means of the angle which the line connecting the two points makes with the horizontal, and the horizontal or inclined distance between the two points; (b) by means of an aneroid barometer carried from one point to the other; (c) by means of the differential spirit leveling between the two points.

The vertical angle may be read with some form of clinometer, or with a transit having a vertical circle.

## BAROMETRIC LEVELING.

198. The weight of the atmosphere at sea level is 14.703 pounds per square inch, equal to the weight of a column of mercury 29.92 inches high, or a column of fresh water 34.7 feet high.

The **aneroid barometer** records the pressure of the atmosphere in inches, the same as a mercurial barometer, the reading being taken from a pointer moving on a circular scale. It must be carefully handled as it is sensitive to shocks. A screw head will be seen through a hole in the back of the outer case by which the needle may be brought to any desired reading, and the instrument corrected whenever it can be compared with a standard. With the aneroid, corrections for instrumental temperature can not be made, and for this reason small pocket instruments are preferable, as carried in the pocket they are not exposed to so great changes in this respect.

The **pressure of the atmosphere** varies with the altitude above sea level, and it also varies with the moisture, temperature, and latitude, which do not depend upon the altitude.

In measuring altitudes with the barometer these other causes of variation must be eliminated so far as possible. It is best done by simultaneous observation at both stations. If the stations are not far apart all disturbing conditions will be substantially the same at each and therefore eliminated, except temperature, which, with considerable difference of altitude, will always be less at the upper than at the lower station.

If *simultaneous* observations *can not* be made, the stations should be occupied with as *little interval of time* between as possible, and better results will be obtained if the time of observation can be so chosen as to take advantage of calm, bright, dry weather.

When the hygrometric conditions are very uniform an aneroid read at intervals on a day's march over a rough country will give a fairly good idea of the profile.

199. **Table of elevations above sea level from barometer readings** (United States Coast and Geodetic Survey), for mean hygrometric conditions and mean temperature of 50° F.:

| Barometer reading. | Altitude above sea level. | Differential for 0.01 inch. | Barometer reading. | Altitude above sea level. | Differential for 0.01 inch. | Barometer reading. | Altitude above sea level. | Differential for 0.01 inch. |
|--------------------|---------------------------|-----------------------------|--------------------|---------------------------|-----------------------------|--------------------|---------------------------|-----------------------------|
| <i>Inches.</i>     | <i>Feet.</i>              | <i>Feet.</i>                | <i>Inches.</i>     | <i>Feet.</i>              | <i>Feet.</i>                | <i>Inches.</i>     | <i>Feet.</i>              | <i>Feet.</i>                |
| 18.0               | 13,918                    | -15.1                       | 22.2               | 8,204                     | -12.2                       | 26.4               | 3,453                     | -10.3                       |
| 18.1               | 13,797                    | -15.0                       | 22.3               | 8,083                     | -12.2                       | 26.5               | 3,330                     | -10.2                       |
| 18.2               | 13,677                    | -14.9                       | 22.4               | 7,960                     | -12.2                       | 26.6               | 3,207                     | -10.2                       |
| 18.3               | 13,468                    | -14.9                       | 22.5               | 7,838                     | -12.1                       | 26.7               | 3,175                     | -10.2                       |
| 18.4               | 13,319                    | -14.7                       | 22.6               | 7,717                     | -12.0                       | 26.8               | 3,073                     | -10.1                       |
| 18.5               | 13,172                    | -14.7                       | 22.7               | 7,597                     | -12.0                       | 26.9               | 2,972                     | -10.1                       |
| 18.6               | 13,025                    | -14.6                       | 22.8               | 7,477                     | -11.9                       | 27.0               | 2,871                     | -10.1                       |
| 18.7               | 12,879                    | -14.6                       | 22.9               | 7,356                     | -11.9                       | 27.1               | 2,770                     | -10.0                       |
| 18.8               | 12,733                    | -14.4                       | 23.0               | 7,236                     | -11.8                       | 27.2               | 2,670                     | -10.0                       |
| 18.9               | 12,588                    | -14.4                       | 23.1               | 7,115                     | -11.7                       | 27.3               | 2,570                     | -10.0                       |
| 19.0               | 12,443                    | -14.3                       | 23.2               | 7,004                     | -11.7                       | 27.4               | 2,470                     | -9.9                        |
| 19.1               | 12,302                    | -14.2                       | 23.3               | 6,887                     | -11.7                       | 27.5               | 2,371                     | -9.9                        |
| 19.2               | 12,160                    | -14.2                       | 23.4               | 6,770                     | -11.6                       | 27.6               | 2,272                     | -9.9                        |
| 19.3               | 12,018                    | -14.1                       | 23.5               | 6,654                     | -11.6                       | 27.7               | 2,173                     | -9.9                        |
| 19.4               | 11,877                    | -14.0                       | 23.6               | 6,538                     | -11.5                       | 27.8               | 2,075                     | -9.8                        |
| 19.5               | 11,737                    | -13.9                       | 23.7               | 6,423                     | -11.5                       | 27.9               | 1,977                     | -9.8                        |
| 19.6               | 11,598                    | -13.9                       | 23.8               | 6,308                     | -11.4                       | 28.0               | 1,880                     | -9.7                        |
| 19.7               | 11,459                    | -13.8                       | 23.9               | 6,194                     | -11.4                       | 28.1               | 1,783                     | -9.7                        |
| 19.8               | 11,321                    | -13.7                       | 24.0               | 6,080                     | -11.3                       | 28.2               | 1,686                     | -9.7                        |
| 19.9               | 11,184                    | -13.7                       | 24.1               | 5,967                     | -11.3                       | 28.3               | 1,589                     | -9.7                        |
| 20.0               | 11,047                    | -13.6                       | 24.2               | 5,854                     | -11.3                       | 28.4               | 1,493                     | -9.6                        |
| 20.1               | 10,911                    | -13.5                       | 24.3               | 5,741                     | -11.2                       | 28.5               | 1,397                     | -9.6                        |
| 20.2               | 10,776                    | -13.4                       | 24.4               | 5,629                     | -11.1                       | 28.6               | 1,302                     | -9.5                        |
| 20.3               | 10,642                    | -13.4                       | 24.5               | 5,518                     | -11.1                       | 28.7               | 1,207                     | -9.5                        |
| 20.4               | 10,508                    | -13.3                       | 24.6               | 5,407                     | -11.1                       | 28.8               | 1,112                     | -9.5                        |
| 20.5               | 10,375                    | -13.3                       | 24.7               | 5,296                     | -11.0                       | 28.9               | 1,018                     | -9.4                        |
| 20.6               | 10,242                    | -13.2                       | 24.8               | 5,186                     | -10.9                       | 29.0               | 924                       | -9.4                        |
| 20.7               | 10,110                    | -13.1                       | 24.9               | 5,077                     | -10.9                       | 29.1               | 830                       | -9.4                        |
| 20.8               | 9,979                     | -13.1                       | 25.0               | 4,968                     | -10.9                       | 29.2               | 736                       | -9.3                        |
| 20.9               | 9,848                     | -13.0                       | 25.1               | 4,859                     | -10.8                       | 29.3               | 643                       | -9.3                        |
| 21.0               | 9,718                     | -12.9                       | 25.2               | 4,751                     | -10.8                       | 29.4               | 550                       | -9.2                        |
| 21.1               | 9,589                     | -12.9                       | 25.3               | 4,643                     | -10.8                       | 29.5               | 458                       | -9.2                        |
| 21.2               | 9,460                     | -12.8                       | 25.4               | 4,535                     | -10.7                       | 29.6               | 366                       | -9.2                        |
| 21.3               | 9,332                     | -12.8                       | 25.5               | 4,428                     | -10.7                       | 29.7               | 274                       | -9.2                        |
| 21.4               | 9,204                     | -12.7                       | 25.6               | 4,321                     | -10.6                       | 29.8               | 182                       | -9.1                        |
| 21.5               | 9,077                     | -12.6                       | 25.7               | 4,215                     | -10.6                       | 29.9               | 91                        | -9.1                        |
| 21.6               | 8,951                     | -12.6                       | 25.8               | 4,109                     | -10.5                       | 30.0               | 00                        | -9.1                        |
| 21.7               | 8,825                     | -12.5                       | 25.9               | 4,004                     | -10.5                       | 30.1               | - 91                      | -9.0                        |
| 21.8               | 8,700                     | -12.5                       | 26.0               | 3,899                     | -10.5                       | 30.2               | -181                      | -9.0                        |
| 21.9               | 8,575                     | -12.4                       | 26.1               | 3,794                     | -10.4                       | 30.3               | -271                      | -9.0                        |
| 22.0               | 8,451                     | -12.4                       | 26.2               | 3,690                     | -10.4                       | 30.4               | -361                      | -9.0                        |
| 22.1               | 8,327                     | -12.3                       | 26.3               | 3,586                     | -10.3                       | 30.5               | -451                      | -8.9                        |

## COEFFICIENTS FOR TEMPERATURE CORRECTION.

200. Argument  $(t+t') =$  Sum of temperatures at the two stations:

| $t+t'$ . | Coefficient <i>C</i> . | $t+t'$ . | Coefficient <i>C</i> . | $t+t'$ . | Coefficient <i>C</i> . |
|----------|------------------------|----------|------------------------|----------|------------------------|
| •        |                        | •        |                        | •        |                        |
| 0        | -0.1024                | 70       | -0.0273                | 130      | +0.0368                |
| 10       | -0.0915                | 80       | -0.0166                | 140      | +0.0472                |
| 20       | -0.0808                | 90       | -0.0058                | 150      | +0.0576                |
| 30       | -0.0698                | 100      | +0.0049                | 160      | +0.0677                |
| 40       | -0.0592                | 110      | +0.0156                | 170      | +0.0779                |
| 50       | -0.0486                | 120      | +0.0262                | 180      | +0.0879                |
| 60       | -0.0380                |          |                        |          |                        |

## Examples:

| Station.        | Barometer.               | Temperature.        |
|-----------------|--------------------------|---------------------|
| Sacramento..... | <i>Inches.</i><br>30.014 | <i>° F.</i><br>59.9 |
| Summit.....     | 28.288                   | 42.1                |

From table of elevations:

|   | Feet.     |
|---|-----------|
| Sacramento.....   | = -12.7   |
| Summit.....   | = 6,901.0 |
| Differential.....   | = 6,913.7 |
| $t + t'$ .....  | = 102°    |
| $\therefore C$ .....  | = 0.0070  |
| $\therefore$ Temperature correction, $6,913.7 \times 0.007$ ..... | = +48.4   |
| $H$ .....   | = 6,962.1 |

| Station.   | Barometer. | Temperature. |
|------------|------------|--------------|
|            | Inches.    | ° F.         |
| Lower..... | 28.075     | 57.3         |
| Upper..... | 22.476     | 38.5         |

From table of elevations:

|  | Feet.     |
|--|-----------|
| Lower.....   | = 7,867.0 |
| Upper.....   | = 1,807.0 |
| Differential.....  | = 6,060.0 |
| $t + t'$ .....   | = 95° .08 |
| $\therefore C$ .....   | = +0.0004 |
| $\therefore$ Temperature correction, $6,060 \times 0.0004$ ..... | = +2.4    |
| $H$ .....  | = 6,062.4 |

## GENERAL RULES FOR USING ANEROID BAROMETERS.

201. The best type of aneroid barometer for use in reconnaissance is one with a dial about  $2\frac{3}{4}$  inches in diameter, graduated to 3,000 feet on the scale, with a least reading of 10 feet. In using the barometer—

(1) Keep it at a temperature as nearly constant as is practicable. This is best done by keeping it in an inner pocket, where it will have nearly the temperature of the body. Remove it from the pocket only for the purpose of reading and return it as soon as possible.

(2) Always hold the barometer with its dial horizontal when reading it and tap it gently two or three times with the finger or pencil before reading.

(3) In clear settled weather it will be found that the pressure variation due to change of temperature follows a regular law. Beginning at about 9 a. m. the elevation scale will show a rise of about 10 feet per hour for about four hours. It will then remain stationary until about 4 p. m., and will then fall regularly until about 7 p. m., when the same reading as at 9 a. m. will be reached. A knowledge of this change will enable proper corrections to be made.

(4) In unsettled weather, before or after a storm, note, if possible, the movement of the needle for an hour before starting work to ascertain its direction and rate of change, and thus be enabled to make proper corrections.

## LEVELING WITH THE HAND LEVEL.

202. Differences in elevation can be determined with considerable accuracy by means of the hand level or by means of the clinometer, using level sights. For reconnaissance work without an assistant,

leveling is done up grade; note where the level line of sight strikes the ground, advance to that point and repeat the operation. Each advance corresponds to a difference of elevation equal to the height of the observer's eye. If an assistant is available, leveling can be done down grade as well as up, in which case much longer sights are possible by the use of an improvised level rod.

The hand level in connection with a standard level rod, carried by an assistant, has a wide application in construction work. It admits of great rapidity in cross-section leveling and gives results sufficiently accurate for construction purposes.

The locator's hand level, combining the virtues of the hand level and the clinometer, is an instrument of peculiar value in all reconnaissance work.

#### THE ENGINEER'S LEVEL.

203. This instrument is shown and its parts indicated in Fig. 29. The instrument is focused and set up as described for the transit, except that, as there is but one level, the telescope must be turned in the direction of one pair of leveling screws and leveled, then turned in the direction of the other pair and leveled again. The second leveling usually disturbs the first and the latter should then be releveled.

The level consists essentially of two geometric straight lines—the line of sight and the vertical axis. The adjustment of the instrument consists in making these two lines truly perpendicular to each other.

This is effected by the use of the level tube. The line of sight (the geometric line through the center of the object glass and the intersection of the cross hairs) is made parallel to the axis of the bubble tubes by making each parallel to the axis of the Y's. The verticality of the vertical axis, in the adjusted instrument, is secured by the operation of leveling.

First, make the line of sight parallel to the axis of the Y's, as follows: Set up the instrument and level carefully; note a small object about 300 feet away that one end of the horizontal cross hair touches; turn the instrument in azimuth a few degrees and note whether the other end of the cross wire cuts the point; if it does the horizontal wire is horizontal. Now unlock the Y clips. Bisect with the intersection of the cross hairs some sharply defined point at a convenient distance; revolve (not reverse) the telescope in the Y's until the bubble comes on top. If there is not coincidence between the line of sight and the axis of the Y's, the intersection of the cross hairs will, in the revolved position, not be in the original mark and the amount that it has moved measures double the error. Correct the horizontal hair, moving it (by tightening the top and loosening the bottom capstan screws which hold the reticle or by tightening the bottom and loosening the top, as the case may be) halfway back toward the original mark. Verify the correction by repeating the entire operation. Two attempts should usually be sufficient to eliminate all error. Then adjust the vertical wire in the same way.

Second: Make the bubble axis parallel to the axis of the Y's, as follows: Set up the instrument and unlock the Y clips. Bring the telescope to a position over one diagonal set of leveling screws and clamp in azimuth. Using the leveling screws, now center the bubble. Then lift the telescope carefully out of the Y's and replace it in them,



reverse end for end. If the bubble axis is not parallel to the axis of the Y's, it will be shown by the bubble leaving the center and the amount of movement measures twice the error. Bring the bubble halfway back by means of the adjusting screws at one end of the level tube.

Now verify the adjustment by repeating the entire operation. Two attempts should usually be sufficient to eliminate all error.

The line of sight and the axis of the bubble tube now being each parallel to the axis of the Y's are parallel to each other, and the level is in adjustment. This is the only essential adjustment of the level, and if the bubble be centered carefully in every new direction that a sight is taken there will be no error in the work.

It is desirable, however, as a matter of convenience, that the vertical axis be made truly vertical, so that if the instrument is leveled in one direction the bubble will remain centered while the instrument is moved in azimuth.

To make the vertical axis truly vertical, proceed as follows:

The instrument must first be adjusted as above indicated. Set up the instrument and bring the telescope over a diagonal set of leveling screws. Center the bubble by the leveling screws. Turn the instrument  $180^\circ$  in azimuth. If the vertical axis is not truly vertical, the bubble will leave the center, and the amount of movement will measure twice the error. Correct by moving the bubble halfway back by means of the large nut under one Y. Verify the adjustment, and, if necessary, repeat.

"Peg method." The method of adjustment of the level given assumes that the two rings on the telescope tube which rest in the Y's are circular and exactly equal by construction. This is looked to by good instrument makers.

The line of sight and axis of the bubble may be made perpendicular independently of these two rings and the axis of the Y's by the method known as the "peg method." This method is described in full under the adjustment of the transit, paragraph 166.

Level rods are of two kinds, target and self-reading or speaking. The target rod is finely graduated and has a metal target sliding on it, which is graduated as a vernier. The levelman signals to the rodman, who moves the target up or down until it is in the correct position, when the reading is taken by the rodman, or else the rod is carried to the levelman to be read. The ordinary form is the New York rod. The rod proper is in two parts, which slide on each other. For readings up to 6.5 feet the target is moved on the rod and read from the graduation on the front part by a vernier on the target. For greater readings the target is clamped at 6.5 feet and the back part of the rod slid up on the front part, the reading being taken from a scale on the *side* of the back part of the vernier on the *side* of the front part. The rod is graduated to hundredths of feet and the verniers read to thousandths.

## FIELD NOTES FOR PROFILE LEVELING.

204.

| Station. | B. S.   | H. I.   | F. S. | Elevation. | B. M. and T. P. elevation. | Remarks.  |
|----------|---------|---------|-------|------------|----------------------------|---|
| B. M. 16 | 7.825   | 115.089 |       |            | 107.264                    | x cut on east end of south abutment of Main Street Bridge over Jones Creek. |
| 0        |         |         | 6.32  | 108.77     |                            |   |
| 1        |         |         | 5.01  | 110.08     |                            |   |
| 2        |         |         | 4.78  | 110.31     |                            |   |
| 3        |         |         | 3.22  | 111.87     |                            |   |
| T. P.    | 7.326   | 119.978 | 2.437 |            | 112.652                    | x cut on northwest corner top step St. Lukes Church.                        |
| 4        |         |         | 8.28  | 111.70     |                            |   |
| 4 70     |         |         | 7.32  | 112.66     |                            |   |
| 5        |         |         | 5.26  | 114.72     |                            |   |
| 6        |         |         | 3.15  | 116.83     |                            |   |
| 6 95     |         |         | 2.14  | 117.84     |                            |   |
| 7        |         |         | 2.05  | 117.93     |                            |   |
| T. P.    | 9.326   | 127.807 | 1.487 |            | 118.541                    |   |
| 9        |         |         | 7.28  | 120.62     |                            |   |
|          | 15.151  |         | 3.874 |            |                            |   |
|          | 3.874   |         |       |            |                            |   |
|          | 11.277  |         |       |            |                            |   |
|          | 107.264 |         |       |            |                            |   |
|          | 118.541 |         |       |            |                            |   |

## FIELD NOTES FOR DIFFERENTIAL LEVELING.

| Station. | B. S.   | H. I.   | F. S. | Elevation. | Remarks.  |
|----------|---------|---------|-------|------------|---|
| B. M. 21 | 8.758   | 363.008 |       | 374.256    | x cut on northeast corner of coping of bridge corner Main and Second Streets. |
| T. P. 1  | 9.364   | 369.936 | 2.437 | 380.571    |   |
| T. P. 2  | 10.213  | 398.003 | 2.146 | 387.790    |   |
| T. P. 3  | 6.428   | 401.215 | 3.216 | 394.787    |   |
| B. M.    |         |         | 0.968 | 400.232    |   |
|          | 34.758  |         | 8.782 |            | Station No. 3.  |
|          | 8.782   |         |       |            |   |
|          | 25.976  |         |       |            |   |
|          | 374.256 |         |       |            |   |
|          | 400.232 |         |       |            |   |

## PROFILE LEVELING.

205. To determine a profile: The line to be profiled is first stationed, every 100 foot point or such other distance as is desired being distinctly marked, usually with a stake. The level is set up and a rod reading called a **back sight** (B. S.) taken on a point, called a **bench mark** (B. M.) whose elevation is known. When the B. S. is added to the elevation of the B. M., it gives the **height of the instrument** (H. I.). Rod readings called **fore sights** (F. S.), may then be read on as many station points as can be conveniently seen from the instrument. The elevation of the point on which the rod rests, when A. F. S. is taken is found by subtracting the F. S. from the H. I.

F. S.'s are taken to all station stakes and also to all changes of slope whether they fall at a station or not; and intermediate stations at such points are located by tape measurements. When all the required F. S.'s have been taken that are desired from first set up and it becomes necessary to move the instrument to a new

position to proceed along the line to be profiled, a turning point (T. P.) is selected and its elevation is determined by a careful F. S. This elevation is to be used to determine the height of instrument at the new position. This is done by setting up the instrument at the

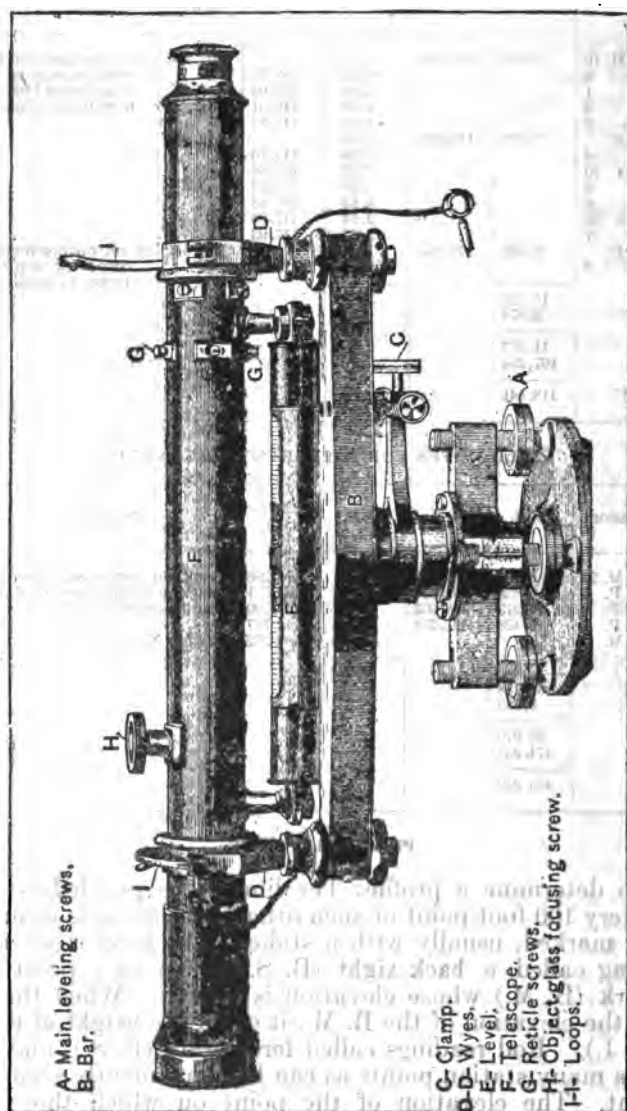


Fig. 29

new position and taking a back sight at the T. P. This B. S. added to the predetermined elevation of the T. P., is the H. I. for the new position. As soon as this is found F. S.'s may be taken on the line. Then a new T. P. is selected from which to determine the H. I. of a

third position of the level; etc. Readings on B. M.'s and T. P.'s should be taken to one more decimal place than those for the profile. The B. M.'s are all carefully described in the notes. As a rule the T. P.'s are not so described, as they are of temporary use only, except when they are taken on easily identified points.

In short lines where great accuracy is not needed, the T. P.'s may be stones or stakes driven into the ground at convenient points. When accurate work is attempted a better T. P. must be used; such as the head of a hatchet the blade of which is firmly driven into the ground, or a large stone well embedded; still better, a steel pin 8 inches long, carried by the rodman for the purpose. Such a pin should be driven into the ground for use and its top should be kept rounded by frequent dressing so that there shall be but one point of contact with the rod; as soon as the new H. I. has been determined from the T. P., the steel pin is pulled from the ground by a cord through an eye in the pin, and used at the next T. P.

The H. I. must always be obtained from a B. M. or proper T. P.; it should never be determined from a stake on the line which is not perfectly firm in the ground and provided with an upper surface giving only one point of contact.

#### DIFFERENTIAL LEVELING.

206. In differential leveling, properly speaking, the only result sought is the determination of the difference of elevation of two points, such as between an existing B. M. and one newly established, etc. No stationing of such a line is necessary and all sights taken are to T. P.'s or B. M.'s. Differential and profile leveling merge into each other and there are few cases in practice where the line run is not a combination of the two.

#### LEVEL NOTES.

207. The forms given in paragraph 207 are recommended. The column arrangement gives the order of work. All level lines should be checked as shown on the forms. The difference between the sum of the B. S.'s and the sum of the F. S.'s, between any two elevations, added or subtracted, as the case may be, to the first elevation will give the other elevation. This check applies only to the sights which are included in the chain of the levels. No F. S. on other than T. P.'s or B. M.'s are part of the chain of levels. This check is arithmetic only and therefore exact. It is in no way a check on the leveling, but only on the accuracy of the notes.

A level line is a curved line everywhere perpendicular to the plumb line, while the line of sight of the instrument is a horizontal line tangent to the level line through the instrument. In order, therefore, to run out a line of levels (curve) by means of a straight line of sight, it is necessary that the F. S. and B. S. be equal in length. The varying densities of layers of air cause a ray of light to be bent in a vertical direction. The effect of this bending (refraction) can be eliminated by limiting the sights to 300 to 400 feet and making the F. S. and B. S. equal. The boiling of the air may make necessary even shorter sights than these.

208. The accuracy of level lines may be checked as follows: Double rodDED lines may be run. In such lines, for every set up of the instru-

ment two (2) T. P.'s are read. They should be close together but should vary in elevation by at least a foot. This gives two independent determinations for each H. I. When these independent determinations differ by small amounts, the work is accepted and notes of both determinations are taken. If they show sudden marked differences, the work is investigated on the spot till the error or mistakes are discovered and corrected. By this method the leveler knows at all times the measure of the precision of his work before he leaves the field.

Another method is to run what are called level loops. The level line is carried forward a mile or so and then closed back to the initial point. If the circuit closes within the allowable limit of error, the work is accepted, the error distributed properly; the work then proceeds from the outer end of the loops as a B. M. and a second loop is run, etc. The allowable error in the precise leveling of the United States Coast and Geodetic Survey is 4 millimeters multiplied by the square root of the distance run in kilometers. For such work self-reading level rods are used and in the construction of the instrument and its manipulation. The observations are made in such a manner as to eliminate the recognized common errors in leveling, which are setting of level on soft ground; unequal expansion and contraction of different parts of the instrument due to temperature changes; irregular refraction of air near the ground; unequal length of back and fore sights; poor turning points; rod not held plumb; bubble not centered when reading is taken. These errors may be eliminated in levels run with the engineer's level and results of considerable accuracy obtained. The ordinary Y level has given results well within the accuracy of precise work. The allowable error of the United States Geological Survey primary levels is equal to the square root of the number of miles run multiplied by 0.04 of a foot (0.04 foot-miles). Work of such accuracy is done only on the main level control lines of a survey; between points thus accurately determined are run level lines of a lesser accuracy by the level of the transit and stadia or by the aneroid, these latter classes of lines being adjusted to the more accurate lines.

#### SPEED OF LEVELING.

209. The speed with which levels may be run varies greatly with the accuracy desired, the character of the country run over, the atmospheric conditions, the method of leveling employed, and the skill of the levelmen and rodmen. Engineering levels of considerable accuracy, such as the primary levels of the United States Geological Survey are run at speeds varying from 50 to 90 miles per month; the precise levels of the Coast and Geodetic Survey have been at the rate of 3 to 5 miles per day (precise levels are, of course, usually run over the best and most favorable grades). Flying levels, in which T. P.'s only are taken, may be run under the most favorable conditions at a rate of over 10 miles per day.

210. The logarithm of a number is the exponent of the power to which a certain other number, called the base, must be raised to produce the given number. The base of the system most used, called common logarithms, is 10.

In any system—

The log. of a product equals the sum of the logs. of the factors.

The log. of a quotient equals the log. of the dividend minus the log. of the divisor; or the log. of a common fraction equals the log. of the numerator minus the log. of the denominator.

The log. of 1 is 0; since the log. 1 = the log.  $\frac{1}{1}$  = the log. 1 - log. 1 = 0.

The log. of a power of a number equals the log. of the number multiplied by the exponent of the power. The log. of a root of a number equals the log. of the number divided by the index of the root.

The first property above is utilized in the construction of the tables. Each log. is the sum of the logs. of two factors of which its number is composed, and the factors may be so chosen that the log. of one is a whole number, called the **characteristic**, and the log. of the other is a decimal fraction, called the **mantissa**. Any number may be resolved into two factors, one of which is the number itself with the decimal point after the first significant figure, and the other the figure 1, alone, or followed or preceded by one or more ciphers.

Thus:

|                        |                 |
|------------------------|-----------------|
| 3760 = 3.76 × 1000     | log. = 3.57518  |
| 376 = 3.76 × 100       | log. = 2.57518  |
| 37.6 = 3.76 × 10       | log. = 1.57518  |
| 3.76 = 3.76 × 1        | log. = 0.57518  |
| 0.376 = 3.76 × 0.1     | log. = -1.57518 |
| 0.0376 = 3.76 × 0.01   | log. = -2.57518 |
| 0.00376 = 3.76 × 0.001 | log. = -3.57518 |

The log. of the constant factor, 3.76 in the above example, is always a positive decimal fraction, and is called the **mantissa**. The log. of the variable factor in the third column above is a whole number and may be positive or negative. It is called the **characteristic**. The logs. of all numbers presenting the same combination of significant figures have the same mantissa regardless of the position of the decimal point. Logarithmic tables contain mantissas only, since the characteristics may be written by inspection and mental calculation. To this rule tables of logarithmic circular functions are an exception, as will be explained later. If the number is whole or mixed, the characteristic of its log. is positive, and one less than the number of places of figures in the integral part, or on the left of the decimal point. If the number is a decimal fraction, the characteristic of its log. is negative, and one greater than the number of ciphers immediately following the decimal point. See example preceding. If the characteristic is positive, the log. is a mixed number and may be treated as such in addition, subtraction, multiplication, and division.

If the characteristic is negative, the log. is not a true mixed number and special treatment is necessary. A negative characteristic may be considered as composed of two numbers, one negative and the other positive. The positive number, prefixed to the mantissa, forms a mixed number for arithmetical operations. The positive and negative parts may be simultaneously increased numerically by the same number without altering the value of the log.

Thus:

$$\begin{aligned} 3.4281 &= \bar{3} + 0.4281 \\ &= \bar{4} + 1.4281 \\ &= 5 + 2.4281, \text{ etc.} \end{aligned}$$

For example, to multiply  $\bar{4}.7265$  by 4.

$$\begin{array}{r} \bar{4}+0.7265 \\ \underline{4} \\ \bar{16}+2.9060=\bar{14}.9060, \text{ which is the required result.} \end{array}$$

To subtract  $\bar{1}.8432$  from  $\bar{3}.1329 = \bar{4} + 1.1329$ .

$$\begin{array}{r} \bar{4}+1.1329 \\ \bar{1}+0.8432 \\ \hline \bar{3}+0.2897=\bar{3}.2897 \end{array}$$

To divide  $\bar{2}.2368$  by 7.  $\bar{2}.2368 = \bar{7} + 5.2368$ .

$$\frac{\bar{7}+5.2368}{7} = \bar{1}+0.7481 = \bar{1}.7481$$

In this case the number added to the minus characteristic should be just enough to make it *exactly divisible* by the divisor.

In the logs. of circular functions a characteristic is given in the tables which is larger by 10 than the true characteristic. These logs. may be used by the above rule by prefixing 10 to each. Thus the log. sine of 21 min. as given in the table = 7.78594. The true log. is  $10 + 7.78594$ , or  $\bar{3}.78594$ . Those who are familiar with the use of these logs. perform the operation on the 10 mentally. The inexperienced will do well to write them out in full.

#### EXPLANATION OF THE TABLE.

211. Table IV gives to five decimal places the common logs. of numbers from 0 to 999 directly, and by interpolation from 0 to 9,999. If the log. of a number larger than 10,000 is desired, factor it and take the sum of the logs. of the factors. Thus,  $\log. 99,225 = \log. \text{ of } 75,000 \text{ plus the log. of } 1.323 = 4.87506 + 0.12156 = 4.99662$ . Or convert the number into a mixed number less than 1,000 and find its log. Thus,  $\log. 992.25 = 992 + \frac{1}{4}$  difference between 992 and 993 = 99,662, which is the mantissa for 99,225.

In the table the logs. of 2 to 9, inclusive, are found at the tops of the columns. For numbers above 10, the first two figures are in the first column, the third at the tops of the columns, and the fourth is interpolated. The right-hand column contains the average difference in each line between logs. in successive columns. For the fourth place multiply one-tenth of the difference on the same line by the fourth figure, and add the product to the log. of the first three figures. Thus:

To find the log. of 4,827, look for 48 in the left-hand column; follow the line to the column headed 2, and take out the mantissa 0.68304 for the number 482. In the right-hand column on the same line is the difference 90, one-tenth of which, 9, multiplied by the fourth figure, 7, = 63, to be added to the log. of 482, making the mantissa of 4,827 = 0.68367. The characteristic is 3 or 1 less than the number of places of integral figures in the number, hence the complete log. of 4,827 is 3.68367.

When the difference exceeds 200, if close results are desired, use the difference obtained by subtracting the number found for the third figure from that in the column for the next higher figure.

The number corresponding to any log. may be obtained from the table by the inverse process. If the given log. is found in the table the corresponding number consists of the two figures on the left

the line, followed by the one at the top of the column. If the exact log. is not in the table, find the next one below and take out the three figures for that. Take the difference between the given log. and the one found in the table next below it and divide this difference by one-tenth the tabulated difference on the line. Write down the quotient for the fourth figure of the required number.

Thus, to find the number corresponding to 1.49638, find 1.49638 in the table and the next below is 49.554. The two figures on the left of the line are 31 and the figure at top of column 2. Hence 31 is the number corresponding to 49.554. The difference between 49.638 and 49.554 is 84, which, divided by 14 or one-tenth of the tabulated difference 138 on the right of the line, gives a quotient of 6 to be set down as the fourth figure. Hence the number required is 0.3136. Since the characteristic is 1, the number is 3.136. The next figures are immediately after the decimal point.

TABLE 1

Common Logarithms, 1 to 100.

|    | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |     |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----|
| 1  | 0.0000 | 0.0004 | 0.0008 | 0.0012 | 0.0015 | 0.0018 | 0.0022 | 0.0025 | 0.0028 | 10  |
| 2  | 0.0033 | 0.0036 | 0.0039 | 0.0043 | 0.0046 | 0.0049 | 0.0053 | 0.0056 | 0.0059 | 20  |
| 3  | 0.0062 | 0.0065 | 0.0068 | 0.0071 | 0.0074 | 0.0077 | 0.0080 | 0.0083 | 0.0086 | 30  |
| 4  | 0.0089 | 0.0092 | 0.0095 | 0.0098 | 0.0101 | 0.0104 | 0.0107 | 0.0110 | 0.0113 | 40  |
| 5  | 0.0116 | 0.0119 | 0.0122 | 0.0125 | 0.0128 | 0.0131 | 0.0134 | 0.0137 | 0.0140 | 50  |
| 6  | 0.0143 | 0.0146 | 0.0149 | 0.0152 | 0.0155 | 0.0158 | 0.0161 | 0.0164 | 0.0167 | 60  |
| 7  | 0.0170 | 0.0173 | 0.0176 | 0.0179 | 0.0182 | 0.0185 | 0.0188 | 0.0191 | 0.0194 | 70  |
| 8  | 0.0197 | 0.0200 | 0.0203 | 0.0206 | 0.0209 | 0.0212 | 0.0215 | 0.0218 | 0.0221 | 80  |
| 9  | 0.0224 | 0.0227 | 0.0230 | 0.0233 | 0.0236 | 0.0239 | 0.0242 | 0.0245 | 0.0248 | 90  |
| 10 | 0.0251 | 0.0254 | 0.0257 | 0.0260 | 0.0263 | 0.0266 | 0.0269 | 0.0272 | 0.0275 | 100 |



TABLE IV—Continued.

Common logarithms, 1 to 999—Continued.

| No.     | 0     | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | Diff. |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 61..... | 78533 | 78604 | 78675 | 78746 | 78816 | 78887 | 78958 | 79028 | 79098 | 79169 | 71    |
| 62..... | 79239 | 79309 | 79379 | 79448 | 79518 | 79588 | 79657 | 79726 | 79796 | 79865 | 70    |
| 63..... | 79934 | 80002 | 80071 | 80140 | 80208 | 80277 | 80345 | 80413 | 80482 | 80550 | 69    |
| 64..... | 80618 | 80685 | 80753 | 80821 | 80889 | 80956 | 81023 | 81090 | 81157 | 81224 | 68    |
| 65..... | 81291 | 81358 | 81424 | 81491 | 81557 | 81624 | 81690 | 81756 | 81822 | 81888 | 67    |
| 66..... | 81954 | 82020 | 82085 | 82151 | 82216 | 82282 | 82347 | 82412 | 82477 | 82542 | 66    |
| 67..... | 82607 | 82672 | 82736 | 82801 | 82866 | 82930 | 82994 | 83058 | 83123 | 83187 | 65    |
| 68..... | 83250 | 83314 | 83378 | 83442 | 83505 | 83569 | 83632 | 83695 | 83758 | 83821 | 64    |
| 69..... | 83884 | 83947 | 84010 | 84073 | 84136 | 84198 | 84260 | 84323 | 84385 | 84447 | 63    |
| 70..... | 84509 | 84571 | 84633 | 84695 | 84757 | 84818 | 84880 | 84941 | 85003 | 85064 | 62    |
| 71..... | 85125 | 85187 | 85248 | 85309 | 85369 | 85430 | 85491 | 85551 | 85612 | 85672 | 61    |
| 72..... | 85733 | 85793 | 85853 | 85913 | 85973 | 86033 | 86093 | 86153 | 86213 | 86272 | 60    |
| 73..... | 86332 | 86391 | 86451 | 86510 | 86569 | 86628 | 86687 | 86746 | 86805 | 86864 | 59    |
| 74..... | 86923 | 86981 | 87040 | 87098 | 87157 | 87215 | 87273 | 87332 | 87390 | 87448 | 58    |
| 75..... | 87506 | 87564 | 87621 | 87679 | 87737 | 87794 | 87852 | 87909 | 87966 | 88024 | 57    |
| 76..... | 88081 | 88138 | 88195 | 88252 | 88309 | 88366 | 88422 | 88479 | 88536 | 88592 | 56    |
| 77..... | 88649 | 88705 | 88761 | 88818 | 88874 | 88930 | 88986 | 89042 | 89098 | 89153 | 55    |
| 78..... | 89209 | 89265 | 89320 | 89376 | 89431 | 89487 | 89542 | 89597 | 89653 | 89707 | 55    |
| 79..... | 89762 | 89817 | 89872 | 89927 | 89982 | 90036 | 90091 | 90145 | 90200 | 90254 | 54    |
| 80..... | 90309 | 90363 | 90417 | 90471 | 90525 | 90579 | 90633 | 90687 | 90741 | 90794 | 54    |
| 81..... | 90848 | 90902 | 90955 | 91009 | 91062 | 91115 | 91169 | 91222 | 91275 | 91328 | 53    |
| 82..... | 91381 | 91434 | 91487 | 91540 | 91592 | 91645 | 91698 | 91750 | 91803 | 91855 | 53    |
| 83..... | 91907 | 91960 | 92012 | 92064 | 92116 | 92168 | 92220 | 92272 | 92324 | 92376 | 52    |
| 84..... | 92427 | 92479 | 92531 | 92582 | 92634 | 92685 | 92737 | 92788 | 92839 | 92890 | 51    |
| 85..... | 92941 | 92993 | 93044 | 93095 | 93146 | 93196 | 93247 | 93298 | 93348 | 93399 | 51    |
| 86..... | 93449 | 93500 | 93550 | 93601 | 93651 | 93701 | 93751 | 93802 | 93852 | 93902 | 50    |
| 87..... | 93951 | 94001 | 94051 | 94101 | 94151 | 94200 | 94250 | 94300 | 94349 | 94398 | 49    |
| 88..... | 94448 | 94497 | 94546 | 94596 | 94645 | 94694 | 94743 | 94792 | 94841 | 94890 | 49    |
| 89..... | 94939 | 94987 | 95036 | 95085 | 95133 | 95182 | 95230 | 95279 | 95327 | 95376 | 48    |
| 90..... | 95424 | 95472 | 95520 | 95568 | 95616 | 95664 | 95712 | 95760 | 95808 | 95856 | 48    |
| 91..... | 95904 | 95951 | 95999 | 96047 | 96094 | 96142 | 96189 | 96236 | 96284 | 96331 | 48    |
| 92..... | 96378 | 96426 | 96473 | 96520 | 96567 | 96614 | 96661 | 96708 | 96754 | 96801 | 47    |
| 93..... | 96848 | 96895 | 96941 | 96988 | 97034 | 97081 | 97127 | 97174 | 97220 | 97266 | 47    |
| 94..... | 97312 | 97359 | 97405 | 97451 | 97497 | 97543 | 97589 | 97635 | 97680 | 97726 | 46    |
| 95..... | 97772 | 97818 | 97863 | 97909 | 97954 | 98000 | 98045 | 98091 | 98136 | 98181 | 46    |
| 96..... | 98227 | 98272 | 98317 | 98362 | 98407 | 98452 | 98497 | 98542 | 98587 | 98632 | 45    |
| 97..... | 98677 | 98721 | 98766 | 98811 | 98855 | 98900 | 98945 | 98989 | 99033 | 99078 | 45    |
| 98..... | 99122 | 99166 | 99211 | 99255 | 99299 | 99343 | 99387 | 99431 | 99475 | 99519 | 44    |
| 99..... | 99563 | 99607 | 99651 | 99694 | 99738 | 99782 | 99825 | 99869 | 99913 | 99956 | 44    |

TABLE V.—Common logarithms of circular functions.

| Arc. | Sine.     | Diff. | Cosine.  | Diff. | Tang.     | Diff. | Cotang.   |       |
|------|-----------|-------|----------|-------|-----------|-------|-----------|-------|
| 0 00 | Inf. neg. | ..... | 10.00000 | ..... | Inf. neg. | ..... | Inf. pos. | 90 00 |
| 01   | 6.46372   | ..... | 10.00000 | ..... | 6.46373   | ..... | 13.53627  | 59    |
| 02   | 7.6476    | 30103 | 10.00000 | ..... | 7.6476    | 30163 | 23524     | 58    |
| 03   | 6.94085   | 17609 | 10.00000 | ..... | 6.94085   | 17609 | 13.05915  | 57    |
| 04   | 7.06579   | 12494 | 10.00000 | ..... | 7.06579   | 12494 | 12.93421  | 56    |
| 05   | 1.6270    | 9691  | 10.00000 | ..... | 1.6270    | 9691  | 83730     | 55    |
| 06   | 24188     | 7918  | 9.99999  | ..... | 24188     | 7918  | 75812     | 54    |
| 07   | 30882     | 6694  | 9.99999  | ..... | 30882     | 6694  | 69117     | 53    |
| 08   | 30632     | 5800  | 9.99999  | ..... | 30632     | 5800  | 63318     | 52    |
| 09   | 41797     | 5115  | 9.99999  | ..... | 41797     | 5115  | 58203     | 51    |
| 10   | 46373     | 4576  | 9.99999  | ..... | 46373     | 4576  | 53627     | 50    |
| 11   | 7.50612   | 4139  | 9.99999  | ..... | 7.50612   | 4139  | 12.49488  | 49    |
| 12   | 54291     | 3779  | 9.99999  | ..... | 54291     | 3779  | 45709     | 48    |
| 13   | 57767     | 3476  | 9.99999  | ..... | 57767     | 3476  | 42233     | 47    |
| 14   | 60085     | 3218  | 9.99999  | ..... | 60085     | 3219  | 39014     | 46    |
| 15   | 63082     | 2996  | 9.99999  | ..... | 63082     | 2996  | 36918     | 45    |
| 16   | 66784     | 2803  | 9.99999  | ..... | 66785     | 2803  | 33215     | 44    |
| 17   | 69417     | 2633  | 9.99999  | ..... | 69418     | 2633  | 30582     | 43    |
| 18   | 71900     | 2482  | 9.99999  | ..... | 71900     | 2482  | 28100     | 42    |
| 19   | 74248     | 2348  | 9.99999  | ..... | 74248     | 2348  | 25752     | 41    |
| 20   | 76475     | 2227  | 9.99999  | ..... | 76476     | 2228  | 23524     | 40    |
| 21   | 7.78594   | 2119  | 9.99999  | ..... | 7.78595   | 2119  | 12.21405  | 39    |
| 22   | 80615     | 2020  | 9.99999  | ..... | 80615     | 2020  | 19384     | 38    |
| 23   | 82545     | 1930  | 9.99999  | ..... | 82546     | 1931  | 17454     | 37    |
| 24   | 84293     | 1848  | 9.99999  | ..... | 84294     | 1848  | 15606     | 36    |
| 25   | 86166     | 1773  | 9.99999  | ..... | 86167     | 1773  | 13833     | 35    |
| 26   | 87869     | 1703  | 9.99999  | ..... | 87871     | 1704  | 12129     | 34    |
| 27   | 89508     | 1639  | 9.99999  | ..... | 89510     | 1639  | 10490     | 33    |
| 28   | 91088     | 1580  | 9.99999  | ..... | 91089     | 1579  | 08911     | 32    |
| 29   | 92612     | 1524  | 9.99998  | ..... | 92613     | 1524  | 07387     | 31    |
| 30   | 94084     | 1472  | 9.99998  | ..... | 94086     | 1473  | 05914     | 30    |
| 31   | 7.95508   | 1424  | 9.99998  | ..... | 7.95510   | 1424  | 12.04490  | 29    |
| 32   | 96887     | 1379  | 9.99998  | ..... | 96889     | 1379  | 03111     | 28    |
| 33   | 98223     | 1336  | 9.99998  | ..... | 98225     | 1336  | 01775     | 27    |
| 34   | 7.99520   | 1297  | 9.99998  | ..... | 7.99522   | 1297  | 12.00478  | 26    |
| 35   | 8.00779   | 1259  | 9.99998  | ..... | 8.00781   | 1259  | 11.99219  | 25    |
| 36   | 02002     | 1223  | 9.99998  | ..... | 02004     | 1223  | 97996     | 24    |
| 37   | 03192     | 1190  | 9.99997  | ..... | 03194     | 1190  | 96805     | 23    |
| 38   | 04350     | 1158  | 9.99997  | ..... | 04353     | 1158  | 95647     | 22    |
| 39   | 05478     | 1128  | 9.99997  | ..... | 05481     | 1128  | 94519     | 21    |
| 40   | 06578     | 1100  | 9.99997  | ..... | 06581     | 1100  | 93419     | 20    |
| 41   | 8.07650   | 1072  | 9.99997  | ..... | 8.07653   | 1072  | 11.92347  | 19    |
| 42   | 08696     | 1046  | 9.99997  | ..... | 08700     | 1047  | 91200     | 18    |
| 43   | 09718     | 1022  | 9.99997  | ..... | 09722     | 1022  | 90278     | 17    |
| 44   | 1.0717    | 998   | 9.99996  | ..... | 1.0720    | 999   | 89280     | 16    |
| 45   | 1.1693    | 976   | 9.99996  | ..... | 1.1696    | 976   | 88304     | 15    |
| 46   | 1.2647    | 954   | 9.99996  | ..... | 1.2651    | 955   | 87349     | 14    |
| 47   | 1.3581    | 934   | 9.99996  | ..... | 1.3585    | 934   | 86415     | 13    |
| 48   | 1.4495    | 914   | 9.99996  | ..... | 1.4500    | 915   | 85500     | 12    |
| 49   | 1.5391    | 895   | 9.99996  | ..... | 1.5395    | 895   | 84605     | 11    |
| 50   | 1.6268    | 877   | 9.99995  | ..... | 1.6273    | 878   | 83727     | 10    |
| 51   | 8.17128   | 860   | 9.99995  | ..... | 8.17133   | 860   | 11.82867  | 9     |
| 52   | 1.7971    | 843   | 9.99995  | ..... | 1.7976    | 843   | 82024     | 8     |
| 53   | 1.8798    | 827   | 9.99995  | ..... | 1.8804    | 828   | 81196     | 7     |
| 54   | 1.9610    | 812   | 9.99995  | ..... | 1.9616    | 812   | 80384     | 6     |
| 55   | 2.0407    | 797   | 9.99994  | ..... | 2.0413    | 797   | 79587     | 5     |
| 56   | 2.1189    | 782   | 9.99994  | ..... | 2.1195    | 782   | 78805     | 4     |
| 57   | 2.1958    | 769   | 9.99994  | ..... | 2.1964    | 769   | 78036     | 3     |
| 58   | 2.2713    | 755   | 9.99994  | ..... | 2.2719    | 755   | 77280     | 2     |
| 59   | 2.3456    | 743   | 9.99994  | ..... | 2.3462    | 743   | 76538     | 1     |
| 60   | 8.24185   | 729   | 9.99993  | ..... | 8.24192   | 730   | 11.75808  | 89 0  |
|      | Cosine.   | Diff. | Sine.    | Diff. | Cotang.   | Diff. | Tang.     | Arc.  |

TABLE V.—Common logarithms of circular functions—Continued.

| Arc. | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |      |
|------|---------|-------|---------|-------|---------|-------|----------|------|
| 1 00 | 8.24185 | 729   | 9.99993 | ..... | 8.24192 | 730   | 11.75608 | 60   |
| 01   | .24903  | 718   | .99993  | ..... | .24910  | 718   | .75609   | 59   |
| 02   | .25609  | 706   | .99993  | ..... | .25616  | 706   | .74383   | 58   |
| 03   | .26304  | 695   | .99993  | ..... | .26311  | 695   | .73668   | 57   |
| 04   | .26988  | 684   | .99992  | ..... | .26996  | 685   | .73004   | 56   |
| 05   | .27661  | 673   | .99992  | ..... | .27669  | 673   | .72331   | 55   |
| 06   | .28324  | 663   | .99992  | ..... | .28332  | 663   | .71658   | 54   |
| 07   | .28977  | 653   | .99992  | ..... | .28986  | 654   | .71014   | 53   |
| 08   | .29621  | 644   | .99991  | ..... | .29629  | 643   | .70371   | 52   |
| 09   | .30255  | 634   | .99991  | ..... | .30263  | 634   | .69737   | 51   |
| 10   | .30879  | 624   | .99991  | ..... | .30888  | 625   | .69112   | 50   |
| 11   | 8.31495 | 616   | 9.99991 | ..... | 8.31505 | 617   | 11.68495 | 49   |
| 12   | .32103  | 608   | .99990  | ..... | .32112  | 607   | .67858   | 48   |
| 13   | .32702  | 599   | .99990  | ..... | .32711  | 599   | .67289   | 47   |
| 14   | .33292  | 590   | .99990  | ..... | .33302  | 591   | .66697   | 46   |
| 15   | .33875  | 583   | .99990  | ..... | .33886  | 584   | .66114   | 45   |
| 16   | .34450  | 575   | .99989  | ..... | .34461  | 575   | .65539   | 44   |
| 17   | .35018  | 568   | .99989  | ..... | .35029  | 568   | .64971   | 43   |
| 18   | .35578  | 560   | .99989  | ..... | .35589  | 560   | .64410   | 42   |
| 19   | .36131  | 553   | .99988  | ..... | .36143  | 554   | .63857   | 41   |
| 20   | .36678  | 547   | .99988  | ..... | .36689  | 546   | .63310   | 40   |
| 21   | 8.37217 | 539   | 9.99988 | ..... | 8.37229 | 540   | 11.62771 | 39   |
| 22   | .37750  | 533   | .99988  | ..... | .37762  | 533   | .62738   | 38   |
| 23   | .38276  | 526   | .99987  | ..... | .38289  | 527   | .61711   | 37   |
| 24   | .38796  | 520   | .99987  | ..... | .38809  | 520   | .61191   | 36   |
| 25   | .39310  | 514   | .99987  | ..... | .39323  | 514   | .60677   | 35   |
| 26   | .39818  | 508   | .99986  | ..... | .39831  | 508   | .60168   | 34   |
| 27   | .40320  | 502   | .99986  | ..... | .40334  | 503   | .59666   | 33   |
| 28   | .40816  | 496   | .99986  | ..... | .40830  | 496   | .59170   | 32   |
| 29   | .41307  | 491   | .99985  | ..... | .41321  | 491   | .58679   | 31   |
| 30   | .41792  | 485   | .99985  | ..... | .41807  | 486   | .58193   | 30   |
| 31   | 8.42272 | 480   | 9.99985 | ..... | 8.42287 | 480   | 11.57713 | 29   |
| 32   | .42746  | 474   | .99984  | ..... | .42762  | 475   | .57238   | 28   |
| 33   | .43216  | 470   | .99984  | ..... | .43231  | 469   | .56768   | 27   |
| 34   | .43680  | 464   | .99984  | ..... | .43696  | 465   | .56304   | 26   |
| 35   | .44139  | 459   | .99983  | ..... | .44156  | 460   | .55844   | 25   |
| 36   | .44594  | 455   | .99983  | ..... | .44611  | 455   | .55389   | 24   |
| 37   | .45044  | 450   | .99983  | ..... | .45061  | 450   | .54939   | 23   |
| 38   | .45489  | 445   | .99982  | ..... | .45507  | 446   | .54493   | 22   |
| 39   | .45930  | 441   | .99982  | ..... | .45948  | 441   | .54052   | 21   |
| 40   | .46366  | 436   | .99982  | ..... | .46385  | 437   | .53615   | 20   |
| 41   | 8.46798 | 432   | 9.99981 | ..... | 8.46817 | 432   | 11.53183 | 19   |
| 42   | .47226  | 428   | .99981  | ..... | .47245  | 428   | .52755   | 18   |
| 43   | .47650  | 424   | .99980  | ..... | .47669  | 424   | .52331   | 17   |
| 44   | .48069  | 419   | .99980  | ..... | .48089  | 420   | .51911   | 16   |
| 45   | .48485  | 416   | .99980  | ..... | .48505  | 416   | .51495   | 15   |
| 46   | .48896  | 411   | .99979  | ..... | .48917  | 412   | .51083   | 14   |
| 47   | .49304  | 408   | .99979  | ..... | .49325  | 408   | .50675   | 13   |
| 48   | .49708  | 404   | .99979  | ..... | .49729  | 404   | .50271   | 12   |
| 49   | .50108  | 400   | .99978  | ..... | .50130  | 401   | .49870   | 11   |
| 50   | .50504  | 396   | .99978  | ..... | .50527  | 397   | .49473   | 10   |
| 51   | 8.50897 | 393   | 9.99977 | ..... | 8.50920 | 393   | 11.49080 | 9    |
| 52   | .51287  | 390   | .99977  | ..... | .51310  | 390   | .48680   | 8    |
| 53   | .51673  | 386   | .99976  | ..... | .51696  | 386   | .48284   | 7    |
| 54   | .52055  | 382   | .99976  | ..... | .52079  | 383   | .47921   | 6    |
| 55   | .52434  | 379   | .99976  | ..... | .52459  | 380   | .47541   | 5    |
| 56   | .52810  | 376   | .99975  | ..... | .52835  | 376   | .47165   | 4    |
| 57   | .53183  | 373   | .99975  | ..... | .53208  | 373   | .46792   | 3    |
| 58   | .53552  | 369   | .99974  | ..... | .53578  | 370   | .46422   | 2    |
| 59   | .53919  | 367   | .99974  | ..... | .53945  | 367   | .46055   | 1    |
| 60   | 8.54282 | 363   | 9.99973 | ..... | 8.54308 | 363   | 11.45692 | 88 0 |
|      | Cosine. | Diff. | Sine.   | Diff. | Cotang. | Diff. | Tang.    | Arc. |

TABLE V.—Common logarithms of circular functions—Continued.

| Arc. | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |      |
|------|---------|-------|---------|-------|---------|-------|----------|------|
| 2 00 | 8.54282 | 363   | 9.99973 | ..... | 8.54308 | 363   | 11.456   | 60   |
| 01   | .54642  | 360   | .99973  | ..... | .54669  | 361   | .453     | 59   |
| 02   | .54999  | 357   | .99973  | ..... | .55027  | 358   | .44973   | 58   |
| 03   | .55354  | 355   | .99972  | ..... | .55382  | 355   | .44618   | 57   |
| 04   | .55705  | 351   | .99972  | ..... | .55734  | 352   | .44266   | 56   |
| 05   | .56054  | 349   | .99971  | ..... | .56083  | 349   | .43917   | 55   |
| 06   | .56400  | 346   | .99971  | ..... | .56429  | 346   | .43571   | 54   |
| 07   | .56743  | 343   | .99970  | ..... | .56773  | 344   | .43227   | 53   |
| 08   | .57084  | 341   | .99970  | ..... | .57114  | 341   | .42886   | 52   |
| 09   | .57421  | 337   | .99969  | ..... | .57452  | 338   | .42548   | 51   |
| 10   | .57757  | 336   | .99969  | ..... | .57788  | 336   | .42212   | 50   |
| 11   | 8.58089 | 332   | 9.99968 | ..... | 8.58121 | 333   | 11.41879 | 49   |
| 12   | .58419  | 330   | .99968  | ..... | .58451  | 330   | .41549   | 48   |
| 13   | .58747  | 328   | .99967  | ..... | .58779  | 328   | .41220   | 47   |
| 14   | .59072  | 325   | .99967  | ..... | .59105  | 326   | .40895   | 46   |
| 15   | .59395  | 323   | .99966  | ..... | .59428  | 323   | .40572   | 45   |
| 16   | .59715  | 320   | .99966  | ..... | .59749  | 321   | .40251   | 44   |
| 17   | .60033  | 318   | .99965  | ..... | .60068  | 319   | .39932   | 43   |
| 18   | .60349  | 316   | .99965  | ..... | .60384  | 316   | .39616   | 42   |
| 19   | .60662  | 313   | .99964  | ..... | .60698  | 314   | .39302   | 41   |
| 20   | .60973  | 311   | .99964  | ..... | .61009  | 311   | .38991   | 40   |
| 21   | 8.61282 | 309   | 9.99963 | ..... | 8.61319 | 310   | 11.38681 | 39   |
| 22   | .61589  | 307   | .99963  | ..... | .61626  | 307   | .38374   | 38   |
| 23   | .61894  | 305   | .99962  | ..... | .61931  | 305   | .38069   | 37   |
| 24   | .62196  | 302   | .99962  | ..... | .62234  | 303   | .37766   | 36   |
| 25   | .62496  | 300   | .99961  | ..... | .62535  | 301   | .37465   | 35   |
| 26   | .62795  | 299   | .99961  | ..... | .62834  | 299   | .37166   | 34   |
| 27   | .63091  | 296   | .99960  | ..... | .63131  | 297   | .36869   | 33   |
| 28   | .63385  | 294   | .99960  | ..... | .63426  | 295   | .36574   | 32   |
| 29   | .63678  | 293   | .99959  | ..... | .63718  | 292   | .36282   | 31   |
| 30   | .63968  | 290   | .99959  | ..... | .64009  | 291   | .35991   | 30   |
| 31   | 8.64256 | 288   | 9.99958 | ..... | 8.64298 | 289   | 11.35702 | 29   |
| 32   | .64543  | 287   | .99957  | ..... | .64585  | 287   | .35415   | 28   |
| 33   | .64827  | 284   | .99957  | ..... | .64870  | 285   | .35130   | 27   |
| 34   | .65110  | 283   | .99956  | ..... | .65154  | 284   | .34846   | 26   |
| 35   | .65391  | 281   | .99956  | ..... | .65435  | 281   | .34565   | 25   |
| 36   | .65670  | 279   | .99955  | ..... | .65715  | 280   | .34285   | 24   |
| 37   | .65947  | 277   | .99955  | ..... | .65993  | 278   | .34007   | 23   |
| 38   | .66223  | 276   | .99954  | ..... | .66269  | 276   | .33731   | 22   |
| 39   | .66497  | 274   | .99953  | ..... | .66543  | 274   | .33457   | 21   |
| 40   | .66769  | 272   | .99953  | ..... | .66816  | 273   | .33184   | 20   |
| 41   | 8.67039 | 270   | 9.99952 | ..... | 8.67087 | 271   | 11.32913 | 19   |
| 42   | .67308  | 269   | .99952  | ..... | .67356  | 269   | .32644   | 18   |
| 43   | .67575  | 267   | .99951  | ..... | .67624  | 268   | .32376   | 17   |
| 44   | .67840  | 265   | .99951  | ..... | .67890  | 266   | .32110   | 16   |
| 45   | .68104  | 264   | .99950  | ..... | .68154  | 264   | .31846   | 15   |
| 46   | .68366  | 262   | .99949  | ..... | .68417  | 263   | .31583   | 14   |
| 47   | .68627  | 261   | .99949  | ..... | .68678  | 261   | .31322   | 13   |
| 48   | .68886  | 259   | .99948  | ..... | .68938  | 260   | .31062   | 12   |
| 49   | .69144  | 258   | .99947  | ..... | .69196  | 258   | .30804   | 11   |
| 50   | .69400  | 256   | .99947  | ..... | .69453  | 257   | .30547   | 10   |
| 51   | 8.69654 | 254   | 9.99946 | ..... | 8.69708 | 255   | 11.30292 | 9    |
| 52   | .69907  | 253   | .99946  | ..... | .69962  | 254   | .30038   | 8    |
| 53   | .70159  | 252   | .99945  | ..... | .70214  | 252   | .29786   | 7    |
| 54   | .70409  | 250   | .99944  | ..... | .70465  | 251   | .29535   | 6    |
| 55   | .70658  | 249   | .99944  | ..... | .70714  | 249   | .29286   | 5    |
| 56   | .70905  | 247   | .99943  | ..... | .70962  | 248   | .29038   | 4    |
| 57   | .71151  | 246   | .99942  | ..... | .71208  | 246   | .28792   | 3    |
| 58   | .71395  | 244   | .99942  | ..... | .71453  | 245   | .28547   | 2    |
| 59   | .71638  | 243   | .99941  | ..... | .71697  | 244   | .28303   | 1    |
| 60   | 8.71880 | 242   | 9.99940 | ..... | 8.71940 | 243   | 11.28060 | 87 0 |
|      | Cosine. | Diff. | Sine.   | Diff. | Tang.   | Diff. | Tang.    | Arc. |

TABLE V.—Common logarithms of circular functions—Continued.

| Arc. | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |      |
|------|---------|-------|---------|-------|---------|-------|----------|------|
| 3 00 | 8.71880 | 242   | 9.99940 | ..... | 8.71940 | 243   | 11.28060 | 60   |
| 01   | .72120  | 240   | .99940  | ..... | .72181  | 241   | .27819   | 59   |
| 02   | .72359  | 239   | .99939  | ..... | .72420  | 239   | .27679   | 58   |
| 03   | .72597  | 238   | .99938  | ..... | .72659  | 239   | .27541   | 57   |
| 04   | .72834  | 237   | .99938  | ..... | .72896  | 237   | .27404   | 56   |
| 05   | .73069  | 235   | .99937  | ..... | .73132  | 236   | .26869   | 55   |
| 06   | .73303  | 234   | .99936  | ..... | .73366  | 234   | .26654   | 54   |
| 07   | .73535  | 232   | .99936  | ..... | .73600  | 234   | .26400   | 53   |
| 08   | .73767  | 232   | .99935  | ..... | .73832  | 232   | .26168   | 52   |
| 09   | .73997  | 230   | .99934  | ..... | .74063  | 231   | .25937   | 51   |
| 10   | .74226  | 229   | .99934  | ..... | .74292  | 229   | .25708   | 50   |
| 11   | 8.74454 | 228   | 9.99933 | ..... | 8.74521 | 229   | 11.25479 | 49   |
| 12   | .74680  | 226   | .99932  | ..... | .74748  | 227   | .25252   | 48   |
| 13   | .74905  | 225   | .99931  | ..... | .74974  | 226   | .25026   | 47   |
| 14   | .75130  | 225   | .99931  | ..... | .75199  | 225   | .24801   | 46   |
| 15   | .75358  | 223   | .99930  | ..... | .75423  | 224   | .24577   | 45   |
| 16   | .75575  | 222   | .99929  | ..... | .75645  | 222   | .24355   | 44   |
| 17   | .75795  | 220   | .99929  | ..... | .75867  | 222   | .24133   | 43   |
| 18   | .76015  | 220   | .99928  | ..... | .76087  | 220   | .23913   | 42   |
| 19   | .76234  | 219   | .99927  | ..... | .76306  | 219   | .23693   | 41   |
| 20   | .76451  | 217   | .99926  | ..... | .76525  | 219   | .23475   | 40   |
| 21   | 8.76667 | 216   | 9.99926 | ..... | 8.76742 | 217   | 11.23258 | 39   |
| 22   | .76883  | 216   | .99926  | ..... | .76958  | 216   | .23042   | 38   |
| 23   | .77097  | 214   | .99924  | ..... | .77173  | 215   | .22827   | 37   |
| 24   | .77310  | 213   | .99923  | ..... | .77387  | 214   | .22613   | 36   |
| 25   | .77522  | 212   | .99923  | ..... | .77599  | 212   | .22400   | 35   |
| 26   | .77733  | 211   | .99922  | ..... | .77811  | 212   | .22189   | 34   |
| 27   | .77943  | 210   | .99921  | ..... | .78022  | 211   | .21978   | 33   |
| 28   | .78152  | 209   | .99920  | ..... | .78232  | 210   | .21768   | 32   |
| 29   | .78360  | 208   | .99920  | ..... | .78441  | 209   | .21559   | 31   |
| 30   | .78567  | 207   | .99919  | ..... | .78649  | 208   | .21351   | 30   |
| 31   | 8.78774 | 207   | 9.99918 | ..... | 8.78855 | 206   | 11.21145 | 29   |
| 32   | .78979  | 205   | .99917  | ..... | .79061  | 206   | .20939   | 28   |
| 33   | .79183  | 204   | .99917  | ..... | .79266  | 205   | .20734   | 27   |
| 34   | .79386  | 203   | .99916  | ..... | .79470  | 204   | .20530   | 26   |
| 35   | .79588  | 202   | .99915  | ..... | .79673  | 203   | .20327   | 25   |
| 36   | .79789  | 201   | .99914  | ..... | .79875  | 202   | .20125   | 24   |
| 37   | .79990  | 201   | .99913  | ..... | .80076  | 201   | .19924   | 23   |
| 38   | .80189  | 199   | .99913  | ..... | .80276  | 200   | .19723   | 22   |
| 39   | .80388  | 199   | .99912  | ..... | .80476  | 200   | .19524   | 21   |
| 40   | .80585  | 197   | .99911  | ..... | .80674  | 198   | .19326   | 20   |
| 41   | 8.80782 | 197   | 9.99910 | ..... | 8.80872 | 198   | 11.19128 | 19   |
| 42   | .80978  | 196   | .99909  | ..... | .81068  | 196   | .18932   | 18   |
| 43   | .81173  | 195   | .99909  | ..... | .81264  | 196   | .18736   | 17   |
| 44   | .81367  | 194   | .99908  | ..... | .81459  | 195   | .18541   | 16   |
| 45   | .81560  | 193   | .99907  | ..... | .81653  | 194   | .18347   | 15   |
| 46   | .81752  | 192   | .99906  | ..... | .81846  | 193   | .18154   | 14   |
| 47   | .81944  | 192   | .99905  | ..... | .82038  | 192   | .17962   | 13   |
| 48   | .82134  | 190   | .99904  | ..... | .82230  | 192   | .17770   | 12   |
| 49   | .82324  | 190   | .99904  | ..... | .82420  | 190   | .17579   | 11   |
| 50   | .82513  | 189   | .99903  | ..... | .82610  | 190   | .17390   | 10   |
| 51   | 8.82701 | 188   | 9.99902 | ..... | 8.82799 | 189   | 11.17201 | 9    |
| 52   | .82888  | 187   | .99901  | ..... | .82987  | 188   | .17018   | 8    |
| 53   | .83075  | 187   | .99900  | ..... | .83175  | 188   | .16825   | 7    |
| 54   | .83261  | 186   | .99899  | ..... | .83361  | 186   | .16639   | 6    |
| 55   | .83446  | 185   | .99898  | ..... | .83547  | 186   | .16453   | 5    |
| 56   | .83630  | 184   | .99898  | ..... | .83732  | 185   | .16268   | 4    |
| 57   | .83813  | 183   | .99897  | ..... | .83916  | 184   | .16084   | 3    |
| 58   | .83996  | 183   | .99896  | ..... | .84100  | 184   | .15900   | 2    |
| 59   | .84177  | 181   | .99895  | ..... | .84282  | 182   | .15717   | 1    |
| 60   | 8.84358 | 181   | 9.99894 | ..... | 8.84464 | 182   | 11.15536 | 86 0 |
|      | Cosine. | Diff. | Sine.   | Diff. | Cotang. | Diff. | Tang.    | Arc. |

**TABLE V.—Common logarithms of circular functions—Continued.**

| Arc.  | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |       |
|---|---------|-------|---------|-------|---------|-------|----------|-------|
| 0 00  | 8.84358 | 181   | 9.99894 | 1     | 8.84464 | 182   | 11.15536 | 00 00 |
| 10  | 8.86128 | 1770  | 9.99885 | 9     | 8.85243 | 1779  | 11.13757 | 10    |
| 20  | 8.87828 | 1700  | 9.99876 | 9     | 8.87823 | 1710  | 11.12047 | 20    |
| 30  | 8.89464 | 1636  | 9.99866 | 10    | 8.89508 | 1645  | 11.10402 | 30    |
| 40  | 9.01040 | 1576  | 9.99856 | 10    | 9.01185 | 1587  | 10.08818 | 40    |
| 50  | 9.2561  | 1521  | 9.99845 | 11    | 9.27716 | 1531  | 10.07384 | 50    |
| 5 00  | 8.94030 | 1469  | 9.99834 | 11    | 8.94193 | 1479  | 11.05808 | 00 10 |
| 10  | 9.5450  | 1420  | 9.99823 | 11    | 9.5827  | 1432  | 10.04373 | 10    |
| 20  | 9.6825  | 1376  | 9.99812 | 11    | 9.70713 | 1346  | 10.02987 | 20    |
| 30  | 9.8157  | 1332  | 9.99800 | 12    | 9.8358  | 1345  | 10.01642 | 30    |
| 40  | 9.9450  | 1293  | 9.99787 | 13    | 9.99662 | 1304  | 10.00318 | 40    |
| 50  | 9.00704 | 1254  | 9.99774 | 13    | 9.00930 | 1268  | 10.99070 | 50    |
| 6 00  | 9.01923 | 1219  | 9.99761 | 13    | 9.02162 | 1232  | 10.97818 | 00 20 |
| 10  | 0.03109 | 1186  | 9.99748 | 13    | 0.03361 | 1199  | 0.96519  | 10    |
| 20  | 0.04262 | 1153  | 9.99734 | 14    | 0.04528 | 1167  | 0.95172  | 20    |
| 30  | 0.05386 | 1124  | 9.99720 | 14    | 0.05606 | 1138  | 0.93814  | 30    |
| 40  | 0.06481 | 1096  | 9.99705 | 15    | 0.06776 | 1109  | 0.92456  | 40    |
| 50  | 0.07548 | 1067  | 9.99690 | 15    | 0.07858 | 1083  | 0.92142  | 50    |
| 7 00  | 9.08589 | 1041  | 9.99678 | 15    | 9.08814 | 1066  | 10.91088 | 00 30 |
| 10  | 0.09606 | 1017  | 9.99659 | 16    | 0.09947 | 1033  | 0.90053  | 10    |
| 20  | 0.10599 | 993   | 9.99643 | 16    | 0.10956 | 1009  | 0.89044  | 20    |
| 30  | 0.11570 | 971   | 9.99627 | 16    | 0.11943 | 987   | 0.88057  | 30    |
| 40  | 0.12519 | 949   | 9.99610 | 17    | 0.12909 | 966   | 0.87091  | 40    |
| 50  | 0.13447 | 928   | 9.99593 | 17    | 0.13854 | 945   | 0.86146  | 50    |
| 8 00  | 9.14355 | 908   | 9.99578 | 18    | 9.14780 | 926   | 10.85220 | 00 40 |
| 10  | 0.15245 | 890   | 9.99557 | 18    | 0.15688 | 904   | 0.84312  | 10    |
| 20  | 0.16116 | 871   | 9.99539 | 18    | 0.16577 | 880   | 0.83423  | 20    |
| 30  | 0.16970 | 854   | 9.99520 | 19    | 0.17450 | 873   | 0.82560  | 30    |
| 40  | 0.17807 | 837   | 9.99501 | 19    | 0.18306 | 856   | 0.81704  | 40    |
| 50  | 0.18628 | 821   | 9.99482 | 19    | 0.19146 | 840   | 0.80864  | 50    |
| 9 00  | 9.19433 | 806   | 9.99462 | 20    | 9.19971 | 825   | 10.80020 | 00 50 |
| 10  | 0.20223 | 790   | 9.99442 | 20    | 0.20742 | 811   | 0.79218  | 10    |
| 20  | 0.20999 | 776   | 9.99421 | 21    | 0.21574 | 796   | 0.78422  | 20    |
| 30  | 0.21761 | 762   | 9.99400 | 21    | 0.22381 | 783   | 0.77630  | 30    |
| 40  | 0.22509 | 748   | 9.99379 | 21    | 0.23130 | 769   | 0.76870  | 40    |
| 50  | 0.23244 | 735   | 9.99357 | 22    | 0.23947 | 757   | 0.76113  | 50    |
| 10 00   | 9.23967 | 723   | 9.99336 | 22    | 9.24632 | 745   | 10.75388 | 01 00 |
| 10  | 0.24677 | 710   | 9.99313 | 22    | 0.25345 | 733   | 0.74585  | 10    |
| 20  | 0.25376 | 699   | 9.99290 | 23    | 0.26046 | 721   | 0.73814  | 20    |
| 30  | 0.26063 | 687   | 9.99267 | 23    | 0.26747 | 711   | 0.73065  | 30    |
| 40  | 0.26739 | 676   | 9.99243 | 24    | 0.27446 | 699   | 0.72340  | 40    |
| 50  | 0.27405 | 666   | 9.99219 | 24    | 0.28145 | 689   | 0.71614  | 50    |
| 11 00   | 9.28080 | 655   | 9.99195 | 24    | 9.28905 | 679   | 10.71116 | 01 10 |
| 10  | 0.28705 | 645   | 9.99173 | 25    | 0.29615 | 670   | 10.69465 | 10    |
| 20  | 0.29340 | 635   | 9.99151 | 25    | 0.30316 | 660   | 10.67814 | 20    |
| 30  | 0.29985 | 625   | 9.99129 | 25    | 0.31017 | 651   | 10.66163 | 30    |
| 40  | 0.30632 | 617   | 9.99107 | 25    | 0.31718 | 642   | 10.64512 | 40    |
| 50  | 0.31289 | 607   | 9.99085 | 25    | 0.32422 | 634   | 10.62861 | 50    |
| 12 00   | 9.32195 | 599   | 9.99063 | 27    | 9.32747 | 625   | 10.61212 | 01 20 |
| 10  | 0.32873 | 590   | 9.99041 | 27    | 0.33453 | 617   | 10.59561 | 10    |
| 20  | 0.33560 | 582   | 9.99019 | 27    | 0.34159 | 608   | 10.57910 | 20    |
| 30  | 0.34254 | 575   | 9.99000 | 28    | 0.34865 | 601   | 10.56259 | 30    |
| 40  | 0.34954 | 569   | 9.98980 | 28    | 0.35571 | 594   | 10.54608 | 40    |
| 50  | 0.35659 | 562   | 9.98960 | 29    | 0.36277 | 587   | 10.52957 | 50    |
| Cosine. Tang. Sine. Tang. Secant. Tang. Secant. Tang. |         |       |         |       |         |       |          |       |

TABLE V.—Common logarithms of circular functions.—Continued.

| Arc.  | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |       |
|-------|---------|-------|---------|-------|---------|-------|----------|-------|
| 13 00 | 9.35209 | 551   | 9.98873 | 29    | 9.38336 | 579   | 10.63864 | 77 00 |
| 10    | .35752  | 543   | .98843  | 29    | .38309  | 573   | .63891   | 50    |
| 20    | .36299  | 537   | .98813  | 30    | .37476  | 567   | .63924   | 40    |
| 30    | .36848  | 528   | .98783  | 30    | .36635  | 559   | .63956   | 30    |
| 40    | .37241  | 523   | .98753  | 30    | .35799  | 554   | .63984   | 20    |
| 50    | .37688  | 517   | .98722  | 31    | .34936  | 547   | .64064   | 10    |
| 14 00 | 9.38367 | 509   | 9.98890 | 32    | 9.39677 | 541   | 10.60323 | 76 00 |
| 10    | .38871  | 504   | .98859  | 31    | .40212  | 535   | .59788   | 50    |
| 20    | .39368  | 497   | .98827  | 32    | .40742  | 530   | .59858   | 40    |
| 30    | .39860  | 492   | .98794  | 33    | .41266  | 524   | .59734   | 30    |
| 40    | .40345  | 485   | .98761  | 33    | .41784  | 518   | .58216   | 20    |
| 50    | .40825  | 480   | .98728  | 33    | .42297  | 513   | .57703   | 10    |
| 15 00 | 9.41300 | 475   | 9.98494 | 34    | 9.42805 | 508   | 10.57185 | 75 00 |
| 10    | .41768  | 468   | .98460  | 34    | .43308  | 503   | .56692   | 50    |
| 20    | .42232  | 464   | .98426  | 34    | .43806  | 498   | .56194   | 40    |
| 30    | .42690  | 458   | .98391  | 35    | .44299  | 493   | .55701   | 30    |
| 40    | .43143  | 453   | .98356  | 35    | .44787  | 488   | .55213   | 20    |
| 50    | .43591  | 448   | .98320  | 36    | .45271  | 484   | .54729   | 10    |
| 16 00 | 9.44034 | 443   | 9.98284 | 36    | 9.45750 | 479   | 10.54250 | 74 00 |
| 10    | .44472  | 438   | .98248  | 36    | .46224  | 474   | .53776   | 50    |
| 20    | .44905  | 433   | .98211  | 37    | .46694  | 470   | .53305   | 40    |
| 30    | .45334  | 429   | .98174  | 37    | .47160  | 466   | .52839   | 30    |
| 40    | .45758  | 424   | .98136  | 38    | .47622  | 462   | .52378   | 20    |
| 50    | .46178  | 420   | .98098  | 38    | .48080  | 458   | .51920   | 10    |
| 17 00 | 9.46593 | 415   | 9.98060 | 38    | 9.48534 | 454   | 10.51466 | 73 00 |
| 10    | .47005  | 412   | .98021  | 39    | .48984  | 450   | .51016   | 50    |
| 20    | .47411  | 406   | .97982  | 39    | .49430  | 446   | .50570   | 40    |
| 30    | .47814  | 403   | .97942  | 40    | .49872  | 442   | .50128   | 30    |
| 40    | .48213  | 399   | .97902  | 40    | .50311  | 439   | .49689   | 20    |
| 50    | .48607  | 394   | .97861  | 41    | .50746  | 435   | .49254   | 10    |
| 18 00 | 9.49998 | 391   | 9.97821 | 40    | 9.51178 | 432   | 10.48828 | 72 00 |
| 10    | .49385  | 387   | .97779  | 42    | .51606  | 428   | .48394   | 50    |
| 20    | .49768  | 383   | .97738  | 41    | .52030  | 424   | .47959   | 40    |
| 30    | .50148  | 380   | .97696  | 42    | .52452  | 422   | .47533   | 30    |
| 40    | .50523  | 375   | .97653  | 43    | .52870  | 418   | .47130   | 20    |
| 50    | .50896  | 373   | .97610  | 43    | .53285  | 415   | .46715   | 10    |
| 19 00 | 9.51264 | 368   | 9.97567 | 43    | 9.53693 | 412   | 10.46303 | 71 00 |
| 10    | .51629  | 365   | .97523  | 44    | .54106  | 409   | .45894   | 50    |
| 20    | .51991  | 362   | .97479  | 44    | .54512  | 406   | .45488   | 40    |
| 30    | .52349  | 358   | .97435  | 44    | .54915  | 403   | .45085   | 30    |
| 40    | .52705  | 356   | .97390  | 45    | .55315  | 400   | .44685   | 20    |
| 50    | .53056  | 351   | .97344  | 46    | .55712  | 397   | .44288   | 10    |
| 20 00 | 9.53905 | 349   | 9.97299 | 45    | 9.56107 | 395   | 10.43898 | 70 00 |
| 10    | .53751  | 346   | .97252  | 47    | .56498  | 391   | .43492   | 50    |
| 20    | .54093  | 342   | .97206  | 46    | .56887  | 389   | .43113   | 40    |
| 30    | .54432  | 339   | .97159  | 47    | .57274  | 387   | .42726   | 30    |
| 40    | .54769  | 337   | .97111  | 48    | .57658  | 384   | .42342   | 20    |
| 50    | .55102  | 333   | .97063  | 48    | .58039  | 381   | .41961   | 10    |
| 21 00 | 9.55433 | 331   | 9.97015 | 48    | 9.58416 | 379   | 10.41582 | 69 00 |
| 10    | .55761  | 328   | .96966  | 49    | .58794  | 376   | .41206   | 50    |
| 20    | .56085  | 324   | .96917  | 49    | .59168  | 374   | .40832   | 40    |
| 30    | .56407  | 322   | .96868  | 49    | .59540  | 372   | .40460   | 30    |
| 40    | .56727  | 320   | .96818  | 50    | .59909  | 369   | .40091   | 20    |
| 50    | .57043  | 316   | .96767  | 51    | .60276  | 367   | .39724   | 10    |
|       | Cosine. | Diff. | Sine.   | Diff. | Cotang. | Diff. | Tang.    | Arc.  |

TABLE V.—Common logarithms of circular functions—Continued.

| Arc.  | Sine.   | Diff. | Costne. | Diff. | Tang.   | Diff. | Cotang.  | Arc.  |
|-------|---------|-------|---------|-------|---------|-------|----------|-------|
| 22 00 | 9.52357 | 314   | 9.96717 | 50    | 9.60641 | 365   | 10.39359 | 68 00 |
| 10    | .52669  | 312   | .96665  | 52    | .61004  | 363   | .38996   | 50    |
| 20    | .52978  | 309   | .96614  | 51    | .61364  | 360   | .38636   | 40    |
| 30    | .53284  | 306   | .96561  | 53    | .61722  | 358   | .38278   | 30    |
| 40    | .53588  | 304   | .96509  | 52    | .62079  | 357   | .37921   | 20    |
| 50    | .53899  | 301   | .96456  | 53    | .62433  | 354   | .37567   | 10    |
| 23 00 | 9.53188 | 299   | 9.96408 | 53    | 9.62785 | 352   | 10.37215 | 67 00 |
| 10    | .53484  | 296   | .96349  | 54    | .63135  | 350   | .36864   | 50    |
| 20    | .53778  | 294   | .96294  | 55    | .63484  | 349   | .36516   | 40    |
| 30    | .54070  | 292   | .96240  | 54    | .63830  | 346   | .36170   | 30    |
| 40    | .54359  | 289   | .96185  | 55    | .64175  | 345   | .35825   | 20    |
| 50    | .54646  | 287   | .96129  | 56    | .64517  | 342   | .35483   | 10    |
| 24 00 | 9.53931 | 285   | 9.96073 | 56    | 9.64858 | 341   | 10.35142 | 66 00 |
| 10    | .54214  | 283   | .96016  | 57    | .65197  | 339   | .34803   | 50    |
| 20    | .54494  | 280   | .95960  | 56    | .65535  | 338   | .34465   | 40    |
| 30    | .54773  | 279   | .95902  | 58    | .65870  | 335   | .34130   | 30    |
| 40    | .55049  | 276   | .95844  | 58    | .66204  | 334   | .33796   | 20    |
| 50    | .55323  | 274   | .95786  | 58    | .66537  | 333   | .33463   | 10    |
| 25 00 | 9.53935 | 272   | 9.95728 | 58    | 9.66867 | 330   | 10.33133 | 65 00 |
| 10    | .53865  | 270   | .95668  | 60    | .67196  | 329   | .32804   | 50    |
| 20    | .53133  | 268   | .95609  | 59    | .67524  | 328   | .32476   | 40    |
| 30    | .53898  | 265   | .95549  | 60    | .67850  | 326   | .32150   | 30    |
| 40    | .53662  | 264   | .95488  | 61    | .68174  | 324   | .31826   | 20    |
| 50    | .53924  | 262   | .95427  | 61    | .68497  | 323   | .31503   | 10    |
| 26 00 | 9.54184 | 260   | 9.95366 | 60    | 9.68818 | 321   | 10.31182 | 64 00 |
| 10    | .54442  | 258   | .95304  | 62    | .69138  | 320   | .30862   | 50    |
| 20    | .54698  | 256   | .95242  | 62    | .69457  | 319   | .30543   | 40    |
| 30    | .54953  | 255   | .95179  | 63    | .69774  | 317   | .30226   | 30    |
| 40    | .55205  | 252   | .95116  | 63    | .70089  | 315   | .29911   | 20    |
| 50    | .55456  | 251   | .95052  | 64    | .70404  | 315   | .29596   | 10    |
| 27 00 | 9.55705 | 249   | 9.94988 | 64    | 9.70717 | 313   | 10.29283 | 63 00 |
| 10    | .55952  | 247   | .94923  | 65    | .71028  | 311   | .28972   | 50    |
| 20    | .56197  | 245   | .94858  | 65    | .71339  | 311   | .28661   | 40    |
| 30    | .56441  | 244   | .94793  | 65    | .71648  | 309   | .28352   | 30    |
| 40    | .56682  | 241   | .94727  | 66    | .71955  | 307   | .28044   | 20    |
| 50    | .56922  | 240   | .94660  | 67    | .72262  | 307   | .27738   | 10    |
| 28 00 | 9.57161 | 239   | 9.94593 | 67    | 9.72567 | 305   | 10.27433 | 62 00 |
| 10    | .57398  | 237   | .94526  | 67    | .72872  | 305   | .27128   | 50    |
| 20    | .57633  | 235   | .94458  | 68    | .73175  | 303   | .26825   | 40    |
| 30    | .57866  | 233   | .94390  | 68    | .73476  | 301   | .26524   | 30    |
| 40    | .58098  | 232   | .94321  | 69    | .73777  | 301   | .26223   | 20    |
| 50    | .58328  | 230   | .94252  | 69    | .74077  | 300   | .25923   | 10    |
| 29 00 | 9.58557 | 229   | 9.94182 | 70    | 9.74375 | 298   | 10.25625 | 61 00 |
| 10    | .58784  | 227   | .94112  | 70    | .74673  | 299   | .25327   | 50    |
| 20    | .59010  | 226   | .94041  | 71    | .74969  | 296   | .25031   | 40    |
| 30    | .59234  | 224   | .93970  | 71    | .75264  | 295   | .24736   | 30    |
| 40    | .59456  | 222   | .93898  | 72    | .75558  | 294   | .24441   | 20    |
| 50    | .59677  | 221   | .93826  | 72    | .75852  | 294   | .24148   | 10    |
| 30 00 | 9.59897 | 220   | 9.93753 | 73    | 9.76144 | 292   | 10.23856 | 60 00 |
| 10    | .60115  | 218   | .93680  | 73    | .76435  | 291   | .23565   | 50    |
| 20    | .60332  | 217   | .93606  | 74    | .76725  | 290   | .23274   | 40    |
| 30    | .60547  | 215   | .93532  | 74    | .77015  | 290   | .22985   | 30    |
| 40    | .60761  | 214   | .93457  | 75    | .77303  | 288   | .22697   | 20    |
| 50    | .60973  | 212   | .93382  | 75    | .77591  | 288   | .22409   | 10    |
|       | Costne. | Diff. | Sine.   | Diff. | Cotang. | Diff. | Tang.    | Arc.  |



TABLE V.—Common logarithms of circular functions—Continued.

| Arc.  | Sine.   | Diff. | Cosine. | Diff. | Tang.   | Diff. | Cotang.  |       |
|-------|---------|-------|---------|-------|---------|-------|----------|-------|
| 31 00 | 9.71184 | 211   | 9.93307 | 75    | 9.77877 | 286   | 10.22123 | 59 00 |
| 10    | .71393  | 209   | .93230  | 77    | .78163  | 286   | .21837   | 50    |
| 20    | .71602  | 209   | .93154  | 76    | .78448  | 285   | .21552   | 40    |
| 30    | .71808  | 206   | .93077  | 77    | .78732  | 284   | .21268   | 30    |
| 40    | .72014  | 206   | .92999  | 78    | .79015  | 283   | .20985   | 20    |
| 50    | .72218  | 204   | .92921  | 78    | .79297  | 282   | .20703   | 10    |
| 32 00 | 9.72421 | 203   | 9.92842 | 79    | 9.79579 | 282   | 10.20421 | 58 00 |
| 10    | .72622  | 201   | .92763  | 79    | .79860  | 281   | .20140   | 50    |
| 20    | .72823  | 201   | .92683  | 80    | .80140  | 280   | .19860   | 40    |
| 30    | .73022  | 199   | .92603  | 80    | .80419  | 279   | .19581   | 30    |
| 40    | .73219  | 197   | .92522  | 81    | .80697  | 278   | .19303   | 20    |
| 50    | .73416  | 197   | .92441  | 81    | .80975  | 278   | .19025   | 10    |
| 33 00 | 9.73611 | 195   | 9.92359 | 82    | 9.81252 | 277   | 10.18748 | 57 00 |
| 10    | .73805  | 194   | .92277  | 82    | .81528  | 276   | .18472   | 50    |
| 20    | .73997  | 192   | .92194  | 83    | .81803  | 275   | .18196   | 40    |
| 30    | .74189  | 192   | .92111  | 83    | .82078  | 275   | .17922   | 30    |
| 40    | .74379  | 190   | .92027  | 84    | .82352  | 274   | .17648   | 20    |
| 50    | .74568  | 189   | .91942  | 85    | .82626  | 274   | .17374   | 10    |
| 34 00 | 9.74756 | 188   | 9.91857 | 85    | 9.82899 | 273   | 10.17101 | 56 00 |
| 10    | .74943  | 187   | .91772  | 85    | .83171  | 272   | .16829   | 50    |
| 20    | .75128  | 185   | .91686  | 86    | .83442  | 271   | .16557   | 40    |
| 30    | .75313  | 185   | .91599  | 87    | .83713  | 271   | .16287   | 30    |
| 40    | .75496  | 183   | .91512  | 87    | .83984  | 271   | .16016   | 20    |
| 50    | .75678  | 182   | .91425  | 87    | .84253  | 269   | .15746   | 10    |
| 35 00 | 9.75859 | 181   | 9.91336 | 89    | 9.84523 | 270   | 10.15477 | 55 00 |
| 10    | .76039  | 180   | .91248  | 88    | .84791  | 268   | .15209   | 50    |
| 20    | .76218  | 179   | .91158  | 90    | .85059  | 268   | .14941   | 40    |
| 30    | .76395  | 177   | .91069  | 89    | .85327  | 268   | .14673   | 30    |
| 40    | .76572  | 177   | .90978  | 91    | .85594  | 267   | .14406   | 20    |
| 50    | .76747  | 175   | .90887  | 91    | .85860  | 266   | .14140   | 10    |
| 36 00 | 9.76922 | 175   | 9.90796 | 91    | 9.86126 | 266   | 10.13874 | 54 00 |
| 10    | .77095  | 173   | .90704  | 92    | .86391  | 265   | .13608   | 50    |
| 20    | .77267  | 172   | .90611  | 93    | .86656  | 265   | .13344   | 40    |
| 30    | .77439  | 172   | .90518  | 93    | .86921  | 265   | .13079   | 30    |
| 40    | .77609  | 170   | .90424  | 94    | .87185  | 264   | .12815   | 20    |
| 50    | .77778  | 169   | .90330  | 94    | .87448  | 263   | .12552   | 10    |
| 37 00 | 9.77946 | 168   | 9.90235 | 95    | 9.87711 | 263   | 10.12289 | 53 00 |
| 10    | .78113  | 167   | .90139  | 96    | .87974  | 263   | .12026   | 50    |
| 20    | .78280  | 167   | .90043  | 96    | .88236  | 262   | .11764   | 40    |
| 30    | .78445  | 165   | .89947  | 96    | .88498  | 262   | .11502   | 30    |
| 40    | .78609  | 164   | .89849  | 98    | .88759  | 261   | .11241   | 20    |
| 50    | .78772  | 163   | .89752  | 97    | .89020  | 261   | .10980   | 10    |
| 38 00 | 9.78934 | 162   | 9.89653 | 99    | 9.89281 | 261   | 10.10719 | 52 00 |
| 10    | .79095  | 161   | .89554  | 99    | .89541  | 260   | .10459   | 50    |
| 20    | .79256  | 161   | .89455  | 99    | .89801  | 260   | .10199   | 40    |
| 30    | .79415  | 159   | .89354  | 101   | .90060  | 259   | .09939   | 30    |
| 40    | .79573  | 158   | .89254  | 100   | .90320  | 260   | .09680   | 20    |
| 50    | .79731  | 158   | .89152  | 102   | .90578  | 258   | .09421   | 10    |
| 39 00 | 9.79887 | 156   | 9.89050 | 102   | 9.90837 | 259   | 10.09163 | 51 00 |
| 10    | .80043  | 156   | .88948  | 102   | .91095  | 258   | .08905   | 50    |
| 20    | .80197  | 154   | .88844  | 104   | .91353  | 258   | .08647   | 40    |
| 30    | .80351  | 154   | .88741  | 103   | .91610  | 257   | .08390   | 30    |
| 40    | .80504  | 153   | .88636  | 105   | .91868  | 258   | .08132   | 20    |
| 50    | .80656  | 152   | .88531  | 105   | .92125  | 257   | .07875   | 10    |
|       | Cosine. | Diff. | Sine.   | Diff. | Cotang. | Diff. | Tang.    | Arc.  |

TABLE V.—Common logarithms of circular functions—Continued.

| Arc.  | Sine.   | Diff. | Cosine. | Diff. | Tang.    | Diff. | Cotang.  |       |
|-------|---------|-------|---------|-------|----------|-------|----------|-------|
| 40 00 | 0.80807 | 151   | 0.88425 | 106   | 0.97281  | 256   | 10.07618 | 50 00 |
| 10    | .80857  | 150   | .88319  | 106   | .97338   | 257   | .07362   | 50    |
| 20    | .81106  | 149   | .88212  | 107   | .97394   | 256   | .07106   | 40    |
| 30    | .81254  | 148   | .88105  | 107   | .97450   | 256   | .06850   | 30    |
| 40    | .81402  | 148   | .87998  | 109   | .97506   | 256   | .06594   | 20    |
| 50    | .81548  | 146   | .87887  | 109   | .97561   | 255   | .06339   | 10    |
| 41 00 | 0.81694 | 146   | 0.87778 | 109   | 0.97616  | 255   | 10.06084 | 49 00 |
| 10    | .81839  | 145   | .87668  | 110   | .97671   | 255   | .05829   | 50    |
| 20    | .81983  | 144   | .87557  | 111   | .97726   | 255   | .05574   | 40    |
| 30    | .82126  | 143   | .87446  | 111   | .97781   | 255   | .05319   | 30    |
| 40    | .82269  | 143   | .87333  | 113   | .97835   | 254   | .05065   | 20    |
| 50    | .82410  | 141   | .87221  | 112   | .97890   | 255   | .04810   | 10    |
| 42 00 | 0.82551 | 141   | 0.87107 | 114   | 0.97944  | 254   | 10.04556 | 48 00 |
| 10    | .82691  | 140   | .86998  | 114   | .97998   | 254   | .04302   | 50    |
| 20    | .82830  | 139   | .86878  | 115   | .98052   | 254   | .04048   | 40    |
| 30    | .82968  | 138   | .86763  | 115   | .98105   | 253   | .03795   | 30    |
| 40    | .83106  | 138   | .86647  | 116   | .98159   | 254   | .03541   | 20    |
| 50    | .83242  | 136   | .86530  | 117   | .98212   | 253   | .03288   | 10    |
| 43 00 | 0.83378 | 136   | 0.86413 | 117   | 0.98266  | 254   | 10.03034 | 47 00 |
| 10    | .83513  | 135   | .86295  | 118   | .97219   | 253   | .02781   | 50    |
| 20    | .83648  | 135   | .86176  | 119   | .97472   | 253   | .02528   | 40    |
| 30    | .83781  | 133   | .86056  | 120   | .97725   | 253   | .02275   | 30    |
| 40    | .83914  | 133   | .85936  | 120   | .97978   | 258   | .02022   | 20    |
| 50    | .84046  | 132   | .85815  | 121   | .98231   | 253   | .01769   | 10    |
| 44 00 | 0.84177 | 131   | 0.85693 | 122   | 0.98484  | 253   | 10.01516 | 46 00 |
| 10    | .84308  | 131   | .85571  | 122   | .98736   | 252   | .01263   | 50    |
| 20    | .84437  | 129   | .85448  | 123   | .98989   | 253   | .01011   | 40    |
| 30    | .84566  | 129   | .85324  | 124   | .99242   | 253   | .00758   | 30    |
| 40    | .84694  | 128   | .85200  | 124   | .99495   | 253   | .00505   | 20    |
| 50    | .84822  | 128   | .85074  | 126   | .99747   | 252   | .00253   | 10    |
| 45 00 | 0.84948 | 126   | 0.84948 | 126   | 10.00000 | 258   | 10.00000 | 45 00 |
|       | Cosine. | Diff. | Sine.   | Diff. | Cotang.  | Diff. | Tang.    | Arc.  |

212. The slide rule is a contrivance for using logs. mechanically. It consists, figure 47, of a rule, in the middle of which is a slide. The edges of the groove and the edges of the slide are graduated, forming four scales called A, B, C, and D. An indicator, which can be set at any point, guides the eye in selecting opposite numbers. The slide rule deals with mantissas only. Characteristics must be obtained by inspection.

**To multiply.**—Move the slide to the *right* until 1 on scale B is opposite the smaller of the two numbers on A; the number on A opposite the larger of the two numbers on B is the product.

**To divide.**—Move the slide to the *left* until the divisor on B is under 1 on A. The number on A opposite the *dividend* on B is the quotient desired. **To multiply and divide simultaneously,** or to solve a proportion, set the divisor on B opposite one of the other numbers on A. The number on A opposite the third number on B is the result desired.

**To find the square of a number.**—Take the number on A opposite the given number on D.

**To find the square root.**—Take the number on D opposite the given number on A. In taking square roots use only the *left half* of A, for an odd number of figures in front of the decimal point, and the *right half* only for *even* number.

**To find a cube.**—Set 1 on B opposite the given number on D. The number on A opposite the given number on B is the cube desired.

**To find a cube root.**—Take the root approximately by inspection. Set this number on B opposite the given number on A. Note whether 1 on C is opposite the approximate root on D. If so, the approximate root is the correct one; if not, move the slide slightly one way or the other until the number on B opposite the given number, and the number on D opposite the one on C are the same. This number is the desired cube root.

Occasional users of the slide rule will do well to adhere to the simple operations above described. Regular users will study the theory and scope of the rule from one of the several treatises on the subject.

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000.

| No. | Square. | Cube.  | Square root. | Cube root. | No. | Square. | Cube.   | Square root. | Cube root. |
|-----|---------|--------|--------------|------------|-----|---------|---------|--------------|------------|
| 1   | 1       | 1      | 1.           | 1.         | 57  | 3249    | 185193  | 7.5498       | 3.8485     |
| 2   | 4       | 8      | 1.4142       | 1.2599     | 58  | 3364    | 195112  | 7.6158       | 3.8709     |
| 3   | 9       | 27     | 1.7321       | 1.4422     | 59  | 3481    | 205370  | 7.6811       | 3.8930     |
| 4   | 16      | 64     | 2.0000       | 1.5874     | 60  | 3600    | 216000  | 7.7460       | 3.9149     |
| 5   | 25      | 125    | 2.2361       | 1.7100     | 61  | 3721    | 226981  | 7.8102       | 3.9365     |
| 6   | 36      | 216    | 2.4495       | 1.8171     | 62  | 3844    | 238328  | 7.8740       | 3.9579     |
| 7   | 49      | 343    | 2.6458       | 1.9129     | 63  | 3969    | 250047  | 7.9373       | 3.9791     |
| 8   | 64      | 512    | 2.8284       | 2.0000     | 64  | 4096    | 262144  | 8.           | 4.         |
| 9   | 81      | 729    | 3.0000       | 2.0801     | 65  | 4225    | 274625  | 8.0623       | 4.0207     |
| 10  | 100     | 1000   | 3.1623       | 2.1544     | 66  | 4356    | 287496  | 8.1240       | 4.0412     |
| 11  | 121     | 1331   | 3.3166       | 2.2240     | 67  | 4489    | 300763  | 8.1854       | 4.0615     |
| 12  | 144     | 1728   | 3.4641       | 2.2894     | 68  | 4624    | 314432  | 8.2462       | 4.0817     |
| 13  | 169     | 2197   | 3.6056       | 2.3513     | 69  | 4761    | 328509  | 8.3066       | 4.1016     |
| 14  | 196     | 2744   | 3.7417       | 2.4101     | 70  | 4900    | 343000  | 8.3666       | 4.1213     |
| 15  | 225     | 3375   | 3.8730       | 2.4662     | 71  | 5041    | 357911  | 8.4261       | 4.1408     |
| 16  | 256     | 4096   | 4.           | 2.5198     | 72  | 5184    | 373248  | 8.4853       | 4.1602     |
| 17  | 289     | 4913   | 4.1231       | 2.5713     | 73  | 5329    | 389017  | 8.5440       | 4.1793     |
| 18  | 324     | 5832   | 4.2426       | 2.6207     | 74  | 5476    | 405224  | 8.6023       | 4.1983     |
| 19  | 361     | 6859   | 4.3589       | 2.6684     | 75  | 5625    | 421875  | 8.6603       | 4.2173     |
| 20  | 400     | 8000   | 4.4721       | 2.7144     | 76  | 5776    | 438976  | 8.7178       | 4.2363     |
| 21  | 441     | 9261   | 4.5826       | 2.7589     | 77  | 5929    | 456533  | 8.7756       | 4.2543     |
| 22  | 484     | 10648  | 4.6904       | 2.8020     | 78  | 6084    | 474552  | 8.8318       | 4.2727     |
| 23  | 529     | 12167  | 4.7956       | 2.8439     | 79  | 6241    | 493039  | 8.8883       | 4.2906     |
| 24  | 576     | 13824  | 4.8990       | 2.8845     | 80  | 6400    | 512000  | 8.9443       | 4.3089     |
| 25  | 625     | 15625  | 5.           | 2.9240     | 81  | 6561    | 531441  | 9.           | 4.3267     |
| 26  | 676     | 17576  | 5.0990       | 2.9625     | 82  | 6724    | 551368  | 9.0564       | 4.3445     |
| 27  | 729     | 19683  | 5.1962       | 3.0000     | 83  | 6889    | 571787  | 9.1104       | 4.3621     |
| 28  | 784     | 21952  | 5.2915       | 3.0366     | 84  | 7056    | 592704  | 9.1652       | 4.3795     |
| 29  | 841     | 24389  | 5.3852       | 3.0723     | 85  | 7225    | 614125  | 9.2195       | 4.3968     |
| 30  | 900     | 27000  | 5.4772       | 3.1072     | 86  | 7396    | 636056  | 9.2736       | 4.4140     |
| 31  | 961     | 29791  | 5.5678       | 3.1414     | 87  | 7569    | 658509  | 9.3274       | 4.4310     |
| 32  | 1024    | 32768  | 5.6569       | 3.1748     | 88  | 7744    | 681472  | 9.3808       | 4.4480     |
| 33  | 1089    | 35937  | 5.7446       | 3.2075     | 89  | 7921    | 704969  | 9.4340       | 4.4647     |
| 34  | 1156    | 39304  | 5.8310       | 3.2396     | 90  | 8100    | 729000  | 9.4868       | 4.4814     |
| 35  | 1225    | 42875  | 5.9161       | 3.2711     | 91  | 8281    | 753571  | 9.5394       | 4.4979     |
| 36  | 1296    | 46656  | 6.           | 3.3019     | 92  | 8464    | 778688  | 9.5917       | 4.5144     |
| 37  | 1369    | 50653  | 6.0828       | 3.3322     | 93  | 8649    | 804357  | 9.6437       | 4.5307     |
| 38  | 1444    | 54872  | 6.1644       | 3.3620     | 94  | 8836    | 830584  | 9.6954       | 4.5468     |
| 39  | 1521    | 59319  | 6.2460       | 3.3912     | 95  | 9025    | 857375  | 9.7468       | 4.5629     |
| 40  | 1600    | 64000  | 6.3246       | 3.4200     | 96  | 9216    | 884736  | 9.7980       | 4.5789     |
| 41  | 1681    | 68921  | 6.4081       | 3.4483     | 97  | 9409    | 912673  | 9.8489       | 4.5947     |
| 42  | 1764    | 74068  | 6.4897       | 3.4760     | 98  | 9604    | 941192  | 9.8995       | 4.6104     |
| 43  | 1849    | 79457  | 6.5674       | 3.5034     | 99  | 9801    | 970299  | 9.9499       | 4.6261     |
| 44  | 1936    | 85184  | 6.6332       | 3.5303     | 100 | 10000   | 1000000 | 10.          | 4.6416     |
| 45  | 2025    | 91225  | 6.7082       | 3.5569     | 101 | 10201   | 1030301 | 10.0499      | 4.6570     |
| 46  | 2116    | 97688  | 6.7823       | 3.5830     | 102 | 10404   | 1061296 | 10.0985      | 4.6725     |
| 47  | 2209    | 103823 | 6.8557       | 3.6088     | 103 | 10609   | 1092727 | 10.1469      | 4.6878     |
| 48  | 2304    | 110592 | 6.9282       | 3.6342     | 104 | 10816   | 1124664 | 10.1950      | 4.7027     |
| 49  | 2401    | 117949 | 7.           | 3.6593     | 105 | 11025   | 1157125 | 10.2429      | 4.7177     |
| 50  | 2500    | 125000 | 7.0711       | 3.6840     | 106 | 11236   | 1190101 | 10.2956      | 4.7326     |
| 51  | 2601    | 132651 | 7.1414       | 3.7089     | 107 | 11449   | 1223543 | 10.3441      | 4.7475     |
| 52  | 2704    | 140908 | 7.2111       | 3.7325     | 108 | 11664   | 1257512 | 10.3923      | 4.7622     |
| 53  | 2809    | 149777 | 7.2801       | 3.7563     | 109 | 11881   | 1292029 | 10.4403      | 4.7769     |
| 54  | 2916    | 159264 | 7.3485       | 3.7798     | 110 | 12100   | 1327100 | 10.4881      | 4.7914     |
| 55  | 3025    | 169375 | 7.4162       | 3.8030     | 111 | 12321   | 1362731 | 10.5357      | 4.8059     |
| 56  | 3136    | 175616 | 7.4833       | 3.8258     | 112 | 12544   | 1400028 | 10.5830      | 4.8203     |

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No. | Square. | Cube.   | Square root. | Cube root. | No. | Square. | Cube.    | Square root. | Cube root. |
|-----|---------|---------|--------------|------------|-----|---------|----------|--------------|------------|
| 113 | 12769   | 1442697 | 11.3001      | 4.8346     | 198 | 39204   | 7797888  | 13.8564      | 5.7690     |
| 114 | 12996   | 1481544 | 11.0771      | 4.8488     | 199 | 39601   | 7986507  | 13.8924      | 5.7790     |
| 115 | 13225   | 1520875 | 11.0738      | 4.8629     | 200 | 40000   | 8000000  | 13.9284      | 5.7890     |
| 116 | 13456   | 1560864 | 11.0708      | 4.8779     | 201 | 40401   | 8120601  | 13.9642      | 5.7989     |
| 117 | 13689   | 1601613 | 11.0187      | 4.8910     | 202 | 40804   | 8242408  | 14.0000      | 5.8089     |
| 118 | 13924   | 1643032 | 11.0628      | 4.9049     | 203 | 41209   | 8365427  | 14.0357      | 5.8189     |
| 119 | 14161   | 1685159 | 11.0607      | 4.9187     | 204 | 41616   | 8489664  | 14.0712      | 5.8289     |
| 120 | 14400   | 1728000 | 11.0545      | 4.9324     | 205 | 42025   | 8615125  | 14.1067      | 5.8389     |
| 121 | 14641   | 1771561 | 11.0484      | 4.9461     | 206 | 42436   | 8741816  | 14.1421      | 5.8489     |
| 122 | 14884   | 1815848 | 11.0454      | 4.9597     | 207 | 42849   | 8868743  | 14.1774      | 5.8589     |
| 123 | 15129   | 1860867 | 11.0905      | 4.9733     | 208 | 43264   | 8996912  | 14.2127      | 5.8689     |
| 124 | 15376   | 1906624 | 11.1355      | 4.9868     | 209 | 43681   | 9126329  | 14.2478      | 5.8789     |
| 125 | 15625   | 1953125 | 11.1803      | 5.0003     | 210 | 44100   | 9257000  | 14.2829      | 5.8889     |
| 126 | 15876   | 2000376 | 11.2250      | 5.0138     | 211 | 44521   | 9388931  | 14.3178      | 5.8989     |
| 127 | 16129   | 2048383 | 11.2694      | 5.0265     | 212 | 44944   | 9522128  | 14.3527      | 5.9089     |
| 128 | 16384   | 2097152 | 11.3137      | 5.0397     | 213 | 45369   | 9656597  | 14.3875      | 5.9189     |
| 129 | 16641   | 2146689 | 11.3578      | 5.0528     | 214 | 45796   | 9792344  | 14.4222      | 5.9289     |
| 130 | 16900   | 2197000 | 11.4018      | 5.0658     | 215 | 46225   | 9929375  | 14.4568      | 5.9389     |
| 131 | 17161   | 2248091 | 11.4455      | 5.0788     | 216 | 46656   | 10067696 | 14.4914      | 5.9489     |
| 132 | 17424   | 2299968 | 11.4891      | 5.0916     | 217 | 47089   | 10207323 | 14.5258      | 5.9589     |
| 133 | 17689   | 2352637 | 11.5326      | 5.1045     | 218 | 47524   | 10348252 | 14.5602      | 5.9689     |
| 134 | 17956   | 2406104 | 11.5758      | 5.1172     | 219 | 47961   | 10490489 | 14.5945      | 5.9789     |
| 135 | 18225   | 2460375 | 11.6190      | 5.1299     | 220 | 48400   | 10634000 | 14.6287      | 5.9889     |
| 136 | 18496   | 2515456 | 11.6619      | 5.1426     | 221 | 48841   | 10778781 | 14.6629      | 5.9989     |
| 137 | 18769   | 2571353 | 11.7047      | 5.1551     | 222 | 49284   | 10924832 | 14.6966      | 6.0089     |
| 138 | 19044   | 2628072 | 11.7473      | 5.1676     | 223 | 49729   | 11072157 | 14.7300      | 6.0189     |
| 139 | 19321   | 2685619 | 11.7898      | 5.1801     | 224 | 50176   | 11220764 | 14.7634      | 6.0289     |
| 140 | 19600   | 2744000 | 11.8322      | 5.1925     | 225 | 50625   | 11370655 | 14.7966      | 6.0389     |
| 141 | 19881   | 2803221 | 11.8743      | 5.2048     | 226 | 51076   | 11521832 | 14.8297      | 6.0489     |
| 142 | 20164   | 2863288 | 11.9164      | 5.2171     | 227 | 51529   | 11674297 | 14.8627      | 6.0589     |
| 143 | 20449   | 2924207 | 11.9583      | 5.2293     | 228 | 51984   | 11828052 | 14.8957      | 6.0689     |
| 144 | 20736   | 2985984 | 12.0000      | 5.2415     | 229 | 52441   | 11983109 | 14.9287      | 6.0789     |
| 145 | 21025   | 3048625 | 12.0416      | 5.2536     | 230 | 52900   | 12139472 | 14.9617      | 6.0889     |
| 146 | 21316   | 3112136 | 12.0830      | 5.2656     | 231 | 53361   | 12297143 | 14.9947      | 6.0989     |
| 147 | 21609   | 3176523 | 12.1244      | 5.2776     | 232 | 53824   | 12456128 | 15.0277      | 6.1089     |
| 148 | 21904   | 3241792 | 12.1655      | 5.2896     | 233 | 54289   | 12616437 | 15.0607      | 6.1189     |
| 149 | 22201   | 3307949 | 12.2066      | 5.3015     | 234 | 54756   | 12778072 | 15.0937      | 6.1289     |
| 150 | 22500   | 3375000 | 12.2474      | 5.3133     | 235 | 55225   | 12941043 | 15.1267      | 6.1389     |
| 151 | 22801   | 3442961 | 12.2882      | 5.3251     | 236 | 55696   | 13105360 | 15.1597      | 6.1489     |
| 152 | 23104   | 3511848 | 12.3288      | 5.3368     | 237 | 56169   | 13271023 | 15.1927      | 6.1589     |
| 153 | 23409   | 3581677 | 12.3693      | 5.3485     | 238 | 56644   | 13438032 | 15.2257      | 6.1689     |
| 154 | 23716   | 3652464 | 12.4097      | 5.3601     | 239 | 57121   | 13606387 | 15.2587      | 6.1789     |
| 155 | 24025   | 3724215 | 12.4499      | 5.3717     | 240 | 57600   | 13776092 | 15.2917      | 6.1889     |
| 156 | 24336   | 3796941 | 12.4900      | 5.3832     | 241 | 58081   | 13947157 | 15.3247      | 6.1989     |
| 157 | 24649   | 3869648 | 12.5300      | 5.3947     | 242 | 58564   | 14119582 | 15.3577      | 6.2089     |
| 158 | 24964   | 3943332 | 12.5698      | 5.4061     | 243 | 59049   | 14293367 | 15.3907      | 6.2189     |
| 159 | 25281   | 4017999 | 12.6095      | 5.4175     | 244 | 59536   | 14468512 | 15.4237      | 6.2289     |
| 160 | 25600   | 4093650 | 12.6491      | 5.4288     | 245 | 60025   | 14645027 | 15.4567      | 6.2389     |
| 161 | 25921   | 4170281 | 12.6886      | 5.4401     | 246 | 60516   | 14822902 | 15.4897      | 6.2489     |
| 162 | 26244   | 4247892 | 12.7279      | 5.4514     | 247 | 61009   | 15002147 | 15.5227      | 6.2589     |
| 163 | 26569   | 4326483 | 12.7671      | 5.4626     | 248 | 61504   | 15182752 | 15.5557      | 6.2689     |
| 164 | 26896   | 4406064 | 12.8062      | 5.4737     | 249 | 62001   | 15364717 | 15.5887      | 6.2789     |
| 165 | 27225   | 4486645 | 12.8452      | 5.4848     | 250 | 62500   | 15548042 | 15.6217      | 6.2889     |
| 166 | 27556   | 4568226 | 12.8841      | 5.4959     | 251 | 63001   | 15732727 | 15.6547      | 6.2989     |
| 167 | 27889   | 4650807 | 12.9228      | 5.5069     | 252 | 63504   | 15918772 | 15.6877      | 6.3089     |
| 168 | 28224   | 4734388 | 12.9615      | 5.5178     | 253 | 64009   | 16106187 | 15.7207      | 6.3189     |
| 169 | 28561   | 4818969 | 13.0000      | 5.5288     | 254 | 64516   | 16294972 | 15.7537      | 6.3289     |
| 170 | 28900   | 4913000 | 13.0384      | 5.5397     | 255 | 65025   | 16485127 | 15.7867      | 6.3389     |
| 171 | 29241   | 5007521 | 13.0767      | 5.5506     | 256 | 65536   | 16676652 | 15.8197      | 6.3489     |
| 172 | 29584   | 5092548 | 13.1149      | 5.5613     | 257 | 66049   | 16869557 | 15.8527      | 6.3589     |
| 173 | 29929   | 5178077 | 13.1529      | 5.5721     | 258 | 66564   | 17063832 | 15.8857      | 6.3689     |
| 174 | 30276   | 5264204 | 13.1909      | 5.5828     | 259 | 67081   | 17259477 | 15.9187      | 6.3789     |
| 175 | 30625   | 5350937 | 13.2288      | 5.5934     | 260 | 67600   | 17456492 | 15.9517      | 6.3889     |
| 176 | 30976   | 5438272 | 13.2665      | 5.6041     | 261 | 68121   | 17654877 | 15.9847      | 6.3989     |
| 177 | 31329   | 5526213 | 13.3041      | 5.6147     | 262 | 68644   | 17854632 | 16.0177      | 6.4089     |
| 178 | 31684   | 5614764 | 13.3417      | 5.6252     | 263 | 69169   | 18055757 | 16.0507      | 6.4189     |
| 179 | 32041   | 5703929 | 13.3791      | 5.6357     | 264 | 69696   | 18258252 | 16.0837      | 6.4289     |
| 180 | 32400   | 5793700 | 13.4164      | 5.6462     | 265 | 70225   | 18462127 | 16.1167      | 6.4389     |
| 181 | 32761   | 5884081 | 13.4536      | 5.6567     | 266 | 70756   | 18667382 | 16.1497      | 6.4489     |
| 182 | 33124   | 5975068 | 13.4907      | 5.6671     | 267 | 71289   | 18874017 | 16.1827      | 6.4589     |
| 183 | 33489   | 6066669 | 13.5277      | 5.6774     | 268 | 71824   | 19082032 | 16.2157      | 6.4689     |
| 184 | 33856   | 6158892 | 13.5647      | 5.6877     | 269 | 72361   | 19291447 | 16.2487      | 6.4789     |
| 185 | 34225   | 6251735 | 13.6015      | 5.6980     | 270 | 72900   | 19502272 | 16.2817      | 6.4889     |
| 186 | 34596   | 6345192 | 13.6382      | 5.7083     |     |         |          |              |            |
| 187 | 34969   | 6439269 | 13.6748      | 5.7185     |     |         |          |              |            |
| 188 | 35344   | 6533972 | 13.7113      | 5.7287     |     |         |          |              |            |
| 189 | 35721   | 6629309 | 13.7477      | 5.7389     |     |         |          |              |            |
| 190 | 36100   | 6725280 | 13.7840      | 5.7490     |     |         |          |              |            |
| 191 | 36481   | 6821897 | 13.8202      | 5.7590     |     |         |          |              |            |

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No. | Square. | Cube.    | Square root. | Cube root. | No. | Square. | Cube.    | Square root. | Cube root. |
|-----|---------|----------|--------------|------------|-----|---------|----------|--------------|------------|
| 271 | 73441   | 19902511 | 16.4631      | 6.4713     | 309 | 122500  | 42875000 | 18.7083      | 7.0472     |
| 272 | 73984   | 20323648 | 16.4924      | 6.4702     | 310 | 123201  | 43243551 | 18.7350      | 7.0540     |
| 273 | 74529   | 20646417 | 16.5227      | 6.4872     | 311 | 123904  | 43614209 | 18.7617      | 7.0607     |
| 274 | 75076   | 20970824 | 16.5529      | 6.4951     | 312 | 124609  | 43986977 | 18.7883      | 7.0674     |
| 275 | 75625   | 20796875 | 16.5831      | 6.5030     | 313 | 125316  | 44361964 | 18.8149      | 7.0740     |
| 276 | 76176   | 21024576 | 16.6132      | 6.5108     | 314 | 126025  | 44738875 | 18.8414      | 7.0807     |
| 277 | 76729   | 21253933 | 16.6433      | 6.5187     | 315 | 126736  | 45118016 | 18.8680      | 7.0873     |
| 278 | 77284   | 21484952 | 16.6733      | 6.5265     | 316 | 127449  | 45499293 | 18.8944      | 7.0940     |
| 279 | 77841   | 21717639 | 16.7033      | 6.5343     | 317 | 128164  | 45882712 | 18.9209      | 7.1006     |
| 280 | 78400   | 21952000 | 16.7332      | 6.5421     | 318 | 128881  | 46268279 | 18.9473      | 7.1072     |
| 281 | 78961   | 22188041 | 16.7631      | 6.5499     | 319 | 129600  | 46656000 | 18.9737      | 7.1138     |
| 282 | 79524   | 22425768 | 16.7929      | 6.5577     | 320 | 130321  | 47045581 | 19.          | 7.1204     |
| 283 | 80089   | 22665187 | 16.8226      | 6.5654     | 321 | 131044  | 47437928 | 19.0263      | 7.1269     |
| 284 | 80656   | 22906304 | 16.8523      | 6.5731     | 322 | 131769  | 47832147 | 19.0526      | 7.1335     |
| 285 | 81225   | 23149125 | 16.8819      | 6.5808     | 323 | 132496  | 48228544 | 19.0788      | 7.1400     |
| 286 | 81796   | 23393656 | 16.9115      | 6.5885     | 324 | 133225  | 48626275 | 19.1050      | 7.1465     |
| 287 | 82369   | 23639903 | 16.9411      | 6.5963     | 325 | 133956  | 49026396 | 19.1311      | 7.1531     |
| 288 | 82944   | 23887872 | 16.9706      | 6.6040     | 326 | 134689  | 49428863 | 19.1572      | 7.1596     |
| 289 | 83521   | 24137569 | 17.          | 6.6115     | 327 | 135424  | 49833682 | 19.1833      | 7.1661     |
| 290 | 84100   | 24389000 | 17.0294      | 6.6191     | 328 | 136161  | 50240409 | 19.2094      | 7.1726     |
| 291 | 84681   | 24642171 | 17.0587      | 6.6267     | 329 | 136900  | 50649000 | 19.2354      | 7.1791     |
| 292 | 85264   | 24897088 | 17.0880      | 6.6343     | 330 | 137641  | 51059481 | 19.2614      | 7.1855     |
| 293 | 85849   | 25153757 | 17.1172      | 6.6419     | 331 | 138384  | 51471884 | 19.2873      | 7.1920     |
| 294 | 86436   | 25412184 | 17.1464      | 6.6494     | 332 | 139129  | 51886117 | 19.3132      | 7.1984     |
| 295 | 87025   | 25672375 | 17.1756      | 6.6568     | 333 | 139876  | 52302362 | 19.3391      | 7.2048     |
| 296 | 87616   | 25934336 | 17.2047      | 6.6644     | 334 | 140625  | 52720475 | 19.3649      | 7.2112     |
| 297 | 88209   | 26198073 | 17.2337      | 6.6719     | 335 | 141376  | 53140376 | 19.3907      | 7.2177     |
| 298 | 88804   | 26463592 | 17.2627      | 6.6794     | 336 | 142129  | 53562633 | 19.4165      | 7.2240     |
| 299 | 89401   | 26730999 | 17.2916      | 6.6868     | 337 | 142884  | 53986264 | 19.4422      | 7.2304     |
| 300 | 90000   | 27000000 | 17.3205      | 6.6943     | 338 | 143641  | 54411269 | 19.4679      | 7.2368     |
| 301 | 90601   | 27270901 | 17.3494      | 6.7018     | 339 | 144400  | 54837708 | 19.4936      | 7.2432     |
| 302 | 91204   | 27543608 | 17.3781      | 6.7092     | 340 | 145161  | 55265631 | 19.5192      | 7.2495     |
| 303 | 91809   | 27818127 | 17.4069      | 6.7166     | 341 | 145924  | 55694968 | 19.5448      | 7.2558     |
| 304 | 92416   | 28094464 | 17.4356      | 6.7240     | 342 | 146689  | 56125767 | 19.5704      | 7.2622     |
| 305 | 93025   | 28372625 | 17.4642      | 6.7313     | 343 | 147456  | 56558014 | 19.5959      | 7.2685     |
| 306 | 93636   | 28652616 | 17.4929      | 6.7387     | 344 | 148225  | 56991663 | 19.6214      | 7.2748     |
| 307 | 94249   | 28934443 | 17.5214      | 6.7460     | 345 | 149000  | 57426716 | 19.6469      | 7.2811     |
| 308 | 94864   | 29218112 | 17.5499      | 6.7533     | 346 | 149776  | 57863169 | 19.6723      | 7.2874     |
| 309 | 95481   | 29503629 | 17.5784      | 6.7606     | 347 | 150554  | 58301000 | 19.6977      | 7.2936     |
| 310 | 96100   | 29791000 | 17.6068      | 6.7679     | 348 | 151334  | 58740269 | 19.7231      | 7.3000     |
| 311 | 96721   | 30080231 | 17.6352      | 6.7752     | 349 | 152116  | 59180900 | 19.7484      | 7.3063     |
| 312 | 97344   | 30371328 | 17.6635      | 6.7824     | 350 | 152900  | 59622961 | 19.7737      | 7.3126     |
| 313 | 97969   | 30664297 | 17.6918      | 6.7897     | 351 | 153686  | 60066454 | 19.7990      | 7.3189     |
| 314 | 98596   | 30959144 | 17.7200      | 6.7969     | 352 | 154474  | 60511469 | 19.8242      | 7.3252     |
| 315 | 99225   | 31255875 | 17.7482      | 6.8041     | 353 | 155264  | 60958006 | 19.8494      | 7.3315     |
| 316 | 99856   | 31554496 | 17.7764      | 6.8113     | 354 | 156056  | 61406075 | 19.8746      | 7.3377     |
| 317 | 100489  | 31855013 | 17.8045      | 6.8185     | 355 | 156850  | 61855684 | 19.8997      | 7.3440     |
| 318 | 101124  | 32157432 | 17.8326      | 6.8256     | 356 | 157646  | 62306833 | 19.9249      | 7.3502     |
| 319 | 101761  | 32461759 | 17.8606      | 6.8328     | 357 | 158444  | 62759522 | 19.9500      | 7.3564     |
| 320 | 102400  | 32768000 | 17.8885      | 6.8399     | 358 | 159244  | 63213761 | 19.9750      | 7.3626     |
| 321 | 103041  | 33076161 | 17.9165      | 6.8470     | 359 | 160046  | 63669550 | 20.          | 7.3688     |
| 322 | 103684  | 33386248 | 17.9444      | 6.8541     | 360 | 160850  | 64126899 | 20.0250      | 7.3750     |
| 323 | 104329  | 33698267 | 17.9722      | 6.8612     | 361 | 161656  | 64585808 | 20.0499      | 7.3812     |
| 324 | 104976  | 34012224 | 18.          | 6.8683     | 362 | 162464  | 65046277 | 20.0748      | 7.3874     |
| 325 | 105625  | 34328125 | 18.0278      | 6.8753     | 363 | 163274  | 65508306 | 20.0996      | 7.3936     |
| 326 | 106276  | 34645976 | 18.0555      | 6.8824     | 364 | 164086  | 65971895 | 20.1244      | 7.4000     |
| 327 | 106929  | 34965783 | 18.0831      | 6.8894     | 365 | 164900  | 66437044 | 20.1491      | 7.4062     |
| 328 | 107584  | 35287552 | 18.1108      | 6.8964     | 366 | 165716  | 66903763 | 20.1737      | 7.4125     |
| 329 | 108241  | 35611289 | 18.1384      | 6.9034     | 367 | 166534  | 67372052 | 20.1983      | 7.4188     |
| 330 | 108900  | 35937000 | 18.1659      | 6.9104     | 368 | 167354  | 67841911 | 20.2228      | 7.4251     |
| 331 | 109561  | 36264691 | 18.1934      | 6.9174     | 369 | 168176  | 68313340 | 20.2473      | 7.4314     |
| 332 | 110224  | 36594368 | 18.2209      | 6.9244     | 370 | 169000  | 68786349 | 20.2717      | 7.4377     |
| 333 | 110889  | 36926037 | 18.2483      | 6.9313     | 371 | 169826  | 69260938 | 20.2961      | 7.4440     |
| 334 | 111556  | 37259704 | 18.2757      | 6.9383     | 372 | 170654  | 69737107 | 20.3204      | 7.4503     |
| 335 | 112225  | 37596375 | 18.3030      | 6.9451     | 373 | 171484  | 70214856 | 20.3447      | 7.4566     |
| 336 | 112896  | 37935056 | 18.3303      | 6.9521     | 374 | 172316  | 70694185 | 20.3689      | 7.4629     |
| 337 | 113569  | 38275753 | 18.3576      | 6.9590     | 375 | 173150  | 71175094 | 20.3931      | 7.4692     |
| 338 | 114244  | 38618472 | 18.3848      | 6.9658     | 376 | 173986  | 71657683 | 20.4173      | 7.4755     |
| 339 | 114921  | 38963219 | 18.4120      | 6.9727     | 377 | 174824  | 72141952 | 20.4414      | 7.4818     |
| 340 | 115600  | 39310000 | 18.4391      | 6.9795     | 378 | 175664  | 72627901 | 20.4655      | 7.4881     |
| 341 | 116281  | 39658821 | 18.4662      | 6.9864     | 379 | 176506  | 73115530 | 20.4895      | 7.4944     |
| 342 | 116964  | 40010688 | 18.4932      | 6.9932     | 380 | 177350  | 73604849 | 20.5135      | 7.5007     |
| 343 | 117649  | 40364607 | 18.5203      | 7.         | 381 | 178196  | 74095858 | 20.5375      | 7.5070     |
| 344 | 118336  | 40720584 | 18.5472      | 7.0068     | 382 | 179044  | 74588467 | 20.5613      | 7.5133     |
| 345 | 119025  | 41078625 | 18.5742      | 7.0136     | 383 | 179894  | 75082676 | 20.5850      | 7.5196     |
| 346 | 119716  | 41438736 | 18.6011      | 7.0203     | 384 | 180746  | 75578485 | 20.6087      | 7.5259     |
| 347 | 120409  | 41791899 | 18.6279      | 7.0271     | 385 | 181600  | 76075894 | 20.6323      | 7.5322     |
| 348 | 121104  | 42147112 | 18.6548      | 7.0338     | 386 | 182456  | 76574903 | 20.6559      | 7.5385     |
| 349 | 121801  | 42504389 | 18.6815      | 7.0406     | 387 | 183314  | 77075512 | 20.6794      | 7.5448     |

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No. | Square. | Cube.     | Square root. | Cube root. | No. | Square. | Cube.     | Square root. | Cube root. |
|-----|---------|-----------|--------------|------------|-----|---------|-----------|--------------|------------|
| 429 | 184041  | 7863589   | 20.7123      | 7.5430     | 588 | 345744  | 202207472 | 24.2487      | 8.2777     |
| 430 | 184900  | 79607000  | 20.7364      | 7.5479     | 599 | 359081  | 131872220 | 22.5610      | 7.9843     |
| 431 | 185761  | 80602391  | 20.7605      | 7.5527     | 610 | 380100  | 132861000 | 22.5823      | 7.9896     |
| 432 | 186624  | 80623168  | 20.7846      | 7.5596     | 611 | 381121  | 133432831 | 22.6053      | 7.9948     |
| 433 | 187489  | 81189737  | 20.8087      | 7.5654     | 612 | 382144  | 134217728 | 22.6274      | 8.         |
| 434 | 188356  | 81746604  | 20.8327      | 7.5712     | 613 | 383169  | 135006697 | 22.6495      | 8.0062     |
| 435 | 189225  | 82312675  | 20.8567      | 7.5770     | 614 | 384196  | 135800744 | 22.6716      | 8.0104     |
| 436 | 190096  | 82888186  | 20.8806      | 7.5829     | 615 | 385225  | 136600875 | 22.6936      | 8.0156     |
| 437 | 190969  | 83463453  | 20.9045      | 7.5889     | 616 | 386256  | 137406096 | 22.7156      | 8.0208     |
| 438 | 191844  | 84037672  | 20.9284      | 7.5944     | 617 | 387289  | 138216413 | 22.7376      | 8.0260     |
| 439 | 192721  | 84610451  | 20.9523      | 7.6001     | 618 | 388324  | 139031832 | 22.7596      | 8.0311     |
| 440 | 193600  | 85184000  | 20.9762      | 7.6059     | 619 | 389361  | 139853359 | 22.7816      | 8.0363     |
| 441 | 194481  | 85766121  | 21.          | 7.6117     | 620 | 390400  | 140680000 | 22.8035      | 8.0415     |
| 442 | 195364  | 86350688  | 21.0238      | 7.6174     | 621 | 391441  | 141511761 | 22.8254      | 8.0466     |
| 443 | 196249  | 86938307  | 21.0476      | 7.6232     | 622 | 392484  | 142348648 | 22.8473      | 8.0517     |
| 444 | 197136  | 87528384  | 21.0713      | 7.6290     | 623 | 393529  | 143190667 | 22.8692      | 8.0569     |
| 445 | 198025  | 88121135  | 21.0950      | 7.6348     | 624 | 394576  | 144037824 | 22.8910      | 8.0620     |
| 446 | 198916  | 88716536  | 21.1187      | 7.6406     | 625 | 395625  | 144890125 | 22.9129      | 8.0671     |
| 447 | 199809  | 89314623  | 21.1424      | 7.6464     | 626 | 396676  | 145747576 | 22.9347      | 8.0723     |
| 448 | 200704  | 89915392  | 21.1660      | 7.6517     | 627 | 397729  | 146610183 | 22.9565      | 8.0774     |
| 449 | 201601  | 90518849  | 21.1896      | 7.6574     | 628 | 398784  | 147477952 | 22.9783      | 8.0825     |
| 450 | 202500  | 91125000  | 21.2132      | 7.6631     | 629 | 399841  | 148350889 | 23.          | 8.0876     |
| 451 | 203401  | 91733851  | 21.2368      | 7.6689     | 630 | 400900  | 149229000 | 23.0217      | 8.0927     |
| 452 | 204304  | 92345408  | 21.2603      | 7.6744     | 631 | 401961  | 149703281 | 23.0434      | 8.0978     |
| 453 | 205209  | 92959677  | 21.2838      | 7.6801     | 632 | 403024  | 150583768 | 23.0651      | 8.1028     |
| 454 | 206116  | 93576664  | 21.3073      | 7.6857     | 633 | 404089  | 151469437 | 23.0868      | 8.1079     |
| 455 | 207025  | 94196375  | 21.3307      | 7.6914     | 634 | 405156  | 152360304 | 23.1084      | 8.1130     |
| 456 | 207936  | 94818816  | 21.3542      | 7.6976     | 635 | 406225  | 153256405 | 23.1301      | 8.1180     |
| 457 | 208849  | 95443993  | 21.3776      | 7.7036     | 636 | 407296  | 154157856 | 23.1517      | 8.1231     |
| 458 | 209764  | 96071912  | 21.4009      | 7.7092     | 637 | 408369  | 155064653 | 23.1733      | 8.1281     |
| 459 | 210681  | 96702679  | 21.4243      | 7.7149     | 638 | 409444  | 155976896 | 23.1948      | 8.1332     |
| 460 | 211600  | 97336000  | 21.4476      | 7.7194     | 639 | 410521  | 156894589 | 23.2164      | 8.1382     |
| 461 | 212521  | 97972181  | 21.4709      | 7.7250     | 640 | 411600  | 157817640 | 23.2379      | 8.1433     |
| 462 | 213444  | 98611128  | 21.4942      | 7.7306     | 641 | 412681  | 158746041 | 23.2594      | 8.1483     |
| 463 | 214369  | 99252847  | 21.5174      | 7.7362     | 642 | 413764  | 159679808 | 23.2809      | 8.1533     |
| 464 | 215296  | 99897344  | 21.5407      | 7.7418     | 643 | 414849  | 160618967 | 23.3024      | 8.1583     |
| 465 | 216225  | 100544625 | 21.5639      | 7.7473     | 644 | 415936  | 161563536 | 23.3238      | 8.1633     |
| 466 | 217156  | 101194696 | 21.5870      | 7.7529     | 645 | 417025  | 162513553 | 23.3452      | 8.1683     |
| 467 | 218089  | 101847563 | 21.6102      | 7.7584     | 646 | 418116  | 163469024 | 23.3666      | 8.1733     |
| 468 | 219024  | 102503232 | 21.6333      | 7.7639     | 647 | 419209  | 164430005 | 23.3880      | 8.1783     |
| 469 | 219961  | 103161769 | 21.6564      | 7.7695     | 648 | 420304  | 165396592 | 23.4094      | 8.1833     |
| 470 | 220900  | 103823000 | 21.6795      | 7.7750     | 649 | 421401  | 166368803 | 23.4307      | 8.1882     |
| 471 | 221841  | 104487181 | 21.7025      | 7.7805     | 650 | 422500  | 167346608 | 23.4521      | 8.1932     |
| 472 | 222784  | 105154408 | 21.7256      | 7.7860     | 651 | 423601  | 168330005 | 23.4734      | 8.1982     |
| 473 | 223729  | 105823917 | 21.7486      | 7.7915     | 652 | 424704  | 169319008 | 23.4947      | 8.2031     |
| 474 | 224676  | 106496424 | 21.7715      | 7.7970     | 653 | 425809  | 170313627 | 23.5160      | 8.2081     |
| 475 | 225625  | 107171875 | 21.7945      | 7.8025     | 654 | 426916  | 171313856 | 23.5372      | 8.2130     |
| 476 | 226576  | 107850176 | 21.8174      | 7.8079     | 655 | 428025  | 172319695 | 23.5584      | 8.2180     |
| 477 | 227529  | 108531333 | 21.8403      | 7.8134     | 656 | 429136  | 173331152 | 23.5797      | 8.2229     |
| 478 | 228484  | 109215352 | 21.8632      | 7.8188     | 657 | 430249  | 174348323 | 23.6008      | 8.2278     |
| 479 | 229441  | 109902259 | 21.8861      | 7.8243     | 658 | 431364  | 175371616 | 23.6220      | 8.2327     |
| 480 | 230400  | 110592000 | 21.9089      | 7.8297     | 659 | 432481  | 176401129 | 23.6432      | 8.2377     |
| 481 | 231361  | 111284641 | 21.9317      | 7.8352     | 660 | 433600  | 177436864 | 23.6643      | 8.2426     |
| 482 | 232324  | 111980168 | 21.9545      | 7.8406     | 661 | 434721  | 178478823 | 23.6854      | 8.2475     |
| 483 | 233289  | 112678587 | 21.9773      | 7.8460     | 662 | 435844  | 179526992 | 23.7065      | 8.2524     |
| 484 | 234256  | 113379904 | 22.          | 7.8514     | 663 | 436969  | 180581367 | 23.7276      | 8.2573     |
| 485 | 235225  | 114084125 | 22.0227      | 7.8568     | 664 | 438096  | 181641952 | 23.7487      | 8.2621     |
| 486 | 236196  | 114791256 | 22.0454      | 7.8622     | 665 | 439225  | 182708763 | 23.7697      | 8.2670     |
| 487 | 237169  | 115501303 | 22.0681      | 7.8676     | 666 | 440356  | 183781808 | 23.7908      | 8.2719     |
| 488 | 238144  | 116214272 | 22.0907      | 7.8730     | 667 | 441489  | 184861083 | 23.8118      | 8.2768     |
| 489 | 239121  | 116930169 | 22.1133      | 7.8784     | 668 | 442624  | 185946592 | 23.8328      | 8.2816     |
| 490 | 240100  | 117648000 | 22.1359      | 7.8837     | 669 | 443761  | 187038337 | 23.8537      | 8.2865     |
| 491 | 241081  | 118367771 | 22.1585      | 7.8891     | 670 | 444900  | 188136304 | 23.8747      | 8.2913     |
| 492 | 242064  | 119089488 | 22.1811      | 7.8944     | 671 | 446041  | 189240513 | 23.8956      | 8.2962     |
| 493 | 243049  | 119823157 | 22.2036      | 7.8998     | 672 | 447184  | 190351872 | 23.9165      | 8.3010     |
| 494 | 244036  | 120568784 | 22.2261      | 7.9051     | 673 | 448329  | 191469387 | 23.9374      | 8.3059     |
| 495 | 245025  | 121326353 | 22.2486      | 7.9105     | 674 | 449476  | 192593056 | 23.9583      | 8.3107     |
| 496 | 246016  | 122086896 | 22.2711      | 7.9158     | 675 | 450625  | 193722883 | 23.9792      | 8.3155     |
| 497 | 247009  | 122849423 | 22.2935      | 7.9211     | 676 | 451776  | 194858976 | 24.          | 8.3203     |
| 498 | 248004  | 123613952 | 22.3159      | 7.9264     | 677 | 452929  | 195991329 | 24.0208      | 8.3251     |
| 499 | 249001  | 124381499 | 22.3383      | 7.9317     | 678 | 454084  | 197130052 | 24.0416      | 8.3300     |
| 500 | 250000  | 125152000 | 22.3607      | 7.9370     | 679 | 455241  | 198275073 | 24.0624      | 8.3348     |
| 501 | 251001  | 125925501 | 22.3830      | 7.9423     | 680 | 456400  | 199426400 | 24.0832      | 8.3396     |
| 502 | 252004  | 126702004 | 22.4054      | 7.9476     | 681 | 457561  | 200584037 | 24.1039      | 8.3443     |
| 503 | 253009  | 127481527 | 22.4277      | 7.9529     | 682 | 458724  | 201747888 | 24.1247      | 8.3491     |
| 504 | 254016  | 128264064 | 22.4499      | 7.9581     | 683 | 459889  | 202918049 | 24.1454      | 8.3539     |
| 505 | 255025  | 129049625 | 22.4722      | 7.9634     | 684 | 461056  | 204094520 | 24.1661      | 8.3587     |
| 506 | 256036  | 129838208 | 22.4944      | 7.9686     | 685 | 462225  | 205277303 | 24.1868      | 8.3634     |
| 507 | 257049  | 130629843 | 22.5167      | 7.9739     | 686 | 463396  | 206466400 | 24.2074      | 8.3682     |
| 508 | 258064  | 131423512 | 22.5389      | 7.9791     | 687 | 464569  | 207661803 | 24.2281      | 8.3730     |

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No.  | Square. | Cube.     | Square root. | Cube root. | No.  | Square. | Cube.     | Square root. | Cube root. |
|------|---------|-----------|--------------|------------|------|---------|-----------|--------------|------------|
| 589. | 346921  | 204388469 | 24.2693      | 8.3825     | 688. | 466224  | 288977632 | 25.8457      | 8.7416     |
| 590. | 348100  | 205629000 | 24.2899      | 8.3972     | 689. | 467761  | 290412539 | 25.8650      | 8.7469     |
| 591. | 349281  | 206883071 | 24.3105      | 8.4019     | 690. | 469300  | 291869000 | 25.8844      | 8.7503     |
| 592. | 350464  | 208149888 | 24.3311      | 8.4067     | 691. | 470841  | 293338041 | 25.9037      | 8.7547     |
| 593. | 351649  | 209429057 | 24.3516      | 8.4114     | 692. | 472384  | 294819328 | 25.9230      | 8.7590     |
| 594. | 352836  | 210720684 | 24.3721      | 8.4161     | 693. | 473929  | 296312847 | 25.9422      | 8.7634     |
| 595. | 354025  | 212024675 | 24.3926      | 8.4208     | 694. | 475476  | 297818672 | 25.9615      | 8.7677     |
| 596. | 355216  | 213341128 | 24.4131      | 8.4255     | 695. | 477025  | 299336825 | 25.9808      | 8.7721     |
| 597. | 356409  | 214670047 | 24.4336      | 8.4302     | 696. | 478576  | 300867316 | 25.9999      | 8.7764     |
| 598. | 357604  | 216011428 | 24.4540      | 8.4349     | 697. | 480129  | 302410283 | 26.0192      | 8.7807     |
| 599. | 358801  | 217365275 | 24.4745      | 8.4396     | 698. | 481684  | 303964832 | 26.0384      | 8.7850     |
| 600. | 360000  | 218731600 | 24.4949      | 8.4443     | 699. | 483241  | 305531000 | 26.0576      | 8.7893     |
| 601. | 361201  | 219618104 | 24.5153      | 8.4490     | 700. | 484800  | 307109000 | 26.0768      | 8.7937     |
| 602. | 362404  | 220514808 | 24.5357      | 8.4537     |      | 486361  | 308708801 | 26.0960      | 8.7980     |
| 603. | 363609  | 221421727 | 24.5561      | 8.4584     |      | 487924  | 310320824 | 26.1151      | 8.8023     |
| 604. | 364816  | 222338864 | 24.5764      | 8.4630     |      | 489489  | 311945067 | 26.1343      | 8.8066     |
| 605. | 366025  | 223266227 | 24.5967      | 8.4677     |      | 491056  | 313581520 | 26.1534      | 8.8109     |
| 606. | 367236  | 224203916 | 24.6171      | 8.4723     |      | 492625  | 315230283 | 26.1725      | 8.8152     |
| 607. | 368449  | 225151935 | 24.6374      | 8.4769     |      | 494196  | 316891360 | 26.1916      | 8.8194     |
| 608. | 369664  | 226110388 | 24.6577      | 8.4816     |      | 495769  | 318564767 | 26.2107      | 8.8237     |
| 609. | 370881  | 227079279 | 24.6779      | 8.4863     |      | 497344  | 320250512 | 26.2298      | 8.8280     |
| 610. | 372100  | 228058600 | 24.6982      | 8.4909     |      | 498921  | 321948609 | 26.2488      | 8.8323     |
| 611. | 373321  | 229048451 | 24.7184      | 8.4956     |      | 500500  | 323659070 | 26.2679      | 8.8366     |
| 612. | 374544  | 230048832 | 24.7386      | 8.4992     |      | 502081  | 325381987 | 26.2869      | 8.8409     |
| 613. | 375769  | 231059747 | 24.7588      | 8.5038     |      | 503664  | 327117360 | 26.3059      | 8.8451     |
| 614. | 376996  | 232081200 | 24.7790      | 8.5084     |      | 505249  | 328865201 | 26.3249      | 8.8493     |
| 615. | 378225  | 233113285 | 24.7992      | 8.5130     |      | 506836  | 330625532 | 26.3439      | 8.8536     |
| 616. | 379456  | 234155996 | 24.8193      | 8.5176     |      | 508425  | 332398367 | 26.3629      | 8.8578     |
| 617. | 380689  | 235209327 | 24.8395      | 8.5222     |      | 510016  | 334183720 | 26.3818      | 8.8621     |
| 618. | 381924  | 236273284 | 24.8596      | 8.5268     |      | 511609  | 335981607 | 26.4008      | 8.8663     |
| 619. | 383161  | 237347861 | 24.8797      | 8.5314     |      | 513204  | 337792032 | 26.4197      | 8.8706     |
| 620. | 384400  | 238433060 | 24.8998      | 8.5360     |      | 514801  | 339615009 | 26.4386      | 8.8748     |
| 621. | 385641  | 239528885 | 24.9199      | 8.5406     |      | 516400  | 341450560 | 26.4575      | 8.8790     |
| 622. | 386884  | 240635332 | 24.9399      | 8.5452     |      | 518001  | 343308689 | 26.4764      | 8.8833     |
| 623. | 388129  | 241752407 | 24.9600      | 8.5498     |      | 519604  | 345179400 | 26.4953      | 8.8875     |
| 624. | 389376  | 242880116 | 24.9800      | 8.5544     |      | 521209  | 347062707 | 26.5141      | 8.8917     |
| 625. | 390625  | 244018465 | 25.          | 8.5590     |      | 522816  | 348958624 | 26.5330      | 8.8959     |
| 626. | 391876  | 245167450 | 25.0200      | 8.5634     |      | 524425  | 350867167 | 26.5518      | 8.9001     |
| 627. | 393129  | 246327075 | 25.0400      | 8.5680     |      | 526036  | 352788344 | 26.5707      | 8.9043     |
| 628. | 394384  | 247497336 | 25.0599      | 8.5726     |      | 527649  | 354722081 | 26.5895      | 8.9085     |
| 629. | 395641  | 248678239 | 25.0799      | 8.5772     |      | 529264  | 356668400 | 26.6083      | 8.9127     |
| 630. | 396900  | 249869790 | 25.0998      | 8.5818     |      | 530881  | 358627327 | 26.6271      | 8.9169     |
| 631. | 398161  | 251072007 | 25.1197      | 8.5863     |      | 532500  | 360598860 | 26.6458      | 8.9211     |
| 632. | 399424  | 252285888 | 25.1396      | 8.5909     |      | 534121  | 362583009 | 26.6646      | 8.9253     |
| 633. | 400689  | 253500431 | 25.1595      | 8.5954     |      | 535744  | 364579776 | 26.6833      | 8.9295     |
| 634. | 401956  | 254726640 | 25.1794      | 8.5999     |      | 537369  | 366589167 | 26.7021      | 8.9337     |
| 635. | 403225  | 255964519 | 25.1992      | 8.6045     |      | 538996  | 368611200 | 26.7208      | 8.9379     |
| 636. | 404496  | 257214064 | 25.2190      | 8.6090     |      | 540625  | 370645987 | 26.7395      | 8.9420     |
| 637. | 405769  | 258475287 | 25.2389      | 8.6136     |      | 542256  | 372693432 | 26.7582      | 8.9462     |
| 638. | 407044  | 259748196 | 25.2587      | 8.6182     |      | 543889  | 374753547 | 26.7769      | 8.9504     |
| 639. | 408321  | 261032799 | 25.2784      | 8.6228     |      | 545524  | 376826320 | 26.7956      | 8.9546     |
| 640. | 409600  | 262329096 | 25.2982      | 8.6273     |      | 547161  | 378911767 | 26.8143      | 8.9588     |
| 641. | 410881  | 263636095 | 25.3180      | 8.6319     |      | 548800  | 381009880 | 26.8329      | 8.9630     |
| 642. | 412164  | 264954792 | 25.3377      | 8.6365     |      | 550441  | 383130671 | 26.8514      | 8.9672     |
| 643. | 413449  | 266285189 | 25.3574      | 8.6411     |      | 552084  | 385264144 | 26.8701      | 8.9714     |
| 644. | 414736  | 267627292 | 25.3772      | 8.6457     |      | 553729  | 387410307 | 26.8887      | 8.9756     |
| 645. | 416025  | 268981107 | 25.3969      | 8.6503     |      | 555376  | 389569160 | 26.9072      | 8.9798     |
| 646. | 417316  | 270346632 | 25.4166      | 8.6549     |      | 557025  | 391740707 | 26.9258      | 8.9840     |
| 647. | 418609  | 271723873 | 25.4362      | 8.6595     |      | 558676  | 393924944 | 26.9444      | 8.9882     |
| 648. | 419904  | 273112836 | 25.4558      | 8.6641     |      | 560329  | 396121887 | 26.9629      | 8.9924     |
| 649. | 421201  | 274513527 | 25.4755      | 8.6687     |      | 561984  | 398331536 | 26.9815      | 8.9966     |
| 650. | 422500  | 275925952 | 25.4951      | 8.6733     |      | 563641  | 400553907 | 26.9999      | 9.0008     |
| 651. | 423801  | 277349167 | 25.5147      | 8.6779     |      | 565300  | 402788920 | 27.0185      | 9.0050     |
| 652. | 425104  | 278784168 | 25.5343      | 8.6825     |      | 566961  | 405036587 | 27.0370      | 9.0092     |
| 653. | 426409  | 280230961 | 25.5539      | 8.6871     |      | 568624  | 407296912 | 27.0555      | 9.0134     |
| 654. | 427716  | 281689492 | 25.5734      | 8.6917     |      | 570289  | 409569907 | 27.0740      | 9.0176     |
| 655. | 429025  | 283159767 | 25.5930      | 8.6963     |      | 571956  | 411855568 | 27.0924      | 9.0218     |
| 656. | 430336  | 284641792 | 25.6125      | 8.7009     |      | 573625  | 414153897 | 27.1109      | 9.0260     |
| 657. | 431649  | 286135583 | 25.6320      | 8.7055     |      | 575296  | 416464016 | 27.1293      | 9.0302     |
| 658. | 432964  | 287641136 | 25.6515      | 8.7101     |      | 576969  | 418786927 | 27.1477      | 9.0344     |
| 659. | 434281  | 289158457 | 25.6710      | 8.7147     |      | 578644  | 421122640 | 27.1662      | 9.0386     |
| 660. | 435600  | 290687552 | 25.6905      | 8.7193     |      | 580321  | 423471167 | 27.1846      | 9.0428     |
| 661. | 436921  | 292228427 | 25.7099      | 8.7239     |      | 582000  | 425832512 | 27.2029      | 9.0470     |
| 662. | 438244  | 293781176 | 25.7294      | 8.7285     |      | 583681  | 428206787 | 27.2213      | 9.0512     |
| 663. | 439569  | 295345807 | 25.7488      | 8.7331     |      | 585364  | 430593992 | 27.2397      | 9.0554     |
| 664. | 440896  | 296922328 | 25.7683      | 8.7377     |      | 587049  | 433004127 | 27.2580      | 9.0596     |
| 665. | 442225  | 298510747 | 25.7878      | 8.7423     |      | 588736  | 435428192 | 27.2764      | 9.0638     |
| 666. | 443556  | 299610064 | 25.8070      | 8.7469     |      | 590425  | 437865287 | 27.2947      | 9.0680     |
| 667. | 444889  | 300721287 | 25.8263      | 8.7515     |      | 592116  | 440315424 | 27.3130      | 9.0722     |

TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No. | Square. | Cube.      | Square root. | Cube root. | No. | Square. | Cube.      | Square root. | Cube root. |
|-----|---------|------------|--------------|------------|-----|---------|------------|--------------|------------|
| 747 | 558009  | 418832723  | 27.3913      | 9.0735     | 826 | 682276  | 565559976  | 28.7402      | 9.3537     |
| 748 | 559504  | 418508992  | 27.3496      | 9.0775     | 827 | 683829  | 566609238  | 28.7576      | 9.3565     |
| 749 | 561001  | 420189749  | 27.3679      | 9.0816     | 828 | 685384  | 567663552  | 28.7750      | 9.3602     |
| 750 | 562500  | 421875000  | 27.3861      | 9.0856     | 829 | 687241  | 569732789  | 28.7924      | 9.3640     |
| 751 | 564001  | 423564751  | 27.4044      | 9.0896     | 830 | 689000  | 571787000  | 28.8097      | 9.3678     |
| 752 | 565504  | 425259008  | 27.4226      | 9.0937     | 831 | 690651  | 573866191  | 28.8271      | 9.4016     |
| 753 | 567009  | 426957777  | 27.4408      | 9.0977     | 832 | 692224  | 575988368  | 28.8444      | 9.4053     |
| 754 | 568516  | 428661064  | 27.4591      | 9.1017     | 833 | 693899  | 578099637  | 28.8617      | 9.4091     |
| 755 | 570025  | 430368875  | 27.4773      | 9.1057     | 834 | 695556  | 5800963704 | 28.8791      | 9.4129     |
| 756 | 571536  | 432081216  | 27.4956      | 9.1098     | 835 | 697225  | 582182875  | 28.8964      | 9.4166     |
| 757 | 573049  | 433798093  | 27.5136      | 9.1138     | 836 | 698896  | 584277056  | 28.9137      | 9.4204     |
| 758 | 574564  | 435519612  | 27.5318      | 9.1178     | 837 | 700569  | 586376253  | 28.9310      | 9.4241     |
| 759 | 576081  | 437245479  | 27.5500      | 9.1218     | 838 | 702244  | 588486472  | 28.9482      | 9.4279     |
| 760 | 577600  | 438976000  | 27.5681      | 9.1258     | 839 | 703921  | 590589719  | 28.9655      | 9.4316     |
| 761 | 579121  | 440711081  | 27.5862      | 9.1298     | 840 | 705600  | 592704000  | 28.9828      | 9.4354     |
| 762 | 580644  | 442450728  | 27.6043      | 9.1338     | 841 | 707281  | 594833321  | 29.          | 9.4391     |
| 763 | 582169  | 444194947  | 27.6225      | 9.1378     | 842 | 708964  | 596967688  | 29.0172      | 9.4429     |
| 764 | 583696  | 445943744  | 27.6406      | 9.1418     | 843 | 710649  | 599097107  | 29.0346      | 9.4466     |
| 765 | 585225  | 447697125  | 27.6586      | 9.1458     | 844 | 712336  | 601211584  | 29.0517      | 9.4503     |
| 766 | 586756  | 449455096  | 27.6767      | 9.1498     | 845 | 714025  | 603351125  | 29.0689      | 9.4541     |
| 767 | 588289  | 451217603  | 27.6948      | 9.1537     | 846 | 715716  | 605495736  | 29.0861      | 9.4578     |
| 768 | 589824  | 452984832  | 27.7128      | 9.1577     | 847 | 717409  | 607645423  | 29.1033      | 9.4615     |
| 769 | 591361  | 454756609  | 27.7308      | 9.1617     | 848 | 719104  | 609800192  | 29.1204      | 9.4652     |
| 770 | 592900  | 456533000  | 27.7489      | 9.1657     | 849 | 720801  | 611960049  | 29.1376      | 9.4690     |
| 771 | 594441  | 458314011  | 27.7669      | 9.1696     | 850 | 722500  | 614125000  | 29.1548      | 9.4727     |
| 772 | 595984  | 460099648  | 27.7849      | 9.1736     | 851 | 724201  | 616295051  | 29.1719      | 9.4764     |
| 773 | 597529  | 461889917  | 27.8029      | 9.1775     | 852 | 725904  | 618470208  | 29.1890      | 9.4801     |
| 774 | 599076  | 463684824  | 27.8209      | 9.1815     | 853 | 727609  | 620650477  | 29.2062      | 9.4838     |
| 775 | 600625  | 465484375  | 27.8388      | 9.1855     | 854 | 729316  | 622835864  | 29.2233      | 9.4875     |
| 776 | 602176  | 467288576  | 27.8568      | 9.1894     | 855 | 731025  | 625026375  | 29.2404      | 9.4912     |
| 777 | 603729  | 469097433  | 27.8747      | 9.1933     | 856 | 732736  | 627222016  | 29.2575      | 9.4949     |
| 778 | 605284  | 470910652  | 27.8927      | 9.1973     | 857 | 734449  | 629422793  | 29.2746      | 9.4986     |
| 779 | 606841  | 472729139  | 27.9106      | 9.2012     | 858 | 736164  | 631628712  | 29.2916      | 9.5023     |
| 780 | 608400  | 474552000  | 27.9286      | 9.2052     | 859 | 737881  | 633839779  | 29.3087      | 9.5060     |
| 781 | 609961  | 476379541  | 27.9464      | 9.2091     | 860 | 739600  | 636056000  | 29.3258      | 9.5097     |
| 782 | 611524  | 478211768  | 27.9643      | 9.2130     | 861 | 741321  | 638277381  | 29.3428      | 9.5134     |
| 783 | 613089  | 480048687  | 27.9821      | 9.2170     | 862 | 743044  | 640503928  | 29.3598      | 9.5171     |
| 784 | 614656  | 481890304  | 28.          | 9.2209     | 863 | 744769  | 642735647  | 29.3769      | 9.5207     |
| 785 | 616225  | 483736625  | 28.0179      | 9.2248     | 864 | 746496  | 644972544  | 29.3939      | 9.5244     |
| 786 | 617796  | 485587656  | 28.0357      | 9.2287     | 865 | 748225  | 647214625  | 29.4109      | 9.5281     |
| 787 | 619369  | 487444403  | 28.0536      | 9.2326     | 866 | 749956  | 649461896  | 29.4279      | 9.5317     |
| 788 | 620944  | 489306872  | 28.0713      | 9.2365     | 867 | 751689  | 651714363  | 29.4449      | 9.5354     |
| 789 | 622521  | 491169009  | 28.0891      | 9.2404     | 868 | 753424  | 653972032  | 29.4618      | 9.5391     |
| 790 | 624100  | 493033900  | 28.1069      | 9.2443     | 869 | 755161  | 656234909  | 29.4788      | 9.5427     |
| 791 | 625681  | 494913671  | 28.1247      | 9.2482     | 870 | 756900  | 658503000  | 29.4958      | 9.5464     |
| 792 | 627264  | 496799088  | 28.1425      | 9.2521     | 871 | 758641  | 660776311  | 29.5127      | 9.5501     |
| 793 | 628849  | 498677257  | 28.1603      | 9.2560     | 872 | 760384  | 663054848  | 29.5296      | 9.5537     |
| 794 | 630436  | 500566184  | 28.1780      | 9.2599     | 873 | 762129  | 665338617  | 29.5466      | 9.5574     |
| 795 | 632025  | 502455985  | 28.1957      | 9.2638     | 874 | 763876  | 667627624  | 29.5635      | 9.5610     |
| 796 | 633616  | 504356336  | 28.2135      | 9.2677     | 875 | 765625  | 669921875  | 29.5804      | 9.5647     |
| 797 | 635209  | 5062661573 | 28.2312      | 9.2716     | 876 | 767376  | 672221376  | 29.5973      | 9.5683     |
| 798 | 636804  | 508186562  | 28.2489      | 9.2754     | 877 | 769129  | 674526133  | 29.6142      | 9.5719     |
| 799 | 638401  | 5101082399 | 28.2666      | 9.2793     | 878 | 770884  | 676836152  | 29.6311      | 9.5756     |
| 800 | 640000  | 512000000  | 28.2843      | 9.2832     | 879 | 772641  | 679151439  | 29.6479      | 9.5792     |
| 801 | 641601  | 513922401  | 28.3019      | 9.2870     | 880 | 774400  | 681472000  | 29.6648      | 9.5828     |
| 802 | 643204  | 515849608  | 28.3196      | 9.2909     | 881 | 776161  | 683797841  | 29.6816      | 9.5865     |
| 803 | 644809  | 517781627  | 28.3373      | 9.2948     | 882 | 777924  | 686128968  | 29.6985      | 9.5901     |
| 804 | 646416  | 519718464  | 28.3549      | 9.2986     | 883 | 779689  | 688465387  | 29.7153      | 9.5937     |
| 805 | 648025  | 521660125  | 28.3725      | 9.3025     | 884 | 781456  | 690807014  | 29.7321      | 9.5973     |
| 806 | 649636  | 523606616  | 28.3901      | 9.3063     | 885 | 783225  | 693154125  | 29.7489      | 9.6010     |
| 807 | 651249  | 525557943  | 28.4077      | 9.3102     | 886 | 784996  | 695506456  | 29.7658      | 9.6046     |
| 808 | 652864  | 527514112  | 28.4253      | 9.3140     | 887 | 786769  | 697864108  | 29.7825      | 9.6082     |
| 809 | 654481  | 529475129  | 28.4429      | 9.3179     | 888 | 788544  | 700227072  | 29.7993      | 9.6118     |
| 810 | 656100  | 531441000  | 28.4605      | 9.3217     | 889 | 790321  | 702596369  | 29.8161      | 9.6154     |
| 811 | 657721  | 533411731  | 28.4781      | 9.3255     | 890 | 792100  | 704969000  | 29.8329      | 9.6190     |
| 812 | 659344  | 535387328  | 28.4956      | 9.3294     | 891 | 793881  | 707347971  | 29.8496      | 9.6226     |
| 813 | 660969  | 537367797  | 28.5132      | 9.3332     | 892 | 795664  | 709732288  | 29.8664      | 9.6262     |
| 814 | 662596  | 539353144  | 28.5307      | 9.3370     | 893 | 797449  | 712121957  | 29.8831      | 9.6298     |
| 815 | 664225  | 541343375  | 28.5482      | 9.3408     | 894 | 799236  | 714516984  | 29.8999      | 9.6334     |
| 816 | 665846  | 543338496  | 28.5657      | 9.3447     | 895 | 801025  | 716917375  | 29.9166      | 9.6370     |
| 817 | 667489  | 545338513  | 28.5832      | 9.3485     | 896 | 802816  | 719323136  | 29.9333      | 9.6406     |
| 818 | 669134  | 547343432  | 28.6007      | 9.3523     | 897 | 804609  | 721734273  | 29.9500      | 9.6442     |
| 819 | 670781  | 549353259  | 28.6182      | 9.3561     | 898 | 806404  | 724150792  | 29.9666      | 9.6477     |
| 820 | 672440  | 551368900  | 28.6356      | 9.3599     | 899 | 808201  | 726572699  | 29.9833      | 9.6513     |
| 821 | 674041  | 553387661  | 28.6531      | 9.3637     | 900 | 810000  | 729000000  | 30.          | 9.6549     |
| 822 | 675684  | 555412248  | 28.6705      | 9.3675     | 901 | 811801  | 731432701  | 30.0167      | 9.6585     |
| 823 | 677329  | 557441767  | 28.6880      | 9.3713     | 902 | 813604  | 733870808  | 30.0333      | 9.6620     |
| 824 | 678976  | 559476224  | 28.7054      | 9.3751     | 903 | 815409  | 736314327  | 30.0500      | 9.6656     |
| 825 | 680625  | 561515625  | 28.7228      | 9.3789     | 904 | 817216  | 738763264  | 30.0666      | 9.6692     |



TABLE VI.—Table of squares, cubes, square roots, and cube roots of numbers from 1 to 1,000—Continued.

| No. | Square. | Cube.     | Square root. | Cube root. | No.  | Square. | Cube.      | Square root. | Cube root. |
|-----|---------|-----------|--------------|------------|------|---------|------------|--------------|------------|
| 905 | 819025  | 741217625 | 20.0832      | 9.6727     | 953  | 908209  | 965523177  | 30.3707      | 9.8498     |
| 906 | 820836  | 748877416 | 20.0998      | 9.6763     | 954  | 910116  | 968250664  | 30.3899      | 9.8442     |
| 907 | 822649  | 746142643 | 20.1164      | 9.6799     | 955  | 912028  | 970983876  | 30.3931      | 9.8477     |
| 908 | 824464  | 748613312 | 20.1330      | 9.6834     | 956  | 913936  | 973722616  | 30.3972      | 9.8511     |
| 909 | 826281  | 751989429 | 20.1496      | 9.6870     | 957  | 915849  | 976467493  | 30.3984      | 9.8546     |
| 910 | 828100  | 755371000 | 20.1662      | 9.6905     | 958  | 917764  | 9792217912 | 30.3916      | 9.8580     |
| 911 | 829921  | 758758031 | 20.1828      | 9.6941     | 959  | 919681  | 981974079  | 30.3977      | 9.8614     |
| 912 | 831744  | 762150328 | 20.1993      | 9.6976     | 960  | 921600  | 984736000  | 30.3989      | 9.8648     |
| 913 | 833569  | 761049497 | 20.2159      | 9.7012     | 961  | 923521  | 987506681  | 31.          | 9.8682     |
| 914 | 835396  | 763551944 | 20.2324      | 9.7047     | 962  | 925444  | 990277128  | 31.0161      | 9.8717     |
| 915 | 837225  | 766060675 | 20.2490      | 9.7082     | 963  | 927369  | 993048947  | 31.0222      | 9.8761     |
| 916 | 839056  | 768575296 | 20.2655      | 9.7118     | 964  | 929296  | 995841844  | 31.0453      | 9.8785     |
| 917 | 840889  | 771085213 | 20.2820      | 9.7153     | 965  | 931225  | 998622125  | 31.0644      | 9.8819     |
| 918 | 842724  | 773600332 | 20.2985      | 9.7188     | 966  | 933156  | 1001428696 | 31.0835      | 9.8854     |
| 919 | 844561  | 776111559 | 20.3150      | 9.7224     | 967  | 935089  | 1004231063 | 31.0986      | 9.8888     |
| 920 | 846400  | 778628000 | 20.3315      | 9.7259     | 968  | 937024  | 1007039232 | 31.1127      | 9.8922     |
| 921 | 848241  | 781129961 | 20.3480      | 9.7294     | 969  | 938961  | 1009853209 | 31.1288      | 9.8956     |
| 922 | 850084  | 783777448 | 20.3645      | 9.7329     | 970  | 940900  | 1012673000 | 31.1448      | 9.8990     |
| 923 | 851929  | 786330467 | 20.3809      | 9.7364     | 971  | 942841  | 1015498611 | 31.1609      | 9.9024     |
| 924 | 853776  | 788889024 | 20.3974      | 9.7400     | 972  | 944784  | 1018330048 | 31.1769      | 9.9058     |
| 925 | 855625  | 791453125 | 20.4138      | 9.7435     | 973  | 946729  | 1021167317 | 31.1929      | 9.9092     |
| 926 | 857476  | 794022776 | 20.4302      | 9.7470     | 974  | 948676  | 1024010424 | 31.2090      | 9.9126     |
| 927 | 859329  | 796597983 | 20.4467      | 9.7505     | 975  | 950625  | 1026859375 | 31.2250      | 9.9160     |
| 928 | 861184  | 799178732 | 20.4631      | 9.7540     | 976  | 952576  | 1029714176 | 31.2410      | 9.9194     |
| 929 | 863041  | 801765089 | 20.4795      | 9.7575     | 977  | 954529  | 1032574833 | 31.2570      | 9.9227     |
| 930 | 864900  | 804357000 | 20.4959      | 9.7610     | 978  | 956484  | 1035441352 | 31.2730      | 9.9261     |
| 931 | 866761  | 806954461 | 20.5123      | 9.7645     | 979  | 958441  | 1038313739 | 31.2890      | 9.9295     |
| 932 | 868624  | 809557468 | 20.5287      | 9.7680     | 980  | 960400  | 1041192000 | 31.3050      | 9.9329     |
| 933 | 870489  | 812166037 | 20.5450      | 9.7715     | 981  | 962361  | 1044076141 | 31.3209      | 9.9362     |
| 934 | 872356  | 814780304 | 20.5614      | 9.7750     | 982  | 964324  | 1046966168 | 31.3369      | 9.9396     |
| 935 | 874225  | 817400275 | 20.5778      | 9.7785     | 983  | 966289  | 1049862207 | 31.3528      | 9.9430     |
| 936 | 876096  | 820025946 | 20.5941      | 9.7820     | 984  | 968256  | 1052763304 | 31.3688      | 9.9464     |
| 937 | 877969  | 822658313 | 20.6105      | 9.7854     | 985  | 970225  | 1055670325 | 31.3847      | 9.9497     |
| 938 | 879844  | 825298372 | 20.6268      | 9.7889     | 986  | 972196  | 1058583256 | 31.4006      | 9.9531     |
| 939 | 881721  | 827936019 | 20.6431      | 9.7924     | 987  | 974169  | 1061502003 | 31.4166      | 9.9565     |
| 940 | 883600  | 830584000 | 20.6594      | 9.7959     | 988  | 976144  | 1064426272 | 31.4325      | 9.9598     |
| 941 | 885481  | 833237621 | 20.6757      | 9.7993     | 989  | 978121  | 1067356069 | 31.4484      | 9.9632     |
| 942 | 887364  | 835896888 | 20.6920      | 9.8028     | 990  | 980100  | 1070291200 | 31.4643      | 9.9666     |
| 943 | 889249  | 838561807 | 20.7083      | 9.8063     | 991  | 982081  | 1073232271 | 31.4802      | 9.9699     |
| 944 | 891136  | 841232384 | 20.7246      | 9.8097     | 992  | 984064  | 1076179198 | 31.4960      | 9.9733     |
| 945 | 893025  | 843908625 | 20.7409      | 9.8132     | 993  | 986049  | 1079131957 | 31.5119      | 9.9766     |
| 946 | 894916  | 846590536 | 20.7571      | 9.8167     | 994  | 988036  | 1082090784 | 31.5278      | 9.9800     |
| 947 | 896809  | 849278123 | 20.7734      | 9.8201     | 995  | 990025  | 1085055487 | 31.5436      | 9.9833     |
| 948 | 898704  | 851971392 | 20.7896      | 9.8236     | 996  | 992016  | 1088026736 | 31.5595      | 9.9866     |
| 949 | 900601  | 854670349 | 20.8058      | 9.8270     | 997  | 994009  | 1091003975 | 31.5753      | 9.9900     |
| 950 | 902500  | 857375000 | 20.8221      | 9.8305     | 998  | 996004  | 1094000000 | 31.5911      | 9.9933     |
| 951 | 904401  | 860085351 | 20.8383      | 9.8339     | 999  | 998001  | 1097002999 | 31.6070      | 9.9967     |
| 952 | 906304  | 862801408 | 20.8545      | 9.8374     | 1000 | 1000000 | 1000000000 | 31.6228      | 10.        |

213. To find the square root of a decimal fraction or mixed number from the foregoing table, multiply by 100 or by 10,000 and find the product in the column of squares. The corresponding number in the first column, with the decimal point one or two places to the left is the desired root.

For the cube root of a similar number, multiply by 1,000 or by 1,000,000, and find the nearest number in column of cubes. The corresponding number in the first column, with the decimal point one or two places to the left, is the desired root.

**Examples:** Required the square root of 5.246.

Multiply by 100; the result is 524, which found in column of squares is opposite 23 in the column of numbers. Moving the decimal point one place to the left to correspond with the multiplication by 100, gives 2.3 for the desired square root, to the first place of decimals and hence approximate only. Second: Multiply by 10,000; the result is 52,460, which found in the column of squares is opposite

229 in the column of numbers. Moving the decimal point two places to the left to correspond to the multiplication by 10,000, the result is 2.29, which is the desired root to the second place of decimals.

Required the cube root of 5.246. Multiply by 1,000, giving 5,246, which found in the column of cubes is opposite the number 17 in the first column. Moving the decimal point one place to the left to correspond to the multiplication by 1,000 gives 1.7, which is the required cube root to one decimal place. Again, multiplying by 1,000,000 gives 5,246,000, which found in the column of cubes is opposite the number 174 in the column of numbers. Moving the decimal point two places to the left to correspond with the multiplication by 1,000,000, gives the number 1.74, which is the desired cube root correct to two places of decimals.

To find the square root or cube root of a number greater than 1,000, find the nearest number in the column of squares or cubes and take the corresponding number in the first column, which will be correct for the number of figures it contains.

For the fourth root, take the square root of the square root. For the sixth root, the square root of the cube root, or the cube root of the square root. Higher roots, the indices of which can be factored in 3's and 2's, may be taken in the same way.

#### CIRCULAR FUNCTIONS.

214. Those most used are shown graphically in fig. 68. They bear a definite relation to the radius of a circle in which they are drawn. When the radius is unity, functions are called *natural*, as natural sine, natural tangent, etc. Their values are given in Table XVI for each 10' of arc. The tabulated values are ratios of the several functions to the radius and if any length, expressed in any unit, considered as a radius, be multiplied by a tabular number, the result will be the corresponding function of the circle of the given radius. The table gives values from 0 to 90°. For greater angles, use the following relations: Subtract the given angle from 180° or 360°, or subtract 180° from the angle, as may be required, to leave a remainder of 90° or less. Take out the required function of the remainder, which is also that of the given angle.

Interpolation for values not in the table may be done approximately by taking the proportional amount of the difference between two consecutive values. Thus, for the sine of 28° 43' take the sine of 28° 40' plus  $\frac{3}{10}$  of the difference between sine 28° 40' and sine 28° 50'.

TABLE VII.—*Natural sines and tangents to a radius 1.*

| Arc. | Sine.   | Tang.   | Cotang.  | Cosine.  | Arc.  |
|------|---------|---------|----------|----------|-------|
| 0 00 | .000000 | .000000 | Infinite | 1.000000 | 99 00 |
| 10   | .002068 | .002068 | 343.7737 | .999958  | 50    |
| 20   | .006817 | .006817 | 171.8384 | .999832  | 40    |
| 30   | .012655 | .008793 | 114.5888 | .999619  | 30    |
| 40   | .018533 | .014636 | 85.9379  | .999328  | 20    |
| 50   | .024439 | .020508 | 68.7809  | .998962  | 10    |
| 1 00 | .030368 | .026455 | 57.2896  | .998527  | 90    |
| 10   | .036308 | .032365 | 49.1038  | .997927  | 80    |
| 20   | .042260 | .038275 | 42.9640  | .997162  | 70    |
| 30   | .048219 | .044185 | 38.1884  | .996237  | 60    |
| 40   | .054184 | .050097 | 34.3877  | .995170  | 50    |
| 50   | .060152 | .056008 | 31.2467  | .993971  | 40    |
| 2 00 | .066123 | .061920 | 28.6425  | .992646  | 30    |
| 10   | .072095 | .067833 | 26.4316  | .991195  | 20    |
| 20   | .078068 | .073746 | 24.5475  | .989628  | 10    |
| 30   | .084041 | .079659 | 22.9037  | .987943  | 90    |
| 40   | .090013 | .085575 | 21.4704  | .986141  | 80    |
| 50   | .095984 | .091491 | 20.2055  | .984222  | 70    |
| 3 00 | .052360 | .052407 | 19.0813  | .982195  | 60    |
| 10   | .058346 | .058393 | 18.0749  | .979971  | 50    |
| 20   | .064332 | .064379 | 17.1893  | .977559  | 40    |
| 30   | .070318 | .070365 | 16.4185  | .974962  | 30    |
| 40   | .076304 | .076351 | 15.7580  | .972195  | 20    |
| 50   | .082290 | .082337 | 15.1941  | .969262  | 10    |
| 4 00 | .069756 | .069803 | 14.3006  | .966177  | 90    |
| 10   | .075742 | .075789 | 13.7267  | .962946  | 80    |
| 20   | .081728 | .081775 | 13.1968  | .959574  | 70    |
| 30   | .087714 | .087761 | 12.7060  | .956066  | 60    |
| 40   | .093700 | .093747 | 12.2505  | .952428  | 50    |
| 50   | .099686 | .099733 | 11.8261  | .948666  | 40    |
| 5 00 | .087157 | .087204 | 11.4305  | .944787  | 30    |
| 10   | .093143 | .093190 | 11.0693  | .940797  | 20    |
| 20   | .099129 | .099176 | 10.7419  | .936694  | 10    |
| 30   | .105115 | .105162 | 10.4483  | .932483  | 90    |
| 40   | .111101 | .111148 | 10.1893  | .928169  | 80    |
| 50   | .117087 | .117134 | 9.9643   | .923756  | 70    |
| 6 00 | .104528 | .104575 | 9.5436   | .919249  | 60    |
| 10   | .110514 | .110561 | 9.2353   | .914654  | 50    |
| 20   | .116500 | .116547 | 8.9303   | .909974  | 40    |
| 30   | .122486 | .122533 | 8.6387   | .905204  | 30    |
| 40   | .128472 | .128519 | 8.3555   | .900349  | 20    |
| 50   | .134458 | .134505 | 8.0805   | .895404  | 10    |
| 7 00 | .121893 | .121940 | 8.1443   | .892542  | 90    |
| 10   | .127879 | .127926 | 7.8830   | .888584  | 80    |
| 20   | .133865 | .133912 | 7.6350   | .884534  | 70    |
| 30   | .139851 | .139898 | 7.3995   | .880397  | 60    |
| 40   | .145837 | .145884 | 7.1760   | .876177  | 50    |
| 50   | .151823 | .151870 | 6.9640   | .871877  | 40    |
|      |         |         |          |          |       |
|      | Cosine. | Cotang. | Tang.    | Sine.    | Arc.  |

TABLE VII.—*Natural sines and tangents*—Continued.

| Arc.  | Sine.    | Tang.   | Cotang.  | Cosine.  |       |
|-------|----------|---------|----------|----------|-------|
| 8 00  | .1391731 | .140540 | 7.115369 | .9902681 | 82 00 |
| 10    | .1420531 | .143508 | 6.963333 | .9898590 | 50    |
| 20    | .1449379 | .146478 | 6.826943 | .9894416 | 40    |
| 30    | .1478264 | .149451 | 6.691156 | .9890159 | 30    |
| 40    | .1507235 | .152426 | 6.556053 | .9885817 | 20    |
| 50    | .1536307 | .155404 | 6.432842 | .9881392 | 10    |
| 9 00  | .1565435 | .158384 | 6.313751 | .9876883 | 81 00 |
| 10    | .1593669 | .161367 | 6.197027 | .9872294 | 50    |
| 20    | .1621779 | .164353 | 6.084438 | .9867615 | 40    |
| 30    | .1650476 | .167342 | 5.975764 | .9862856 | 30    |
| 40    | .1679159 | .170334 | 5.870904 | .9858013 | 20    |
| 50    | .1707828 | .173329 | 5.769368 | .9853097 | 10    |
| 10 00 | .1736482 | .176327 | 5.671281 | .9848078 | 80 00 |
| 10    | .1765121 | .179327 | 5.576378 | .9842985 | 50    |
| 20    | .1793746 | .182331 | 5.484505 | .9837808 | 40    |
| 30    | .1822355 | .185339 | 5.395517 | .9832549 | 30    |
| 40    | .1850949 | .188349 | 5.309279 | .9827206 | 20    |
| 50    | .1879528 | .191363 | 5.225664 | .9821781 | 10    |
| 11 00 | .1908090 | .194380 | 5.144554 | .9816272 | 79 00 |
| 10    | .1936636 | .197400 | 5.065835 | .9810680 | 50    |
| 20    | .1965166 | .200424 | 4.989402 | .9805005 | 40    |
| 30    | .1993679 | .203452 | 4.915157 | .9799247 | 30    |
| 40    | .2022176 | .206483 | 4.843004 | .9793406 | 20    |
| 50    | .2050655 | .209518 | 4.772856 | .9787483 | 10    |
| 12 00 | .2079117 | .212536 | 4.704630 | .9781476 | 78 00 |
| 10    | .2107561 | .215598 | 4.638245 | .9775386 | 50    |
| 20    | .2135988 | .218644 | 4.573828 | .9769215 | 40    |
| 30    | .2164396 | .221694 | 4.510708 | .9762960 | 30    |
| 40    | .2192786 | .224748 | 4.449418 | .9756623 | 20    |
| 50    | .2221158 | .227806 | 4.389694 | .9750203 | 10    |
| 13 00 | .2249511 | .230868 | 4.331375 | .9743701 | 77 00 |
| 10    | .2277844 | .233934 | 4.274706 | .9737116 | 50    |
| 20    | .2306159 | .237004 | 4.219331 | .9730449 | 40    |
| 30    | .2334454 | .240078 | 4.165209 | .9723699 | 30    |
| 40    | .2362729 | .243157 | 4.112361 | .9716867 | 20    |
| 50    | .2390984 | .246240 | 4.061070 | .9709953 | 10    |
| 14 00 | .2419219 | .249328 | 4.010780 | .9702957 | 76 00 |
| 10    | .2447433 | .252420 | 3.961651 | .9695879 | 50    |
| 20    | .2475627 | .255516 | 3.913642 | .9688719 | 40    |
| 30    | .2503800 | .258617 | 3.866713 | .9681476 | 30    |
| 40    | .2531952 | .261723 | 3.820828 | .9674152 | 20    |
| 50    | .2560082 | .264833 | 3.775961 | .9666746 | 10    |
| 15 00 | .2588190 | .267949 | 3.732050 | .9659258 | 75 00 |
| 10    | .2616277 | .271069 | 3.688092 | .9651689 | 50    |
| 20    | .2644342 | .274194 | 3.647046 | .9644037 | 40    |
| 30    | .2672384 | .277324 | 3.608983 | .9636306 | 30    |
| 40    | .2700403 | .280459 | 3.563574 | .9628490 | 20    |
| 50    | .2728400 | .283599 | 3.520603 | .9620594 | 10    |
|       | Cosine.  | Cotang. | Tang.    | Sine.    | Arc.  |

TABLE VII.—*Natural sines and tangents—Continued.*

| Arc.  | Sine.    | Tang.    | Cotang.   | Cosine.  |       |
|-------|----------|----------|-----------|----------|-------|
| 32 00 | .5299433 | .634399  | 1.609334  | .8490481 | 58 00 |
| 10    | .5317539 | .636981  | 1.599123  | .8469630 | 50    |
| 20    | .5343440 | .639968  | 1.579807  | .8449608 | 40    |
| 30    | .5377946 | .6437070 | 1.559385  | .8430314 | 30    |
| 40    | .5420507 | .6481167 | 1.538955  | .8411849 | 20    |
| 50    | .5471971 | .6532979 | 1.5186715 | .8403613 | 10    |
| 33 00 | .5440890 | .649407  | 1.530965  | .8386708 | 57 00 |
| 10    | .5470793 | .653561  | 1.530102  | .8370837 | 50    |
| 20    | .5495030 | .657710  | 1.529426  | .8354978 | 40    |
| 30    | .5519670 | .661885  | 1.519835  | .8339158 | 30    |
| 40    | .5544603 | .666076  | 1.561328  | .8323378 | 20    |
| 50    | .5569730 | .670284  | 1.491903  | .8307607 | 10    |
| 34 00 | .5594929 | .674508  | 1.482561  | .8291876 | 56 00 |
| 10    | .5611021 | .678749  | 1.473298  | .8276174 | 50    |
| 20    | .5640896 | .683006  | 1.464114  | .8260503 | 40    |
| 30    | .5664632 | .687281  | 1.455009  | .8244862 | 30    |
| 40    | .5689611 | .691572  | 1.445980  | .8229251 | 20    |
| 50    | .5713912 | .695881  | 1.437026  | .8223670 | 10    |
| 35 00 | .5738576 | .700207  | 1.428148  | .8198120 | 55 00 |
| 10    | .5763638 | .704551  | 1.419342  | .8172481 | 50    |
| 20    | .5788623 | .708913  | 1.410609  | .8146861 | 40    |
| 30    | .5807680 | .713283  | 1.401948  | .8121155 | 30    |
| 40    | .5830687 | .717681  | 1.393357  | .8124229 | 20    |
| 50    | .5864294 | .722107  | 1.384835  | .8107234 | 10    |
| 36 00 | .5877853 | .726542  | 1.376381  | .8091170 | 54 00 |
| 10    | .5903361 | .730996  | 1.367995  | .8075038 | 50    |
| 20    | .5929819 | .735469  | 1.359676  | .8058837 | 40    |
| 30    | .5948228 | .739961  | 1.351422  | .8042569 | 30    |
| 40    | .5971586 | .744472  | 1.343233  | .8026232 | 20    |
| 50    | .5994893 | .749003  | 1.335107  | .8009827 | 10    |
| 37 00 | .6019150 | .753554  | 1.327044  | .7993355 | 53 00 |
| 10    | .6041356 | .758124  | 1.319044  | .7976815 | 50    |
| 20    | .6064511 | .762715  | 1.311104  | .7960208 | 40    |
| 30    | .6087614 | .767327  | 1.303226  | .7943533 | 30    |
| 40    | .6110666 | .771968  | 1.295405  | .7926792 | 20    |
| 50    | .6133666 | .776611  | 1.287644  | .7909983 | 10    |
| 38 00 | .6156615 | .781285  | 1.279941  | .7893108 | 52 00 |
| 10    | .6179611 | .785980  | 1.272295  | .7876165 | 50    |
| 20    | .6202555 | .790697  | 1.264706  | .7844157 | 40    |
| 30    | .6225446 | .795435  | 1.257172  | .7830062 | 30    |
| 40    | .6247885 | .800196  | 1.249693  | .7807940 | 20    |
| 50    | .6270671 | .804979  | 1.242268  | .7785733 | 10    |
| 39 00 | .6293304 | .809784  | 1.234897  | .7771460 | 51 00 |
| 10    | .6315784 | .814611  | 1.227578  | .7753121 | 50    |
| 20    | .6338510 | .819462  | 1.220312  | .7734716 | 40    |
| 30    | .6360973 | .824336  | 1.213097  | .7716246 | 30    |
| 40    | .6383201 | .829233  | 1.205932  | .7697710 | 20    |
| 50    | .6405506 | .834154  | 1.198818  | .7679110 | 10    |
|       | Cosine.  | Cotang.  | Tang.     | Sine.    | Arc.  |

## TABLE VII.—Natural sines and tangents.—Continued.

| Arc.  | Sine.    | Tang.    | Cotang.  | Cosine.  |       |
|-------|----------|----------|----------|----------|-------|
| 40 00 | .6427876 | .839099  | 1.191753 | .7660444 | 50 00 |
| 10    | .6450132 | .844068  | 1.184737 | .7641714 | 50    |
| 20    | .6472334 | .849062  | 1.177799 | .7622919 | 40    |
| 30    | .6494490 | .854080  | 1.170943 | .7604060 | 30    |
| 40    | .6516672 | .859124  | 1.163976 | .7585136 | 20    |
| 50    | .6538809 | .864192  | 1.157149 | .7566148 | 10    |
| 41 00 | .6560900 | .869286  | 1.150368 | .7547096 | 49 00 |
| 10    | .6582916 | .874406  | 1.143632 | .7527980 | 50    |
| 20    | .6604886 | .879552  | 1.136941 | .7508800 | 40    |
| 30    | .6626820 | .884725  | 1.130294 | .7489557 | 30    |
| 40    | .6648723 | .889924  | 1.123693 | .7470261 | 20    |
| 50    | .6669661 | .895150  | 1.117130 | .7450881 | 10    |
| 42 00 | .6691306 | .900404  | 1.110612 | .7431448 | 48 00 |
| 10    | .6712896 | .905685  | 1.104156 | .7411953 | 50    |
| 20    | .6734427 | .910994  | 1.097702 | .7392394 | 40    |
| 30    | .6755904 | .916331  | 1.091308 | .7372773 | 30    |
| 40    | .6777329 | .921696  | 1.084966 | .7353090 | 20    |
| 50    | .6798681 | .927091  | 1.078642 | .7333345 | 10    |
| 43 00 | .6819984 | .932515  | 1.072368 | .7313537 | 47 00 |
| 10    | .6841229 | .937968  | 1.066134 | .7293668 | 50    |
| 20    | .6862416 | .943451  | 1.059938 | .7273736 | 40    |
| 30    | .6883546 | .948944  | 1.053780 | .7253744 | 30    |
| 40    | .6904617 | .954458  | 1.047659 | .7233690 | 20    |
| 50    | .6925630 | .960002  | 1.041576 | .7213574 | 10    |
| 44 00 | .6946584 | .965668  | 1.035530 | .7193398 | 46 00 |
| 10    | .6967479 | .971326  | 1.029520 | .7173161 | 50    |
| 20    | .6988315 | .976995  | 1.023546 | .7152863 | 40    |
| 30    | .7009003 | .982697  | 1.017607 | .7132504 | 30    |
| 40    | .7029631 | .988431  | 1.011703 | .7112086 | 20    |
| 50    | .7050209 | .994199  | 1.005834 | .7091607 | 10    |
| 45 00 | .7070688 | 1.000000 | 1.000000 | .7071068 | 45 00 |
|       | Cosine.  | Cotang.  | Tang.    | Sine.    | Arc.  |

## PROPERTIES OF CIRCLES.

215. The ratio of the diameter to the circumference is represented in mathematics by  $\pi$ , called Pi. Its value can not be exactly expressed. To 5 decimal places it is 3.14159, which equals  $\frac{22}{7}$  nearly. Log.  $\pi$  equals 0.4971499.

Diam.  $\times 3.14159$  = circ.

Diam.  $\times 0.886277$  = side of square of equal area.

Diam.  $\times 0.7071$  = side of inscribed square.

$\frac{1}{2} \pi D^2 = 0.7854 \times D^2$  = area of the circle.

$\pi r^2 = 3.1416 \times r^2$  = area of the circle.

The length of an arc of  $n^\circ = r \times 0.017453$ .

Example: If the radius is 542 feet, the length of an arc of  $18^\circ 20' = 18^\circ.33 \times 542 \times 0.017453 = 165.5$  feet.

## PROPERTIES OF SOME PLANE FIGURES.

216. Triangles are classed as equilateral when the three sides are of equal length; isosceles, when two sides only are equal; acute-angled, when each of its angles is less than  $90^\circ$ ; obtuse-angled, when one angle is greater than  $90^\circ$ .

The sum of the angles of any triangle is  $180^\circ$ . The sides are directly proportional to the sines of the opposite angles, the greatest and least sides opposite the greatest and least angles.

Formulas for the solution of plane triangles. (Fig. 69.)

Given two sides, as  $a$  and  $b$ , and an angle opposite to one of them, as  $B$ .

$$\sin. A = \frac{a \sin. B}{b}; C = 180^\circ - (A + B); c = \frac{a \sin. C}{\sin. A}.$$

Given 2 angles, as  $A$  and  $B$ , and the included side  $c$ , the most common case.

$$C = 180^\circ - (A + B); a = \frac{c \sin. A}{\sin. C}; b = \frac{c \sin. B}{\sin. A}.$$

Given 2 sides as  $a$  and  $b$ , and the included angle  $C$ .

$$180^\circ - C = A + B$$

$$\tan. \frac{A - B}{2} = \frac{(a - b) \frac{(A + B)}{2}}{a + b}$$

$$A = \frac{A + B}{2} + \frac{A - B}{2}; B = \frac{A + B}{2} - \frac{A - B}{2}; C = \frac{a \sin. C}{\sin. A}.$$

Given the 3 sides—

$$\frac{a + b + c}{2} = S; \sin. \frac{A}{2} = \sqrt{\frac{(S - b)(S - c)}{bc}};$$

$$\sin. \frac{B}{2} = \sqrt{\frac{(S - a)(S - c)}{ac}}; \sin. \frac{C}{2} = \sqrt{\frac{(S - a)(S - b)}{ab}}.$$

For every right-angled triangle the sine of the right angle is 1, and the following relations result: The side opposite the right angle is called the hypotenuse. (Fig. 69.)

$$\text{Hypotenuse} = a = c \div \sin. C = c \times \sec. B = \frac{b}{\cos. C}$$

$$= b \times \sec. C = \sqrt{b^2 + c^2};$$

$$b = a \times \sin. B = a \times \cos. C = c \times \cotang. C = c \times \tang. B;$$

$$c = a \times \sin. C = a \times \cos. B = b \times \tang. C;$$

$$\sin. B = \frac{b}{a} \cos. C; \sin. C = \frac{c}{a} \cos. B;$$

$$\tang. B = \frac{b}{c} = \cotang. C; \tang. C = \frac{c}{b} = \cotang. B.$$

The area of a triangle equals any side multiplied by  $\frac{1}{2}$  the perpendicular distance from that side to the opposite angle. If the perpendicular from the angle does not intersect the opposite side, prolong the side, but do not include the prolongation in its length for computing the area. All triangles which have a common side and their opposite angles in a straight line parallel to the common side are equal in area.

A line bisecting one angle divides the opposite side into parts proportional to the adjacent sides. In fig. 70,  $ab$  bisects the angle at  $a$  and  $bc:ac::bd:ad$ .

Lines drawn from each angle to the middle of the opposite side intersect in a common point, which is the center of gravity of the triangle. The shorter part of each line is  $\frac{1}{2}$  the longer (fig. 71).

A line joining the middle points of two sides is parallel to the third side and  $\frac{1}{2}$  its length. In fig. 71 the line  $ef$ , joining the middle points of  $ab$  and  $bc$ , is parallel to  $ac$ , and  $\frac{1}{2}$  its length. Lines joining  $eg$  and  $fg$  would be parallel to  $ab$  and  $bc$ , and half their length, respectively.

Similar triangles are those which have the same angles and differ only in length of sides. The ratio between corresponding sides of all similar triangles is the same, since it is the ratio of the same function of the same angles. Hence, if two sides of a triangle and one of the corresponding sides of a similar triangle are known, the other corresponding side may be determined. The simplest test of similar triangles is that their corresponding sides are parallel or perpendicular. The principle of similar triangles is of great utility in field geometry.

The side of a square equals the diameter of an inscribed circle; or the diameter of a circumscribed circle  $\times 0.7071$ . The diagonal of a square equals one side  $\times 1.4142$ .

The area of a trapezoid, fig. 72, equals  $\frac{1}{2}$  the sum of the parallel sides  $ab$  and  $cd$  multiplied by the distance between them,  $ef$ .

The area of a trapezium—no two sides parallel—figure 73, equals  $\frac{1}{2}$  the diagonal  $ac$  multiplied by the sum of the perpendiculars,  $bf$  and  $de$ .

The side of a hexagon equals the radius of a circumscribed circle. The area equals the square of 1 side  $\times 2.598$ . The side of an octagon equals the radius of a circumscribed circle  $\times 0.7633$ . The area equals the square of one side  $\times 4.8289$ .

To draw an octagon in a square (fig. 74).—From each corner, with a radius equal to  $\frac{1}{2}$  the diagonal, describe arcs as shown. Join the point at which they cut the sides. If a square stick be scribed at a distance from each corner equal to 0.3, the side of the square and the corners chamfered to the marks, the resulting section will be nearly a true octagon.

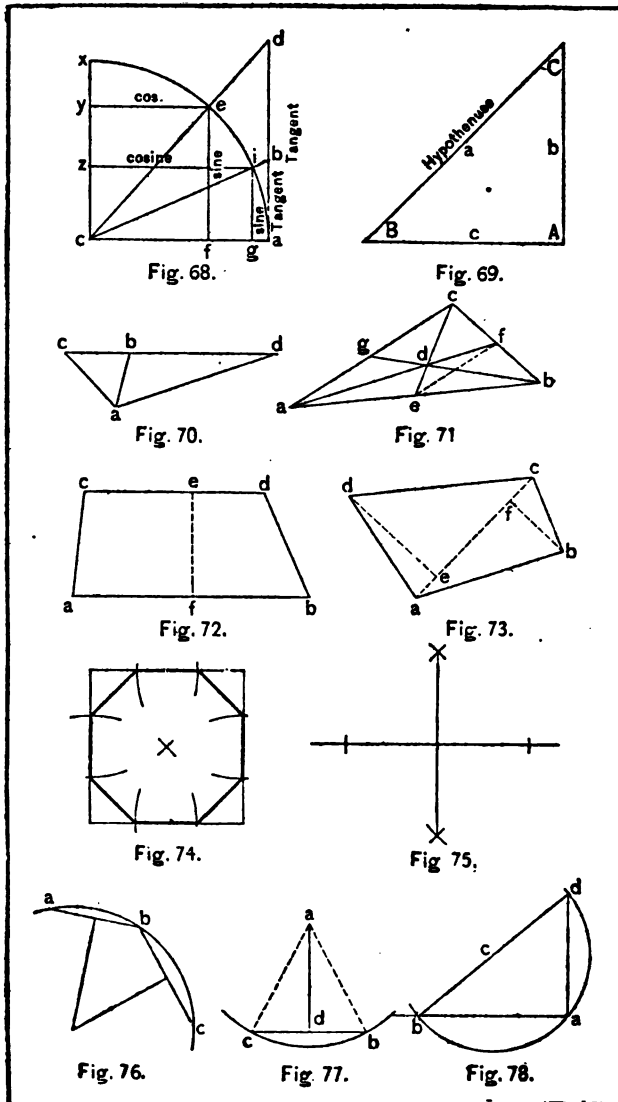
#### GEOMETRICAL CONSTRUCTIONS.

217. To divide a straight line into any number of equal parts: From one end of the line draw another, making any convenient angle with it, as  $10^\circ$  or  $20^\circ$ . On this auxiliary line lay off any assumed distance as many times as the number of equal parts desired. Join the last point so determined with the end of the first line. Through each of the points marked on the auxiliary line draw a line parallel to the line joining the ends. These lines will divide the given line into the desired number of equal parts.

To draw a perpendicular from a given point on a line: Mark 2 points equidistant from the given point, fig. 75, and with them as centers and a radius greater than their distance from the given point describe arcs on each side of the line. Connect one intersection with the given point by a straight line, which is the perpendicular required. As a check on accuracy, note whether the line passes through the other intersection.



If the given point is at one end of the line, from a convenient point *c* outside the line describe a semicircle passing through the given point and cutting the line again as at *b*, fig. 78. Draw a straight line *bc* through the center to the arc on the other side, as at *d*. The line *da* is the perpendicular required.



From a given point to let fall a perpendicular to a given line: From the given point, fig. 77, describe an arc cutting the line twice. With these two points proceed as in erecting a perpendicular at a given point, fig. 75, or bisect the portion of the line between the intersections, as at *d*, and draw the line *ad*, which is the perpendicular required.

To describe a circle passing through 3 given points: Join the points by 2 lines, as  $ab$  and  $bc$ , fig. 76, and construct a bisecting perpendicular on each. The perpendiculars intersect at the center of the required circle.

218. Areas are to each other as the squares of similar lines; similar triangles as the squares of corresponding sides, or of perpendiculars from corresponding angles to opposite sides, etc.

Squares are to each other as the squares of the sides or diagonals.

Other regular polygons are to each other as the squares of the sides or of the radii of inscribed or circumscribed circles.

Circles are to each other as the squares of diameters, or radii, or chords of equal arcs.

#### SPHERES AND CUBES.

219. The surface of a sphere  $= 4 \pi r^2 = 12.5664 r^2 = 3.1416 d^2 = 0.3183$  circ. squared  $= 4 \times$  area of a great circle  $=$  diam.  $\times$  circ.  $=$  the curved surface of circumscribed cylinder.

The surfaces of two spheres are to each other as the squares of corresponding lines.

The volume of a sphere  $= \frac{4}{3} \pi r^3 = 4.1888 r^3 = 0.5236 d^3 = 0.01689$  circ.<sup>3</sup>  $= \frac{2}{3}$  diam.  $\times$  area of great circle  $= \frac{2}{3}$  vol. of circumscribed cylinder  $= 0.5326$  vol. of circumscribed cube.

The volumes of spheres and cubes are to each other as the cubes of their corresponding lines, or the squares of corresponding surfaces; for a sphere, the radius, the diameter, the area of a great circle, or of any circle subtending equal angles at the center; for a cube, an edge, a diagonal of a side, or a diagonal of the cube. The diagonal of a cube  $=$  the edge  $\times 1.7321$ .

#### GRAVITATION.

220. The earth's attraction is measured by the increase in the velocity of a falling body which that attraction produces in a second of time. This quantity is represented by  $g$ , and its value at the surface of the earth on the equator is 32.092 feet. This means that if any body is falling freely its velocity at the end of any second of time is 32.092 feet per second greater than at the beginning of that second. If the body starts from rest, its velocity at the beginning is 0, and at the end of the first second is  $g$ . The velocity of any falling body at any instant equals  $g$  multiplied by the number of seconds the body has been falling. This relation is strictly true for a vacuum only, but for moderate heights is nearly correct in air.

The value of  $g$  varies slightly with the latitude as shown in the following table:

TABLE XVII.

221. Values of  $g$  at surface of earth in different latitudes:

| Latitude.    | Value of $g$<br>in feet. | Latitude.     | Value of $g$<br>in feet. |
|--------------|--------------------------|---------------|--------------------------|
| Equator..... | 32.09                    | 52° 15'.....  | 32.19                    |
| 20° 40'..... | 32.11                    | 60°.....      | 32.21                    |
| 30°.....     | 32.13                    | 69° 15'.....  | 32.23                    |
| 37° 10'..... | 32.15                    | 90° pole..... | 32.25                    |
| 45°.....     | 32.17                    |               |                          |

222. The value of  $g$  varies also with the distance from the center of the earth; or the distance above or below the surface, diminishing in both cases. This diminution is approximately 0.016 foot for each mile above the surface and 0.008 foot for each mile below.

223. The fundamental law of motion of falling bodies is  $v^2 = 2gh$ , in which  $v$  = the velocity at any point in feet per second;  $h$ , the distance through which the body has fallen from rest to the given instant.

As  $v = gt$ ,  $h = \frac{1}{2}gt^2 = 16t^2$ . These relations are strictly true only in vacuo, but for small, smooth, dense objects are approximately correct for motion in air up to 5 seconds.

#### CENTRIFUGAL FORCE.

224. If  $w$  = the weight of a revolving body and  $n$  the number of revolutions per minute,  $r$  = the radius of revolution or the distance of center of gravity of the body from center of motion, and  $c$  = the centrifugal force or pull on the radius in pounds, then  $c = 0.00034wn^2$

#### Equivalents of measure.

##### LENGTHS.

1 meter, m = 10 decimeters, dm = 100 centimeters, cm = 1000 millimeters, mm.  
1 meter, m = 0.1 decameter, dkm = 0.01 hectometer, hm = 0.001 kilometer, km.  
1 meter, m = 39.37 inches, U. S. Standard = 39.370113 inches, British standard.  
1 millimeter, mm = 1000 microns,  $\mu$  = 0.03937 inch = 39.37 mils.

| Meters,<br>m. | Inches,<br>in. | Feet,<br>ft. | Yard,<br>yd. | Rods,<br>r. | Chains,<br>ch. | Miles, U. S. |            | Kilo-<br>meters,<br>km. |
|---------------|----------------|--------------|--------------|-------------|----------------|--------------|------------|-------------------------|
|               |                |              |              |             |                | Statute.     | Nautical.  |                         |
| 1             | 39.37          | 3.28083      | 1.09361      | 0.19884     | 0.04971        | 0.0006214    | 0.00053996 | 0.001                   |
| 0.02540       | 1              | 0.08333      | 0.02778      | 0.05051     | 0.01263        | 0.001578     | 0.001371   | 0.02540                 |
| 0.00440       | 12             | 1            | 0.33333      | 0.06061     | 0.01515        | 0.01894      | 0.01645    | 0.03048                 |
| 0.01440       | 36             | 3            | 1            | 0.18182     | 0.04545        | 0.05682      | 0.04934    | 0.09144                 |
| 0.02921       | 198            | 16.5         | 5.5          | 1           | 0.25           | 0.03125      | 0.02714    | 0.05029                 |
| 0.1188        | 792            | 66           | 22           | 4           | 1              | 0.01250      | 0.01085    | 0.02012                 |
| 0.6350        | 6330           | 5280         | 1760         | 320         | 80             | 1            | 0.86839    | 1.60935                 |
| 0.00025       | 72962.5        | 6080.20      | 2026.73      | 308.497     | 92.1243        | 1.15155      | 1          | 1.60935                 |
| 0.0001        | 39370          | 3280.83      | 1093.61      | 198.838     | 49.7096        | 0.62137      | 0.53959    | 1                       |

1 yard, U. S. = 1.0000029 yards British. 1 yard British = 0.9999971 yard U. S.  
1 chain, Gunter's = 100 links. 1 link = 7.92 inches.  
1 cable length, U. S. = 120 fathoms = 960 spans = 720 feet = 219.457 meters.  
1 league, U. S. = 3 statute miles = 24 furlongs.  
1 international geographical mile =  $\frac{1}{60}$  at equator = 7422 m = 4.611808 U. S. statute miles.  
1 international nautical mile =  $\frac{1}{60}$  at meridian = 1852 m = 0.999826 U. S. nautical miles.  
1 U. S. nautical mile =  $\frac{1}{60}$  of circumference of sphere whose surface equals that of the earth = 6080.27 feet = 1.85328 statute miles = 1553.27 meters.  
1 British nautical mile = 6080.00 feet = 1.15152 statute miles = 1853.19 meters.

##### SURFACES AND AREAS.

1 sq. meter, m<sup>2</sup> = 100 sq. decimeters, dm<sup>2</sup> = 10000 sq. centimeters, cm<sup>2</sup>.  
1 sq. meter, m<sup>2</sup> = 0.01 are, a = 0.0001 hectare, ha.  
1 sq. millimeter, mm<sup>2</sup> = 0.01 cm<sup>2</sup> = 0.00155 sq. inch = 1217.36 circ. mils.  
1 are, a = 1 sq. decameter, dkm = 0.0247104 acre.

| Square<br>meters,<br>m <sup>2</sup> . | Square<br>inches,<br>sq. in. | Square<br>feet,<br>sq. ft. | Square<br>yards,<br>sq. yd. | Square<br>rods,<br>sq. r. | Acres,<br>A.  | Hectares,<br>ha. | Square<br>miles,<br>statute. | Square<br>kilo-<br>meters,<br>km <sup>2</sup> . |
|---------------------------------------|------------------------------|----------------------------|-----------------------------|---------------------------|---------------|------------------|------------------------------|---|
| 1                                     | 1550.00                      | 10.7639                    | 1.19599                     | 0.03954                   | 0.002471      | 0.00001          | 0.0003861                    | 0.001   |
| 0.00452                               | 1                            | 0.000644                   | 0.0007716                   | 0.0002551                 | 0.0000002471  | 0.0000000001     | 0.0000000003861              | 0.0000000001                                    |
| 0.0002920                             | 144                          | 1                          | 0.11111                     | 0.03673                   | 0.000002920   | 0.0000000002920  | 0.0000000003597              | 0.0000000002920                                 |
| 0.000018                              | 1296                         | 9                          | 1                           | 0.03306                   | 0.00000000018 | 0.00000000000018 | 0.0000000000003328           | 0.000000000000018                               |
| 25.0000                               | 39204                        | 272.25                     | 30.25                       | 1                         | 0.00625       | 0.00000000025    | 0.0000000000009766           | 0.00000000000025                                |
| 4046.87                               | 6272640                      | 43560                      | 4840                        | 160                       | 1             | 0.00404687       | 0.0000000000001563           | 0.0000000000004047                              |
| 10000                                 | 15499969                     | 107639                     | 11859.9                     | 395.366                   | 2.47104       | 1                | 0.003861                     | 0.01  |
| 25.0000                               | 39204                        | 272.25                     | 30.25                       | 1                         | 0.00625       | 0.00000000025    | 0.0000000000009766           | 0.00000000000025                                |
| 1000000                               | 1549996900                   | 10763900                   | 11859900                    | 39536.6                   | 247.104       | 100              | 0.038610                     | 1   |

1 sq. rod, sq. perch, or sq. perch = 625 sq. links =  $\frac{1}{16}$  acre.  
1 sq. chain, Gunter's = 16 sq. rods =  $\frac{1}{4}$  acre.  
1 acre = 4 sq. rods = 160 sq. rods. Square of 1 acre = 208.7103 feet square.  
Notations  $\frac{1}{2}$ ,  $\frac{1}{4}$ , etc., indicate that the  $\frac{1}{2}$ ,  $\frac{1}{4}$ , etc., are to be replaced by 2, 3, 4, etc., ciphers.  
Example: 1 sq. rod = 0.0000009766 sq. miles.

*Equivalents of measure.*

## VOLUME AND CAPACITY.

1 cu. meter,  $m^3$ —1,000 cu. decimeter,  $dm^3$ —1,000,000 cu. centimeters,  $cm^3$ .  
 1 liter, l—10 deciliters, dl—100 centiliters, cl—1,000 milliliters, ml—1,000 cu. centimeters,  $cm^3$ , or cc.  
 1 liter, l—0.1 decaliter, dkl—0.01 hectoliter, hl—1 cu. decimeter,  $dm^3$ .

| Cubic<br>decimeter,<br>$dm^3$ , l. | Cubic<br>inches,<br>cu. in. | Cubic<br>feet,<br>cu. ft. | Cubic<br>yards,<br>cu. yd. | U. S. quarts.     |                | U. S. gallons.     |                 | U. S.<br>bushels,<br>bu. |
|------------------------------------|-----------------------------|---------------------------|----------------------------|-------------------|----------------|--------------------|-----------------|--------------------------|
|                                    |                             |                           |                            | Liquid,<br>l. qt. | Dry,<br>d. qt. | Liquid,<br>l. gal. | Dry,<br>d. gal. |                          |
| 1                                  | 61.0234                     | 0.03531                   | 0.1306                     | 1.05668           | 0.90808        | 0.26417            | 0.22702         | 0.02838                  |
| 0.01639                            | 1                           | 0.15787                   | 0.12143                    | 0.01732           | 0.01488        | 0.14329            | 0.13720         | 0.14650                  |
| 28.3170                            | 1728                        | 1                         | 0.03704                    | 29.9221           | 25.7140        | 7.48055            | 6.42851         | 0.80356                  |
| 764.559                            | 46656                       | 27                        | 1                          | 807.806           | 694.279        | 201.974            | 173.570         | 21.6962                  |
| 0.94636                            | 57.75                       | 0.03342                   | 0.1238                     | 1                 | 0.85937        | 0.25               | 0.21494         | 0.02686                  |
| 1.10123                            | 67.2006                     | 0.03889                   | 0.1440                     | 1.16365           | 1              | 0.29091            | 0.25            | 0.03125                  |
| 3.78543                            | 231                         | 0.13368                   | 0.4951                     | 4                 | 3.43747        | 1                  | 0.85937         | 0.10742                  |
| 4.40492                            | 268.803                     | 0.15556                   | 0.5761                     | 4.65460           | 4              | 1.16365            | 1               | 0.125                    |
| 35.2393                            | 2150.42                     | 1.24446                   | 0.04609                    | 37.2368           | 32             | 9.30920            | 8               | 1                        |

U. S. dry measure: 1 bushel—4 pecks—8 gallons—32 quarts—64 pints.

U. S. liquid measure: 1 gallon—4 quarts—8 pints—32 gills—128 fluid ounces.

U. S. apoth. measure: 1 fl. ounce,  $\frac{1}{2}$ —8 fl. drams,  $\frac{1}{3}$ —480 minims,  $\frac{1}{4}$ —29.574 cu.  $cm^3$ .

British Imperial gallon dry and liquid measure—1.03202 U. S. dry gal.—1.20091 U. S. liquid gal.

British Imperial gallon—277.410 cu. in.—4545.9631  $cm^3$ .

Weight of water at maximum density, 4° C, 45° lat., and sea level.

1 cu. ft.—62.4283 lbs. av.—28.3170 kg. 1 cu. in.—0.57804 oz. av.—16.3872 g.

1 gal., U. S. liquid—8.34545 lbs.—3.78543 kg.

1 gal., British Imperial—10.0221 lbs.—4.5459631 kg.

## MASSES AND WEIGHTS.

1 gram, g—10 decigrams, dg—100 centigrams, cg—1,000 milligrams, mg.

1 gram, g—0.1 decagram, dkg—0.01 hectogram, hg—0.001 kilogram, kg.

1 kilogram, kg—1 cu. decimeter of water or liter, 4° C, 45° lat., and sea level—15432.35639 grains, U. S. and British standard.

| Kilo-<br>grams,<br>kg. | Grains,<br>gr. | Ounces.         |                    | Pounds.         |                    | Tons.                        |                               |                               |
|------------------------|----------------|-----------------|--------------------|-----------------|--------------------|------------------------------|-------------------------------|-------------------------------|
|                        |                | Troy,<br>oz. t. | Avoir.,<br>oz. av. | Troy,<br>lb. t. | Avoir.,<br>lb. av. | Net,<br>short,<br>2,000 lbs. | Gross,<br>long,<br>2,240 lbs. | Metric,<br>long,<br>1,000 kg. |
| 1                      | 15432.4        | 32.1507         | 35.2740            | 2.67923         | 2.20462            | 0.11102                      | 0.19842                       | 0.001                         |
| 0.16480                | 1              | 0.12083         | 0.12286            | 0.17736         | 0.14220            | 0.17143                      | 0.16378                       | 0.00480                       |
| 0.03110                | 480            | 1               | 1.09714            | 0.08333         | 0.06857            | 0.33429                      | 0.33061                       | 0.03110                       |
| 0.02635                | 437.5          | 0.91146         | 1                  | 0.07595         | 0.06250            | 0.31125                      | 0.27900                       | 0.26355                       |
| 0.37324                | 5760           | 12              | 13.1657            | 1               | 0.82236            | 0.11114                      | 0.13674                       | 0.03732                       |
| 0.45359                | 7000           | 14.5833         | 16                 | 1.21528         | 1                  | 0.00050                      | 0.04464                       | 0.04536                       |
| 907.185                | 14000000       | 29166.7         | 32000              | 2430.56         | 2000               | 1                            | 0.89296                       | 0.90719                       |
| 1016.05                | 15690000       | 32666.7         | 35840              | 2722.22         | 2240               | 1.12                         | 1                             | 1.01605                       |
| 1000                   | 15432356       | 32150.7         | 35274.0            | 2679.23         | 2204.62            | 1.10231                      | 0.98421                       | 1                             |

1 ounce avoird.—16 drams, avoird. 1 ounce troy—20 pennyweight, dwt.

1 ounce apoth.,  $\frac{1}{2}$ —8 drams,  $\frac{1}{3}$ —24 scruples,  $\frac{1}{4}$ —480 grains, gr—31.1035 g.

1 hundred weight—1/20 long ton—4 quarters—8 stone—112 lbs.—50.8024 kg.

Notations  $\frac{1}{2}$ ,  $\frac{1}{3}$ , etc., indicate that the  $\frac{1}{2}$ ,  $\frac{1}{3}$ , etc., are to be replaced by 2, 3, 4, etc., ciphers.

Example: 1 grain—0.02083—0.002083 oz. t. 1 grain—0.06480—0.0006480 kg.

*Equivalents of measure.*

## FORCES OR WEIGHTS PER UNITS OF LENGTH, LINEAR WEIGHTS.

1 dyne per centimeter = 0.00101979 g/cm = 0.000183719 poundal/in.  
 1 gram per centimeter = 980.5966 dynes/cm = 0.180154 poundal/in.  
 1 poundal per inch = 5443.11 dynes/cm = 5.55081 g/cm = 0.0310632 pound/in.

| Grams per centimeter, g/cm. | Grains per inch, gr./in. | Pounds per inch, lb./in. | Pounds per foot, lb./ft. | Pounds per yard, lb./yd. | Kilo-grams per meter, kg/m. | Net tons, 2,000 pounds, per mile. | Gross tons, 2,240 pounds, per mile. | Metric tons, 1,000 kg. per kilometer. |
|-----------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-----------------------------|-----------------------------------|-------------------------------------|---------------------------------------|
| 1                           | 39.1663                  | 0.15600                  | 0.06720                  | 0.20159                  | 0.10                        | 0.17740                           | 0.15839                             | 0.10                                  |
| 0.02551                     | 1                        | 0.1429                   | 0.1714                   | 0.5143                   | 0.2551                      | 0.34528                           | 0.34041                             | 0.2551                                |
| 178.579                     | 7000                     | 1                        | 12                       | 36                       | 17.8579                     | 31.6800                           | 28.2857                             | 17.8579                               |
| 14.8816                     | 583.333                  | 0.06333                  | 1                        | 3                        | 1.48816                     | 2.64000                           | 2.35714                             | 1.48816                               |
| 4.96054                     | 194.444                  | 0.02778                  | 0.33333                  | 1                        | 0.49605                     | 0.88000                           | 0.78571                             | 0.49605                               |
| 10                          | 391.983                  | 0.05600                  | 0.67197                  | 2.01591                  | 1                           | 1.77400                           | 1.58393                             | 1                                     |
| 5.63698                     | 220.960                  | 0.03157                  | 0.37879                  | 1.13636                  | 0.56370                     | 1                                 | 0.89286                             | 0.56370                               |
| 6.31342                     | 247.475                  | 0.03535                  | 0.42424                  | 1.27273                  | 0.63134                     | 1.12                              | 1                                   | 0.63134                               |
| 10                          | 391.983                  | 0.05600                  | 0.67197                  | 2.01591                  | 1                           | 1.77400                           | 1.58393                             | 1                                     |

## FORCES OR WEIGHTS PER UNITS OF AREA, PRESSURE.

1 dyne per sq. centimeter = 0.00101979 g/cm<sup>2</sup> = 0.000466646 pounds/in.<sup>2</sup>.  
 1 gram per sq. centimeter = 980.5966 dynes/cm<sup>2</sup> = 0.457592 pounds/in.<sup>2</sup>.  
 1 poundal per sq. inch = 2142.95 dynes/cm<sup>2</sup> = 2.18536 g/cm<sup>2</sup> = 0.0310632 pound/in.<sup>2</sup>.

| Kilo-grams per square centimeter, kg/cm. <sup>2</sup> | Pounds per square inch, lb./in. <sup>2</sup> | Pounds per square foot, lb./ft. <sup>2</sup> | Net tons, 2,000 pounds per square foot. | Atmospheres, standard, 760 mm. | Columns of mercury, Hg. 13.59593 sp. g. |         | Columns of water, max. density 4° C. |         |
|---|--|--|---|--------------------------------|---|---------|--------------------------------------|---------|
|   |  |  |   |                                | Milli-meters.                           | Inches. | Meters.                              | Feet.   |
| 1   | 14.2234                                      | 2048.17                                      | 1.02408                                 | 0.96778                        | 735.514                                 | 28.9572 | 10                                   | 32.8083 |
| 0.07031   | 1  | 144  | 0.07200                                 | 0.06804                        | 51.7116                                 | 2.03588 | 0.70307                              | 2.30665 |
| 0.14882   | 0.16944                                      | 1  | 0.00050                                 | 0.14725                        | 0.35911                                 | 0.01414 | 0.14882                              | 0.01602 |
| 0.97648   | 13.8889                                      | 2000   | 1                                       | 0.94502                        | 718.216                                 | 28.2762 | 9.76482                              | 32.0367 |
| 1.03329   | 14.6969                                      | 2116.35                                      | 1.05818                                 | 1                              | 760                                     | 29.9212 | 10.3329                              | 33.9006 |
| 0.11360   | 0.01934                                      | 2.78468                                      | 1.11392                                 | 0.11216                        | 1                                       | 0.03937 | 0.011360                             | 0.04461 |
| 0.03453   | 0.49119                                      | 70.7310                                      | 0.03537                                 | 0.03342                        | 25.4001                                 | 1       | 0.34534                              | 1.13299 |
| 0.10  | 1.42234                                      | 204.817                                      | 0.10241                                 | 0.09678                        | 73.5514                                 | 2.89572 | 1                                    | 3.28083 |
| 0.03048   | 0.43353                                      | 62.4283                                      | 0.03121                                 | 0.02950                        | 22.4185                                 | 0.88262 | 0.30480                              | 1       |

## FORCES OR WEIGHTS PER UNITS OF VOLUME, DENSITY.

1 dyne per cu. centimeter = 0.00101979 gram/cm<sup>3</sup> = 0.00118528 pounds/in.<sup>3</sup>.  
 1 gram per cu. centimeter = 980.5966 dynes/cm<sup>3</sup> = 1.162283 pounds/in.<sup>3</sup>.  
 1 poundal per cu. inch = 843.683 dynes/cm<sup>3</sup> = 0.860378 g/cm<sup>3</sup> = 0.0310632 pound/in.<sup>3</sup>.

| Grams per cubic centimeter, g/cm. <sup>3</sup> | Pounds per cubic inch, lb./in. <sup>3</sup> | Pounds per cubic foot, lb./ft. <sup>3</sup> | Pounds per cubic yard, lb./yd. <sup>3</sup> | Kilo-grams per cubic meter, kg/m. <sup>3</sup> | Pounds per bushel, U. S. | Pounds per gallon, dry, U. S. | Pounds per gallon, liquid, U. S. | Kilo-grams per hectoliter, kg/hl. |
|--|---|---|---|--|--------------------------|-------------------------------|----------------------------------|-----------------------------------|
| 1  | 0.03613                                     | 62.4283                                     | 1685.56                                     | 1000   | 77.6893                  | 9.71116                       | 8.34545                          | 100                               |
| 27.6797  | 1   | 1728  | 46656                                       | 27679.7  | 2150.42                  | 268.803                       | 231                              | 2767.97                           |
| 0.01602  | 0.15787                                     | 1   | 27  | 16.0184  | 1.24446                  | 0.15556                       | 0.13368                          | 1.60184                           |
| 0.15933  | 0.12143                                     | 0.03704                                     | 1   | 0.59327  | 0.04609                  | 0.15762                       | 0.14951                          | 0.05933                           |
| 0.001  | 0.3613                                      | 0.06243                                     | 1.68556                                     | 1  | 0.07769                  | 0.9711                        | 0.8345                           | 0.10                              |
| 0.01287  | 0.14650                                     | 0.80356                                     | 21.6962                                     | 12.8718  | 1                        | 0.125                         | 0.10742                          | 1.28718                           |
| 0.10297  | 0.13720                                     | 6.42851                                     | 173.570                                     | 102.974  | 8                        | 1                             | 0.85637                          | 10.2974                           |
| 0.11983  | 0.14329                                     | 7.48052                                     | 201.974                                     | 119.826  | 9.30920                  | 1.16365                       | 1                                | 11.9826                           |
| 0.01   | 0.3613                                      | 0.62428                                     | 16.8557                                     | 10   | 0.77689                  | 0.09711                       | 0.08345                          | 1                                 |

Notations 2, 3, 4, etc., indicate that the 1, 2, 3, 4, etc., are to be replaced by 2, 3, 4, etc., ciphers.  
 Example: 1 kg/m<sup>3</sup> = 0.13613 = 0.00003613 lb./in.<sup>3</sup>.

*Equivalents of measure.*

## ENERGY, WORK, HEAT.

- 1 dyne-centimeter = 1 erg = 0.00101979 gram-centimeter = 0.737612 foot-pound.  
 1 gram-centimeter = 980.5966 ergs = 0.7233 foot-pound.  
 1 foot-pound = 13557300 ergs = 13825.5 gram-centimeters.

| Kilogram-meters, kg-m. | Foot-pounds, ft.-lbs. | Horsepower-hour. |                    | Poncelet-hours, 100 kg-m-h. | Kilowatt-hours, kw-h. | Joules, 10 <sup>7</sup> ergs, j-s. | Thermal units.     |                  |
|------------------------|-----------------------|------------------|--------------------|-----------------------------|-----------------------|------------------------------------|--------------------|------------------|
|                        |                       | U. S., h. p.-h.  | Metric, 75 kg-m-h. |                             |                       |                                    | B. T. U., b. t. u. | Calorie, kg-cal. |
| 1                      | 7.23300               | 0.73653          | 0.13704            | 0.2778                      | 0.2724                | 9.80697                            | 0.9296             | 0.2342           |
| 0.13826                | 1                     | 0.75051          | 0.15121            | 0.3840                      | 0.3766                | 1.35573                            | 0.1285             | 0.3239           |
| 273745                 | 1980000               | 1                | 1.01387            | 0.76040                     | 0.74565               | 2684340                            | 2544.66            | 641.240          |
| 270000                 | 1952910               | 0.98632          | 1                  | 0.75                        | 0.73545               | 2647610                            | 2509.83            | 632.467          |
| 360000                 | 2603880               | 1.31509          | 1.33333            | 1                           | 0.98060               | 3530147                            | 3346.44            | 843.289          |
| 367123                 | 2655403               | 1.34111          | 1.35972            | 1.01979                     | 1                     | 3600000                            | 3412.66            | 859.975          |
| 0.10198                | 0.73761               | 0.33725          | 0.13777            | 0.2853                      | 0.2778                | 1                                  | 0.9490             | 0.2389           |
| 107.577                | 778.104               | 0.39930          | 0.39984            | 0.2988                      | 0.2930                | 1054.90                            | 1                  | 0.25200          |
| 426.900                | 3087.77               | 0.1559           | 0.1581             | 0.1186                      | 0.1163                | 4186.17                            | 3.96832            | 1                |

## POWER, RATE OF ENERGY AND HEAT.

- 1 erg per sec. = 1 dyne-cm/sec. = 0.00101979 gram-cm/sec. = 0.737612 foot-pounds/sec.  
 1 gram-centimeter per second = 980.5966 ergs/sec. = 0.7233 foot-pounds/sec.  
 1 foot-pound per second = 13557300 ergs/sec. = 13825.5 gram-cm/sec.

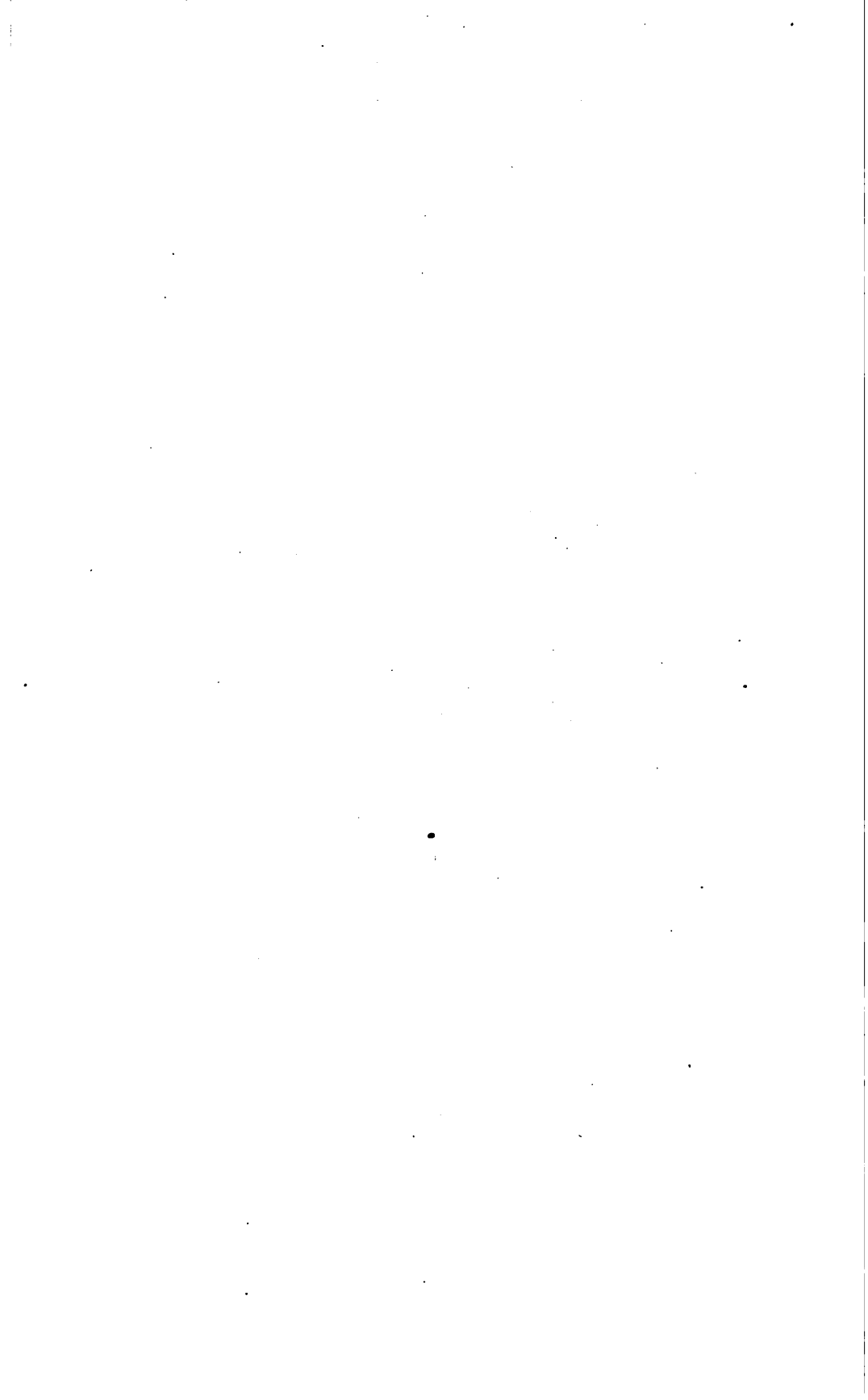
| Kilogram-meters per second, kg-m/s. | Foot-pounds per second, ft.-lbs./s. | Horsepower.            |                    | Poncelet, 100 kg-m/s. | Kilowatt, kw. | Watts, 10 <sup>7</sup> ergs/s. | Thermal units per sec. |                    |
|-------------------------------------|-------------------------------------|------------------------|--------------------|-----------------------|---------------|--------------------------------|------------------------|--------------------|
|                                     |                                     | U. S., 550 ft.-lbs./s. | Metric, 75 kg-m/s. |                       |               |                                | B. T. U., btu/s.       | Calorie, kg-cal/s. |
| 1                                   | 7.23300                             | 0.01315                | 0.01333            | 0.01                  | 0.9806        | 9.80597                        | 0.9296                 | 0.2342             |
| 0.13826                             | 1                                   | 0.1818                 | 0.1843             | 0.1383                | 0.1356        | 1.35573                        | 0.1285                 | 0.3237             |
| 76.0404                             | 550                                 | 1                      | 1.01387            | 0.76040               | 0.74565       | 745.650                        | 0.70685                | 0.17812            |
| 75                                  | 542.475                             | 0.98632                | 1                  | 0.75                  | 0.73545       | 735.448                        | 0.69718                | 0.17569            |
| 100                                 | 723.300                             | 1.31509                | 1.33333            | 1                     | 0.98060       | 980.597                        | 0.92957                | 0.23425            |
| 101.979                             | 737.612                             | 1.34111                | 1.35972            | 1.01979               | 1             | 1000                           | 0.94796                | 0.23888            |
| 0.10198                             | 0.73761                             | 0.1341                 | 0.1360             | 0.1020                | 0.001         | 1                              | 0.9490                 | 0.2389             |
| 107.577                             | 778.104                             | 1.41474                | 1.43436            | 1.07577               | 1.05490       | 1054.90                        | 1                      | 0.25200            |
| 426.900                             | 3087.77                             | 5.61412                | 5.69200            | 4.26900               | 4.18617       | 4186.17                        | 3.96832                | 1                  |

## VELOCITIES AND ACCELERATIONS.

- 1 kine = 1 centimeter per second = 0.0328083 foot per second.  
 1 radian per second = 57.2958 degrees per sec. = 0.159155 revolutions per sec.  
 1 gravity = 980.5966 centimeters per sec. per sec. = 32.1717 feet per sec. per sec.

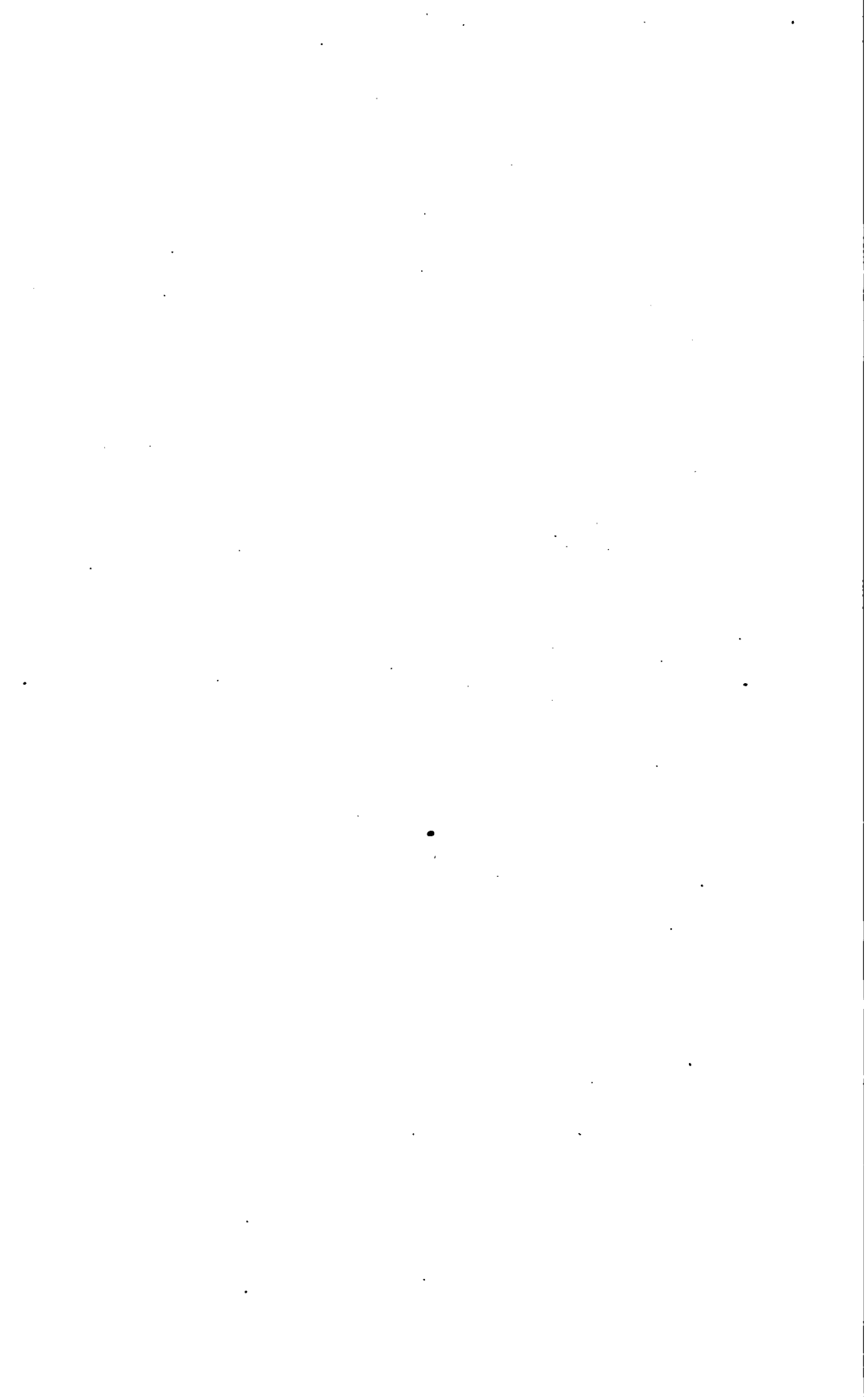
| Meters per second, m/s. | Feet per second, ft./s. | Miles per hour, M/h. | Knots per hour, U. S. | Kilo-meters hour, km/h. | Meter per sec/sec, m/s². | Feet per sec/sec, ft./s². | Miles per hour/sec, M/h-s. | Kilo-meter per hour/sec, km/h-s. |
|-------------------------|-------------------------|----------------------|-----------------------|-------------------------|--------------------------|---------------------------|----------------------------|----------------------------------|
| 1                       | 3.28083                 | 2.23693              | 1.94254               | 3.6                     |                          |                           |                            |                                  |
| 0.30480                 | 1                       | 0.68182              | 0.59209               | 1.09728                 |                          |                           |                            |                                  |
| 0.44704                 | 1.46667                 | 1                    | 0.86839               | 1.60935                 |                          |                           |                            |                                  |
| 0.51479                 | 1.68894                 | 1.15155              | 1                     | 1.85325                 |                          |                           |                            |                                  |
| 0.27778                 | 0.91134                 | 0.62137              | 0.53959               | 1                       |                          |                           |                            |                                  |
|                         |                         |                      |                       |                         | 1                        | 3.28083                   | 2.23693                    | 3.6                              |
|                         |                         |                      |                       |                         | 0.30480                  | 1                         | 0.68182                    | 1.09728                          |
|                         |                         |                      |                       |                         | 0.44704                  | 1.46667                   | 1                          | 1.60935                          |
|                         |                         |                      |                       |                         | 0.27778                  | 0.91134                   | 0.62137                    | 1                                |

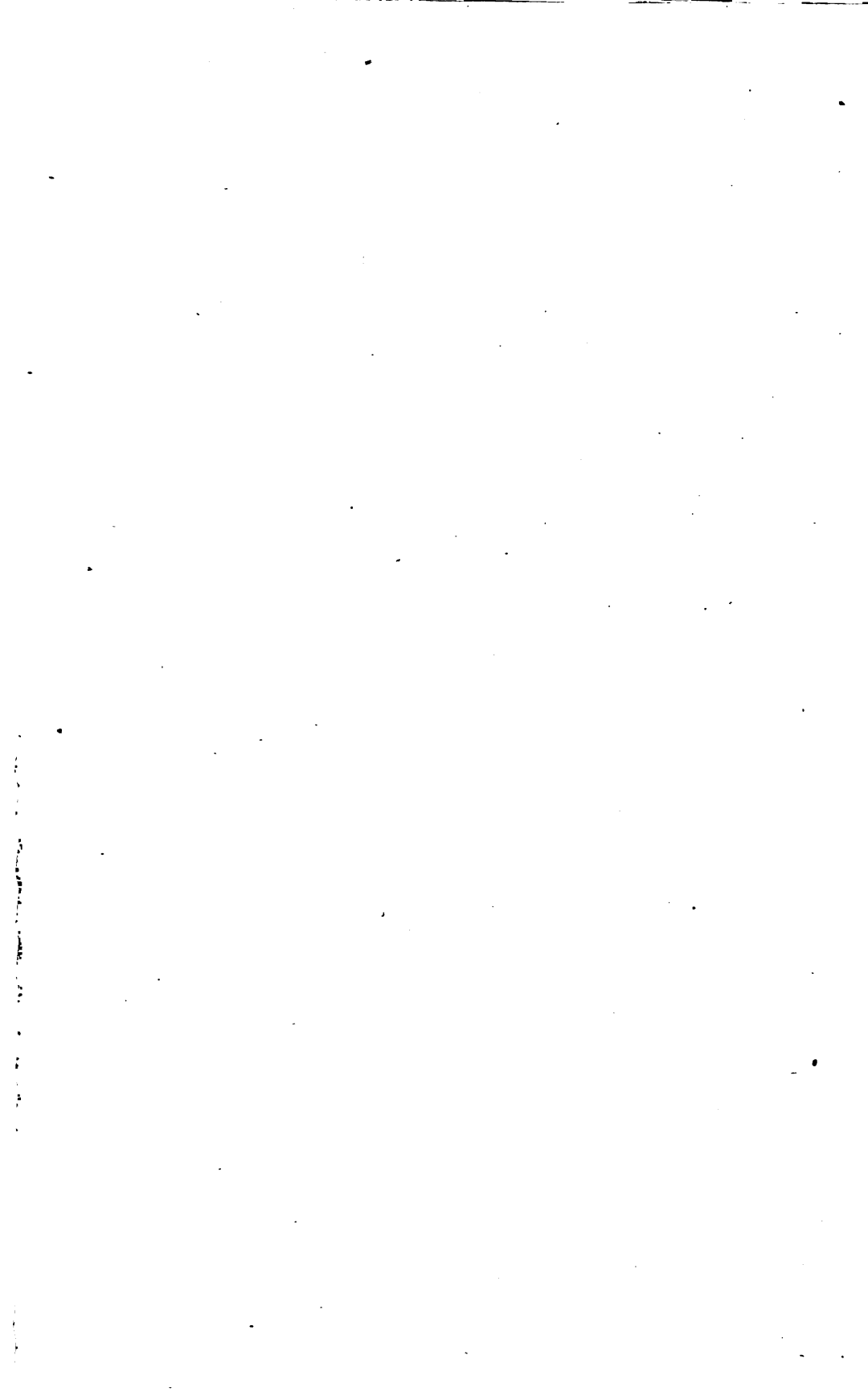
Notations 2, 3, 4, etc., indicate that the 1, 2, 3, 4, etc., are to be replaced by 2, 3, 4, etc., ciphers.  
 Example: 1 calorie = 0.1163 = 0.001163 kilowatt-hours.

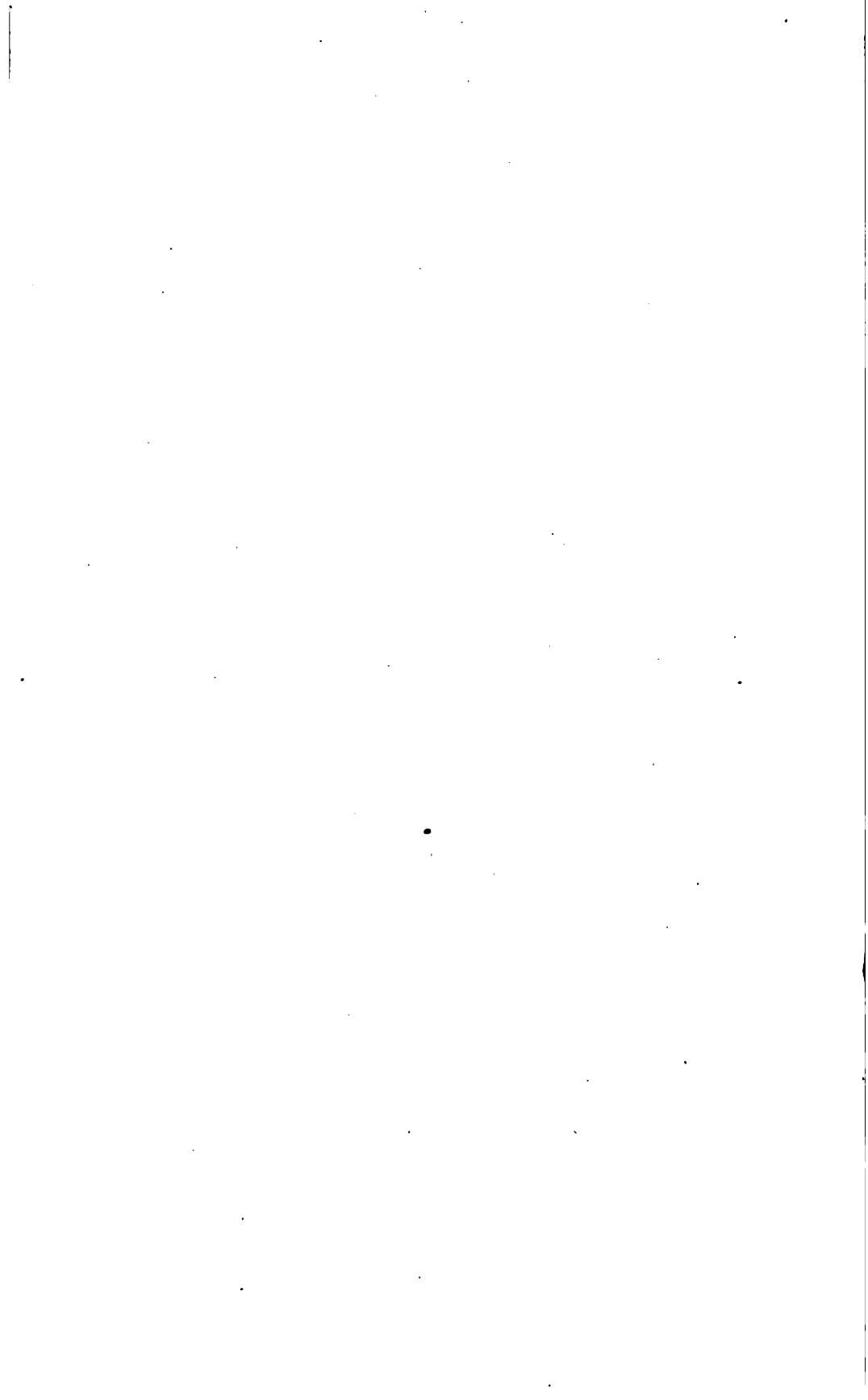














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